Field Measurement of the Acoustic Nonlinearity Parameter in Turbine Blades

Yolanda L. Hinton
U.S. Army Research Laboratory
Vehicle Technology Directorate
Langley Research Center, Hampton, Virginia

Jeong K. Na
Energy Services Group, Williamsburg, Virginia

William T. Yost
Langley Research Center, Hampton, Virginia

Gregory L. Kessel
Virginia Power, Glen Allen, Virginia

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National Aeronautics and  
Space Administration  
Langley Research Center  
Hampton, Virginia 23681-2199

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INTRODUCTION

As an acoustic wave passes through a material, nonlinearities in the material produce harmonics of the acoustic wave. The amplitudes of the incident wave and the harmonics are related by the acoustic nonlinearity parameter. The acoustic nonlinearity parameter, $\beta$, is influenced by crystal structure, fatigue state, dislocation dipole density, precipitates and their phases, coherency strains, and other material conditions. The nonlinearity parameter has been shown to be sensitive to fatigue in stainless steel turbine blades [1].

The acoustic nonlinearity parameter is defined by the nonlinear form of the classic wave equation:

$$\frac{\partial^2 u}{\partial t^2} = c^2 (1 - \beta \frac{\partial u}{\partial a}) \frac{\partial^2 u}{\partial a^2}$$

where $u$ is particle displacement, $a$ is a Lagrangian coordinate, and $c$ is the infinitesimal wave speed. $\beta$ is a material property, described by

$$\beta = \left( \frac{A_2}{A_1^2} \right) \frac{8c^2}{\omega^2 a}$$

where $A_1$ and $A_2$ are the particle displacement amplitudes of the fundamental and second harmonic acoustic waves respectively, and $\omega$ is the angular frequency of the fundamental wave. Yost and Cantrell [2] proposed a substitutional technique for measuring $\beta$ using resonant ultrasonic transducers rather than absolute displacement transducers. In the case that $\beta$ is known for a given reference material, $\beta'$ may be measured for another specimen by measuring the voltage output from resonant transducers for both materials and using the equation

$$\beta' = \left( \frac{c'}{c} \right)^2 \left( \frac{d}{d'} \right) \left( \frac{V_2^n/V_1^n}{V_2/V_1} \right) \beta$$

where $V_1$ and $V_2$ are the peak output voltages for the fundamental and second harmonic waves, $c$ is longitudinal wave speed, and $d$ is the distance traveled (the specimen thickness). The primed values refer to the unknown specimen and the unprimed values refer to the reference specimen. It is necessary that the same measurement system be used to measure both materials, and that the specimens be of the same acoustic impedance.
EXPERIMENTAL PROCEDURES

The acoustic nonlinearity parameter was measured in turbine blades made of 403 stainless steel on Unit 5 at Virginia Power’s Chesterfield Power Station during a maintenance outage. These blades were designed for a forty-year life and had been in service 34 years. Measurements were taken by holding two transducers in contact with and on opposite sides of the turbine blades. The transducers were placed and gently rocked back and forth until the amplitude of the received signal was maximized, in order to compensate for the curvature of the blades. A Harisonic 5 MHz, 0.5 inch diameter, damped PZT ultrasonