Magnesium-aluminum-zirconium oxide amorphous ternary composite: a dense and stable optical coating

ABSTRACT

In the present work, the process parameter dependent optical and structural properties of MgO-Al₂O₃-ZrO₂ ternary mixed-composite material have been investigated. Optical properties were derived from spectrophotometric measurements. The surface morphology, grain size distributions, crystallographic phases and process dependent material composition of films have been investigated through the use of Atomic Force Microscopy (AFM), X-ray diffraction analysis and Energy Dispersive X-ray (EDX) analysis. EDX analysis made evident the correlation between the optical constants and the process dependent compositions in the films. It is possible to achieve environmentally stable amorphous films with high packing density under certain optimized process conditions.

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Magnesium-aluminum-zirconium oxide amorphous ternary composite: a dense and stable optical coating

By

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Title Page

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ABSTRACT

In the present work, the process parameter dependent optical and structural properties of MgO-Al2O3-ZrO2 ternary mixed-composite material have been investigated. Optical properties were derived from spectrophotometric measurements. The surface morphology, grain size distributions, crystallographic phases and process dependent material composition of films have been investigated through the use of Atomic Force Microscopy (AFM), X-ray diffraction analysis and Energy Dispersive X-ray (EDX) analysis. EDX analysis made evident the correlation between the optical constants and the process dependent compositions in the films. It is possible to achieve environmentally stable amorphous films with high packing density under certain optimized process conditions.

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1. Introduction

The post-deposition instability of conventional physical-vapor-deposited, refractory-oxide-thin-films has persisted as a major obstacle in optical coating technology.\(^1\) Precision filters which make use of such films suffer from water vapor induced spectral shift. In typical electron beam deposited coatings, the root cause of this undesirable feature is columnar growth structure.\(^1\)\(^-\)\(^3\) This structure contains void distributions and grain boundaries which allow water vapor to adsorb and desorb from the film leading to substantial instabilities in optical and mechanical properties. One of the possible approaches to eliminate such a growth condition is to provide more kinetic energy to the vapor molecules. This leads to greater mobility during the condensation process thereby leading to higher packing density.\(^1\)\(^-\)\(^4\) Alternately, one may mix several materials in the vapor state to achieve similar results.\(^5\) Among the various film growth structures, it is always preferable to have a amorphous (or glassy) film structure for better stability and improved optical properties as opposed to the usual polycrystalline or very rare crystalline structures.\(^6\)\(^-\)\(^7\) The amorphous structure is also important in reducing the bulk scattering losses in the films.\(^6\) Over the years, such growth conditions have been achieved by various advanced techniques which include reactive sputtering, ion beam sputtering (IBS), plasma ion-assisted deposition, etc.\(^8\)\(^-\)\(^11\) Such techniques are quite complex and some times difficult to implement for the non-quarterwave coating design. In recent years, composite films are gaining the attention of researchers attempting to develop more stable optical coatings. It has been already established that it is possible to achieve novel film properties by mixing various thin film materials either during the vapor stage or as a solid solution.\(^12\) Since co-deposition techniques require very high quality process calibration and control, composite materials in solid solutions are favorable because of the simplified deposition process.\(^12\)\(^,\)\(^13\) It has been reported by various investigators that it is possible to stabilize the tetragonal or cubic phase in ZrO\(_2\) by adding various other refractory oxides which include MgO, CaO, Al\(_2\)O\(_3\), Y\(_2\)O\(_3\), etc.\(^14\) Some of the binary composites have excellent process modulated index tunability. Our earlier work on ZrO\(_2\)MgO binary system has shown a very interesting oxygen dependent refractive index tunability for the films deposited from the solid solution.\(^12\) The majority of earlier reports on other partially stabilized binary systems have reported polycrystalline film structures.\(^15\) So far, a very limited amount work has been
performed on ternary composite systems. In the present work, we have carried out extensive investigations on MgO-Al2O3-ZrO2 ternary system and optimized the process to highly stable optical coatings. Interestingly, it has been observed that cubic structure typical to ZrO2-MgO system has been completely eliminated by adding the third component Al2O3 to the solid solution. The films evaporated from the ternary composite have a highly amorphous structure, which is the most preferable growth condition for high spectral quality and environmentally stable optical coatings.

2. Earlier Research on Partial Stabilized Zirconia Films

Historically, Zirconia (ZrO2) has played a very important role in optical coating technology because of its superior properties such as high refractive index, high melting temperature, hardness, low thermal conductivity, better corrosion resistance, extended spectral transmission, better compatibility with SiO2 and stability for high power laser applications. The polymorphic nature of ZrO2 is very well known and has been the subject of many studies. Partially stabilized zirconias (PSZ's) are mostly two-phase ceramics that have optical and mechanical properties generally superior to those of fully stabilized bodies. The main advantage of PSZ over fully stabilized zirconia is its low overall thermal expansion coefficient. It is possible to stabilize the tetragonal, monoclinic or cubic phase in the material by adding suitable quantities of various other refractory oxides to zirconia which include MgO, In2O3, Y2O3, CaO, Al2O3, Sc2O3, SnO2, ZnO, CeO, etc. Very interestingly, some of these refractory oxides have exhibited extended solid solubility in ZrO2 yielding very different optical and structural properties. A variety of structural symmetries can be achieved through the addition of different amounts of stabilizing solutes to the ZrO2 host. It has been reported by Qadri and coworkers that the cubic phase can be conveniently achieved in electron beam co-evaporated zirconia-zincia thin films. Gilmore and his coworker reported achieving the tetragonal phase in magnetron sputtered ZrO2-Al2O3 films. Tsai and co-worker reported that the off-axis grown yttria-stabilized-zirconia (YSZ) films exhibit atomically smooth interfaces. It is generally accepted, however, that the most useful mechanical properties are obtained by partial stabilization so that, most frequently, a two or three-phase microstructure results. During earlier investigations, experimenters reported that the improved properties in partially stabilized zirconia (PSZ) materials were due to the simultaneous presence of both monoclinic and cubic structures. Subsequently it was reported that it is possible to achieve a room temperature stable tetragonal phase by adding a suitable amount of CaO to zirconia. Although the results on binary mixtures are very interesting and benefited number of technological programs, not much work
has been performed with ternary mixtures. There are a few reports available on zirconia-magnesia-ceria ternary compositions. Ruff and co-workers have reported some results on ZrO$_2$-ThO$_2$-CaO, ZrO$_2$-ThO$_2$-MgO, ZrO$_2$-BeO-CaO and ZrO$_2$-BeO-CeO$_2$ ternary systems.\textsuperscript{21-22} On the basis of the results presented in these experiments, it is observed that the melting point of zirconia can be lowered by addition of the third component CeO$_2$. So far no investigations have been carried out on optical and physical properties of ternary systems. In the present study we have investigated optical and structural properties of a very interesting ternary composite, MgO-Al$_2$O$_3$-ZrO$_2$, evaporated from a solid solution. Earlier investigations report that zirconia can be stabilized to a cubic phase with the addition of MgO, whereas the addition of Al$_2$O$_3$ leads to tetragonal phase.\textsuperscript{20} During the present investigation, we have observed that, when both Al$_2$O$_3$ and MgO are present in the composite, both of the above phases disappear leading to most desirable amorphous condition. Very interesting non-linear optical and structural inhomogeneities have been observed in films deposited under various deposition conditions. It is also possible to obtain very high packing density in the composite leading to practically negligible air-to-vacuum shift in the spectral characteristics of the coatings.

3. Experimental Details

The Balzers BAK-760 coating system, optical monitor, and other analytical equipment used for this experiment has been described elsewhere in detail.\textsuperscript{12} We deposited ternary composite films on 25-mm-diameter, 3- to 5-mm-thick optically polished quartz and BK7 substrates by evaporating optical grade MgO-Al$_2$O$_3$-ZrO$_2$ solid solution typically 99.0% pure (M/s CERAC Inc., supplied, stock number M-1126). A total of over twenty samples deposited under various process conditions were prepared for the present optimization study. When a particular parameter was varied, the other parameters were kept constant at an optimum value to observe the distinct changes in the optical and structural properties of the film. Energy Dispersive X-ray (EDX) analysis confirmed the presence of a trace amount of Ca in some of the thin film samples. During e-beam evaporation from a crucible, this material has a tendency to form towering structures of 1-2" in height that somewhat resemble stalagmites. One has to take necessary precaution while using multi-crucible sources for the deposition because such growths may obstruct the crucible rotation while switching between the materials. Careful pre-conditioning designed to initially obtain a level, uniform melt sometimes reduces this undesirable behavior. During this investigation, the pre- and post-deposition transmittance and reflectance spectra of the films were recorded.
BALZERS GSM-420 broadband, optical monitor/controller over 350-975nm. Post-deposition spectral characteristics over an extended wavelength region (200-2000nm) were recorded using a Perkin-Elmer Lamda-19 UV-vis-NIR spectrophotometer. The mean optical constants were derived by use of “SPECTR” software developed by Sahoo. This software has a special provision to draw the computer generated envelopes for the transmittance and reflectance extrema even for the films that have highly non-linear inhomogeneity. The semi-quantitative process dependent compositions of the films were determined by EDX analysis. The Surface morphologies of selected coatings were investigated using Scanning electron microscopy (SEM). Surface topography, bearing ratio and power spectral densities of coatings were analyzed using a Topometrix TMX 2000 series atomic force microscope. Structural properties of the films were investigated using X-ray diffraction analysis carried out on Rigaku (USA) diffractometer system.

4. Films with Non-linear and Mixed Inhomogeneity

It has been observed during online spectral monitoring of the films under certain deposition condition that index of refraction varied continuously along the growth direction in several non-linear fashions. Such non-linear and mixed inhomogeneities have very interesting effects on overall spectral characteristics of the coatings. We have already discussed these effects in our earlier investigations on ZrO₂MgO binary system. Most recently, an extensive theoretical analysis has been published by Tikhanravov et al., on influences of mixed inhomogeneities on the spectral characteristics of single thin films. It is interesting to note that the transmittance and reflectance extrema in films of this type show considerable modulation which is very different than in films with linear inhomogeneity. In linear inhomogeneity, the change in spectral amplitude becomes more prominent for the wavelengths that satisfy the relationship:

$$\lambda_m = \frac{2 \cdot n_2 \cdot z}{m} \quad m=1,2,3,...$$

where the various notations in this equation are as per the reference-25. In case n > n₂ > nₐ, the wavelengths λₘ corresponds to transmittance maxima (reflectance minima). In films with non-linear inhomogeneity, the interference extrema modulation depends on the extent and quality of the non-linear growth. For a weakly absorbing dielectric film with a functional index inhomogeneity of h(z), the modulation in reflectance and transmittance amplitudes at normal incidence are given by the following analytical expressions:
\[
\delta R(\lambda) = -\frac{4\pi n}{\lambda n_i} T(\lambda) \int_0^1 r'(\lambda) \left( \cos \frac{2\pi n z}{\lambda} + i \frac{n_i}{n} \sin \frac{2\pi n z}{\lambda} \right)^2 \tilde{n}(z) \, dz ,
\]

and

\[
\delta T(\lambda) = -\delta R(\lambda) + \frac{4\pi n}{\lambda n_i} T(\lambda) \int_0^1 \left( \cos \frac{2\pi n z}{\lambda} + i \frac{n_i}{n} \sin \frac{2\pi n z}{\lambda} \right)^2 \text{Im}[\tilde{n}(z)] \, dz ,
\]

where the various terms have their meanings as per the reference 25. If the function \(\tilde{n}(z)\) is smooth so that its derivatives, including higher order terms, can be neglected, then the above expressions can be assessed more conveniently. In case of highly nonlinear index functions, the computation of amplitudes of spectral modulation is very complex. These expressions also can be used for films with mixed modes of inhomogeneity (i.e. mixture of both homogeneous and inhomogeneous growth profiles). These mixed inhomogeneities are very frequently observed in composite films.12

In case of our present studies, we observed the most intense modulation to be in weakly absorbing region of the spectra (i.e. near-UV and UV region). The derivation of optical constants for such films from spectrophotometric measurements alone is extremely difficult. Sometimes numerical modeling helps in getting a starting solution for the computation. Fortunately the interference peak positions are very weakly affected by changes in index inhomogeneities.26,27 As a result, it is possible to compute the mean refractive index from the order of the peaks, peak positions and physical thickness as described by our earlier work. In such case, information from quartz crystal data, on-line optical monitoring values and thickness of the films measured by an independent technique appreciably improves the computational accuracy. Also, it is known that for a film with small inhomogeneity, the best fit with a homogeneous film model is obtained with a refractive index that is close to the geometrical mean of the refractive index values at the physical boundaries (i.e. the top and bottom) of the inhomogeneous film.25 Computation of mean optical constants for non-linear inhomogeneous films has been discussed extensively in our earlier work on ZrO2-MgO binary composite films.12 The same procedure has been adopted to derive optical constants of the present ternary films. The modulated experimental reflectance and transmittance of two non-linear inhomogeneous films have been depicted in Fig.1 and Fig. 2. It is also observed that it is possible to obtain fairly homogeneous growth structure under ambient as well as higher substrate temperature as shown in Fig.3. It is observed that the mean refractive indexes of the films (\(n_m\)) follow a four-parameter Cauchy dispersion equation as follows:

\[
n_m(\lambda) = a_0 + \frac{a_2}{\lambda^2} + \frac{a_3}{\lambda^3} + \frac{a_4}{\lambda^4} .
\]
where \( a_1, a_2, a_3 \) and \( a_4 \) are the coefficients for fitting. In Table-1, Cauchy coefficients for the films deposited under various substrate temperature (same rate and oxygen pressure) have been presented. The mean extinction coefficients \( (k_m) \) of these films follow a four-parameter logistic dispersion equation as follows:

\[
 k_m(\lambda) = \frac{a}{1 + (\lambda/c)^b} 
\]

In this equation, the parameter \( a \) is the asymptotic maximum, \( b \) is the slope parameter, \( c \) is the value at inflexion point of the curve and \( d \) is a symmetry parameter. The values of the coefficients for the films deposited under varying substrate temperature are given in Table-2.

5. Effect of Substrate Temperature

Substrate temperature has a very prominent effect on optical constants as well as structural properties in this composite. The films grown under ambient conditions show a fairly homogeneous growth structure. It is worth mentioning that even at ambient conditions the films have very high packing densities. The pre- and post-deposition transmittance characteristic of one such film is depicted in Fig. 4, where it can easily be seen that there is infinitesimal air-to-vacuum shift. The films are fairly homogeneous at the two extreme experimental temperatures as shown in Fig. 3. The rates and oxygen pressures were maintained at 0.4 nm/s and base pressure, respectively, as the substrate temperature was varied. At all other temperatures, non-linear inhomogeneity was the dominant growth structure and this is evident in the transmittance and reflectance spectra. In Fig. 1 and Fig. 2, such a behavior is depicted for two different substrate temperatures and oxygen pressures. The films grown at ambient temperature have the minimum index as shown in Fig. 5. When the substrate temperature was increased from ambient to 125 °C, the corresponding refractive index increased from 1.68 to 1.86 @ \( \lambda = 600 \text{nm} \) and then decreased to 1.78 with the further increase of temperature to 175 °C. When the temperature is increased beyond 175 °C, the refractive index value improved and it approached saturation above 237 °C. This interesting behavior is most likely due to temperature dependent compositional changes in the films, which are clearly evident in the EDX analysis. The mean extinction coefficients also have shown a similar behavior. There is a remarkable improvement in these coefficients in the temperature ranges between 150 to 200 °C as shown in Fig. 6.

Excluding the dip in the curve, the variation in refractive index as a function of substrate temperature approximately follows the trend one might expect for
conventional dielectrics. Typically, the refractive index monotonically improves as temperature increases, up to an optimal value, due to higher mobility that leads to better packing density and improved order in the film. Extinction coefficients typically improve with higher substrate temperatures, once again up to a limiting maximum temperature. Crystallographic, structural, and compositional changes, however, may alter the conventional trends.

6. Effect of Rate of Evaporation

Rate has a very distinct influence on optical constants as well as structural properties of the composite films under present investigation. As it is well known, the amount of kinetic energy that the vapor atoms carry after leaving the source is dependent upon the rate of deposition. This influences the mobility of the atoms during nucleation and growth of the films on the substrate. During the rate variation, the substrates' temperatures and oxygen pressures were maintained constant at 162 °C and 1x10⁻⁴ mbar respectively. It is observed that the rate of evaporation has an optimum value that leads to the improved and favorable optical constants. We found this value to be 1 nm/s for our present set of conditions. Further increases in the rate deteriorated the index value appreciably, as shown in the Fig. 7. Similar trend was also observed for the mean extinction coefficients. The extinction coefficient values became higher for the films deposited rate more than 1nm/s, as depicted in Fig. 8. Such behavior can be attributed to various compositional changes that occur due to the dynamics of the nucleation and growth process under different rates of deposition.

In conventional films, both refractive indices typically improve monotonically to optimum values (higher refractive index and lower extinction coefficient) as rate increases to an optimum value due to improved vapor energy and mobility. Beyond an optimum rate, incomplete relaxation occurs along with trapping of gases in voids leading to decreased index and higher roughness. In the present ternary films, the refractive index follows this trend, whereas the extinction coefficient remains consistently low except at the fastest rate.

7. Effect of Oxygen Pressure

Oxygen pressure also has a very pronounced effect on the films growth conditions. During variation of oxygen pressure, the substrates' temperatures and deposition rates were maintained at 162 °C and 0.4 nm/s respectively. The optical constants showed an optimum value for the films deposited at 5x10⁻⁵ mbar as shown in
the Fig. 9. On both side of this value the index shows a downward trend. The slope for mean refractive index above $3 \times 10^{-4}$ mbar is steeper compared to that of lower oxygen values. It is interesting to note that the oxygen enrichment factor is not as high as in the case of binary composites. The extinction coefficients increase in value at higher oxygen pressure, especially for the films deposited above $3 \times 10^{-4}$ mbar as depicted in Fig. 10. It is interesting to note from the EDX results that relative amount of Zr in the films became higher than Al at higher oxygen pressures above $6 \times 10^{-4}$ mbar. This might be due to a relatively longer mean free path for the higher atomic mass Zr material in the oxygen or perhaps to a superior accommodation coefficient of Zr under higher oxygen pressure.

With reactive evaporation of most dielectric oxides, both refractive indices typically improve monotonically to optimum values (higher refractive index and lower extinction coefficient) as oxygen pressure increases to an optimum value due to improved oxidation of the film materials. Beyond an optimum pressure, the energy of impinging material declines as the mean free path declines. In addition, excessive trapping of gases in voids occurs. Once again these effects lead to decreased index and higher roughness. In the present ternary films, the refractive index follows this trend, whereas the extinction coefficient remains consistently low except at the higher pressures.

8. Atomic Force Microscope (AFM) Analysis

We have used atomic force microscopy to investigate the surface topography both qualitatively and quantitatively. The equipment used for this investigation is a Topometrix TMX 2000 series Explorer AFM. The probes used for the scans are the standard triangular cantilever types (AFM tips-1520) with a typical spring constant of 0.032 N/m. The surface morphology of a film deposited with a substrate temperature of 162 °C, deposition rate of 1 nm/s and oxygen pressure of $2 \times 10^{-4}$ mbar is depicted in Fig. 11. The power spectral density (PSD) function resulting from topographic measurements provide much qualitative information on the surface profile and grain structure in thin films. It is well known in topographic analysis that the roughness is proportional to the area under the curve for each PSD plot. The evolution of roughness can be very well described based on the transitions in PSD plots. The statistical PSD function ($P(k)$) is defined as the square of the magnitude of the Fourier transform of the surface profile; it provides pertinent information concerning the
amplitude of the surface features as a function of lateral spatial frequency. From a line height profile $Z(x)$, the $P(k)$ function is derived as

$$P(k) = \frac{1}{L} \left| \int dx \cdot e^{i2\pi kx} \cdot Z(x) \right|^2 \text{ in units of } \text{Å}^2 \mu\text{m},$$

(6)

where $L$ is the scan length in μm, $Z(x)$ the line height profile in Å and $k$ the spatial frequency in μm$^{-1}$. The bearing ratio, which is defined as the percentage of total data appearing above the selected $Z$-height, also helps in presenting the distribution of various sizes of grains in the sample. The temperature, rate and oxygen pressure dependent PSD function and bearing ratio (BR) plots are depicted in the Figs. 12-17. It can be seen from Fig. 12, that the grain size and surface roughness is the highest for the films deposited at a substrate temperature of 175 °C. The films deposited at highest substrate temperature have shown the lowest surface roughness as well as smaller grain size. But like refractive index plots, the temperature dependent roughness also has shown a very interesting modulative effect between 125-190 °C. The films deposited at both the highest and lowest rates of evaporation have shown higher roughness values as compared with intermediate rates of deposition. Films deposited between 0.6-1.0 nm/s have the minimum roughness, as shown in the Fig. 13. The films deposited under base pressure have smoother surface profiles that those deposited at high oxygen pressure, as depicted in the Fig. 14. Films deposited at 8x10$^{-4}$ mbar have very high roughness values. Bearing ratio plots for the films deposited under different process parameters have been depicted in Figs. 15-17. The BR plot for the film deposited under our highest experimental oxygen pressure are most distinctive, indicative of a very rough surface.

9. X-ray Diffraction Analysis

X-ray diffraction measurements were carried out on a Rigaku (USA) diffractometer with Cu(Kα) (λ=1.5418 Å) radiation. The angular resolution was ±0.02° for each sample. Since the films were deposited on quartz as well as BK7 substrates, the short-range order of SiO$_2$ contributes to the background structure, especially in the lower 2θ region. Diffraction spectra from most of the samples have shown completely amorphous structure. Films grown at higher deposition rates and lower oxygen pressure, however, show an extremely weak tetragonal phase as depicted in the Fig. 18. The films deposited at both ambient and at the highest experimental temperatures are the most completely amorphous, as shown in the Fig. 19. This characteristic is most likely due to the presence of higher relative quantities of Al$_2$O$_3$ in the sample. Earlier works by Glimore and co-worker on ZrO$_2$+Al$_2$O$_3$ composite have indicated amorphous
structure in their reactive magnetron sputtered films.\textsuperscript{20} The phase diagram of zirconia and alumina has been reported to be of eutectic type with a very low solid phase solubility factor.\textsuperscript{20} It is also reported that it is possible to convert the amorphous structures to a stable tetragonal phase with suitable post-annealing. Our experiments have shown that the rate of evaporation has more prominent effect on the crystallographic phase as compared to substrate temperature and oxygen pressure as shown in Fig. 18.

10. Compositional Analysis by Energy-Dispersive X-Ray (EDX)

In order to determine the cause of large variation in the optical constants in films prepared under varied deposition conditions, we tried to investigate the variation in composition in the samples. Other investigators have pointed out that the relative amounts of either Al$_2$O$_3$ or MgO in binary solution with ZrO$_2$ substantially affects the optical and structural properties. In order to measure the relative amount of Zr, Al, Mg and O$_2$ in our samples, we performed relative compositional analysis using the energy dispersive X-ray (EDX) feature available in a 4Pi Environmental Scanning Electron Microscope, model Spectral Engine-II. The electron beam energy used was 10 KeV with a Detector resolution of 145 eV. The carbon peak at 0.25KeV is the usual peak associated with hydrocarbon contamination nearly always present on samples introduced from the laboratory environments. Most of the films have shown the presence of a trace amount of Ca in the samples (also indicated by the supplier). A typical EDX spectrum, shown for the film deposited at substrate temperature of 188 °C, rate 0.4 nm/s and without additional oxygen, is depicted in Fig. 20. Comparisons between the material composition and optical constants in films deposited under varying process conditions reveal very interesting, but complex, relationships. The relative amount of Zr in the composite films varied drastically as a function of oxygen pressure in a non-systematic fashion as shown in Fig. 21. The lowest index occurs at the highest oxygen pressure where Zr content reaches a maximum; however, the lowest Zr content does not correspond to the highest index value. Regarding variations in composition as a function of deposition rate, the largest compositional variation occurs at the minimum deposition rate value of 4 nm/s (Fig. 22). At this value, the relative amount of Zr is drastically lower and Mg is slightly higher, whereas the index of refraction is rather low. At other deposition rate values, there is minimal variation in composition with moderate change in index. EDX analysis of the films deposited with various substrate temperatures (Fig. 23) have clearly indicated the relative increase in Zr content with the temperature except at our highest experimental temperature. There
is some complex modulation of the relative composition of Mg and O₂ as a function of temperature. Overall, it is difficult to establish any suitable functional dependence between the compositions and mean optical constants. This is, most probably, due to very complex growth structure of the ternary composite film involving four elements (Zr, Al, Mg and O₂) that are affected by the dynamics of the nucleation process on the substrate surface.

11. Metal Dielectric Spectral Selective Solar Filter

Using this composite material, we have been able to start development of a highly stable pre-filter coating for a solar vector magnetograph instrument. It is well known the most popular metals like Ag, Au and Al have better film properties when deposited under ambient conditions. Metallic films mostly carry a tensile stress. When combined with dielectrics, one has to use a dielectric with compressive stress or very low tensile stress in order to develop stable multilayer metal-dielectric filters, especially when number of metal layers is high in the device. Most conventional dielectrics have very inferior optical properties when deposited under ambient conditions. Most of the time, the post-deposition behavior is very unstable in devices that make use of such dielectrics. The MgO-Al₂O₃-ZrO₂ ternary composite used in this study has excellent optical and mechanical properties even under ambient conditions. Because of overall low residual stress, it is an ideal material for developing metal-dielectric filter. The high packing density of the films even at ambient conditions makes the post-deposition spectral characteristic very stable as is evident in comparisons between the measurements in air and vacuum. In Figs. 24 and 25, we have shown the experimental spectral characteristics of two different developmental metal-dielectric filters measured in air as well as vacuum. The typical design for these filters (Fig. 25) is as follows:

Sub. (72.48T 15.77M 132.33T 15.55M 432.48T 14.66M 134.12T 23.93M 727.71T 13.03M 78.7Tr) Air,

where T is the ternary composite layer and M is the silver layer. All the design thicknesses are given in nm (physical thickness). Silver thicknesses in this design are constrained to remain more than a critical thickness in order to avoid island growth and the high stress regions.

12. Conclusion

The process parameter dependent optical and structural properties of MgO-Al₂O₃-ZrO₂ ternary composite films have been investigated in detail. A highly stable, stress-free, amorphous structure has been achieved in these films ideal for development
of environmentally stable optical coatings. The stress-free feature has enabled
development of stable, precision metal-dielectric multilayer filters. This composite also
has very interesting non-linear inhomogeneous properties as is evident in the
transmittance and reflectance spectra. It may be possible to make use of such behavior
to develop rugate filters. It is also possible to achieve the homogeneous growth
conditions, which can be utilized in development of conventional optical coatings. It is
difficult at this point to establish a suitable functional dependence between various
elementary compositions and optical properties of the ternary film. Such an
understanding may be possible with more complex on-line analysis and modeling of the
deposition-parameter-dependent-nucleation process in these films.

13. Acknowledgment

This research was performed while N.K. Sahoo held a National Research
Council-NASA/Marshall Space Flight Center (MSFC) Research Associateship. The
authors acknowledge the help of Marcus Vlasse of MSFC in carrying out the x-ray
diffraction analysis and are also grateful to him for the useful technical discussions in
interpreting the data. The authors also acknowledge the help of J.E. Coston of MSFC in
performing EDX and SEM analysis.
14. References


### Table - 1

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Table - 2

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<th>Sub. Temp in °C</th>
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<th>Coefficient 'b'</th>
<th>Coefficient 'c'</th>
<th>Coefficient 'd'</th>
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Caption to Tables

Table 1: Cauchy coefficients for the films deposited under the same rate of deposition (0.4 nm/s) and with no additional oxygen, but with varying substrate temperatures.

Table 2: Logistic coefficients for the films deposited under the same rate of deposition (0.4 nm/s) and with no additional oxygen, but with varying substrate temperatures.
Caption to Figures

Fig. 1: Transmittance and Reflectance characteristics of the experimental films deposited under substrate temperature of 200 °C, rate 0.4 nm/s and base value of oxygen pressure. Interference peaks in the lower end of the spectra have been considerably modulated because of structural non-linear inhomogeneity.

Fig. 2: Transmittance and Reflectance characteristics of the experimental films deposited under substrate temperature of 162 °C, rate 0.4 nm/s and oxygen pressure of 5x10⁻⁵ mbar. Interference peaks in the lower end of the spectra have also been considerably modulated because of structural non-linear inhomogeneity at this process condition.

Fig. 3: Transmittance and Reflectance characteristics of the experimental films deposited under two extreme experimental substrate temperatures (ambient and 237 °C), rate 0.4 nm/s and base pressure of oxygen. Dispersive behavior in interference peaks clearly indicates the absence of non-linear inhomogeneity. On-line optical monitoring has indicated a fairly homogeneous growth at these conditions.

Fig. 4: Experimental characteristics of an as deposited film measured in air as well as vacuum. Spectral characteristics have shown almost negligible transition between both the measurements.

Fig. 5: Spectral variation of mean refractive index with respect to the substrate temperature. The rates and oxygen pressures were maintained at 0.4 nm/s and base value respectively.

Fig. 6: Spectral variation of mean extinction coefficient with respect to the substrate temperature. The rates and oxygen pressures were maintained at 0.4 nm/s and base value respectively.
Fig. 7: Spectral variation of mean refractive index with respect to the rate of deposition. The substrates' temperatures and oxygen pressures were maintained at 162 °C and 1x10^-4 mbar respectively.

Fig. 8: Spectral variation of mean extinction coefficient with respect to the rate of deposition. The substrates' temperatures and oxygen pressures were maintained at 162 °C and 1x10^-4 mbar respectively.

Fig. 9: Spectral variation of mean refractive index with respect to the oxygen pressure. The rates and substrate temperatures were maintained at 0.4 nm/s and 162 °C respectively.

Fig. 10: Spectral variation of mean extinction coefficient with respect to the oxygen pressure. The rates and substrate temperatures were maintained at 0.4 nm/s and 162 °C respectively.

Fig. 11: Surface topography of a composite film deposited under optimum rate of deposition.

Fig. 12: Power Spectral Densities (PSDs) and surface roughness of the films deposited under various substrate temperatures.

Fig. 13: Power Spectral Densities (PSDs) and surface roughness of the films deposited under various rates of deposition.

Fig. 14: Power Spectral Densities (PSDs) and surface roughness of the films deposited under various oxygen pressures.

Fig. 15: Bearing Ratio plots for the films deposited under various substrate temperatures.

Fig. 16: Bearing Ratio plots for the films deposited under various rates of deposition.

Fig. 17: Bearing Ratio plots for the films deposited under various oxygen pressures.
Fig. 18: X-ray diffraction peaks of the films deposited under various deposition rates and oxygen pressures. Some of the films have shown an extremely weak tetragonal structure.

Fig. 19: X-ray diffraction analysis of the films deposited under different substrate temperatures.

Fig. 20: A typical EDX analysis spectrum of a film deposited under substrate temperature 188 °C, rate 0.4 nm/s and without any additional oxygen.

Fig. 21: EDX analyses of the films showing oxygen pressure dependent composition and mean refractive index values.

Fig. 22: EDX analyses of the films showing rate dependent composition and mean refractive index values.

Fig. 23: EDX analyses of the films showing substrate temperature dependent composition and mean refractive index values.

Fig. 24: Experimental spectral characteristic of a metal dielectric filter using Ag and the ternary composite.

Fig. 25: Experimental spectral characteristic of a metal dielectric filter using Ag and the ternary composite.
Non-linear Inhomogeneity
Temperature=200 °C
Rate=0.4 nm/s
Oxygen Pressure=Base value

Transmittance
Reflectance
Wavelength (nm)
200 400 600 800 1000 1200 1400 1600 1800 2000

Strong Modulation of Reflectance & Transmittance extrema due to non-linear inhomogeneity
Non-linear Inhomogeneity

Temperature = 162 °C
Rate = 0.4 nm/s
Oxygen Pressure = 5 × 10^{-5} mbar
Fairly Homogeneous conditions
(a) : T=Ambient, R=0.4 nm/s, O₂=Base Pressure
(b) : T=237 °C, R=0.4 nm/s, O₂=Base Pressure
(c) : Substrate Transmittance
(d) : Substrate Reflectance
Air-to-vacuum Shift

T=Ambient, R=0.4nm/s, No Oxygen

(a): --- Measured in Vacuum
(b): ---- Measured in Air
(c): --------- Substrate Transmittance
             (Sub.: BALZERS BK7)
Temperature Effect

- (a) Ambient
- (b) 125 °C
- (c) 150 °C
- (d) 162 °C
- (e) 175 °C
- (f) 188 °C
- (g) 200 °C
- (h) 237 °C
Effect of Substrate Temperature

(a) : Ambient
(b) : 150 °C
(c) : 175 °C
(d) : 200 °C
(e) : 125 °C
(f) : 162 °C
(g) : 188 °C
(h) : 237 °C

@ \( \lambda = 600 \text{nm} \)
Mean Refractive Index vs. Rate (nm/sec)

@ \( \lambda = 600 \text{nm} \)

Rate Effect:
- (a) : 0.4 nm/s
- (b) : 0.6 nm/s
- (c) : 0.8 nm/s
- (d) : 1.0 nm/s
- (e) : 1.2 nm/s

Mean Refractive Index vs. Wavelength (nm)
Graph 1: Mean Extinction Coefficient vs. Rate (nm/sec) at \( \lambda = 600\text{nm} \)

Graph 2: Rate Effect
(a) 0.4nm/s
(b) 0.6nm/s
(c) 0.8nm/s
(d) 1.0nm/s
(e) 1.2nm/s

Graph 3: Mean Extinction Coefficient (k) vs. Wavelength (nm)
Oxygen Effect
(a) : Base Pressure
(b) : 5x10^{-5} mbar
(c) : 1x10^{-4} mbar
(d) : 3x10^{-4} mbar
(e) : 6x10^{-4} mbar
(f) : 8x10^{-4} mbar

Mean Refractive Index (n)

Wavelength (nm)
Effect Of Oxygen Pressure

(a) : Ambient    (b) : $5 \times 10^{-5}$ mbar
(c) : $1 \times 10^{-4}$ mbar    (d) : $3 \times 10^{-4}$ mbar
(e) : $6 \times 10^{-4}$ mbar    (f) : $8 \times 10^{-4}$ mbar

Mean Extinction Coefficient ($k$) vs. Wavelength (nm)

Mean Extinction Coefficient vs. Oxygen Pressure (mbar)

@ $\lambda = 600$ nm
Area Ra=1.0389 nm
Area RMS=1.3019 nm
Average Height=9.2630 nm
(Temp=162°C, R=1.0 nm/s, Oxy=1.0e-4 mbar)
Power Spectral Density

Spatial Frequency (k) (μm⁻¹)

Rate Effect
(a) 0.4nm/s
(b) 0.6nm/s
(c) 0.8nm/s
(d) 1.0nm/s
(e) 1.2nm/s

Area RMS Roughness (nm)

Rate (nm/s)
Oxygen Effect
(a) — Ambient
(b) — 5x10⁻⁵ mbar
(c) — 1x10⁻⁴ mbar
(d) — 3x10⁻⁴ mbar
(e) — 6x10⁻⁴ mbar
(f) — 8x10⁻⁴ mbar

Power Spectral Density

Spatial Frequency (k) (μm⁻¹)
Oxygen Effect
(a) -- Base Pressure
(b) -- 5e-5mbar
(c) -- 1e-4mbar
(d) -- 3e-4mbar
(e) -- 6e-4mbar
(f) -- 8e-4mbar

![Graph showing the effect of oxygen at different pressures on bearing ratio and roughness.](image)
XRD-Analysis for the Films deposited under different Rates & Oxygen pressures but at same Substrate Temperature (@ T=162°C)

(a): R=0.4nm/s, O₂=5x10⁻⁵mbar
(b): R=0.6nm/s, O₂=1x10⁻⁴mbar
(c): R=0.8nm/s, O₂=1x10⁻⁴mbar
(d): R=1.0nm/s, O₂=1x10⁻⁴mbar
(e): R=1.2nm/s, O₂=1x10⁻⁴mbar
X-Ray Diffraction Analysis

- MCF @ T=Ambient
  (Amorphous Structure)

- MCF @ T=237 °C
  (Amorphous Structure)

- Blank Substrate
MG/AL/ZR-OXIDE FILM ON BK7 GLASS DISK

SAMPLE #10

Analyst: COSTON/SMITHERS  keV: 10.00  Current: 0.50  Live Time: 100.00  eV/Channel= 10.00
Detector Resolution: 145.00 eV  Take-off angle= 35.00  Spectrum # 1 From the file: 1997-199 Spectrum.Dat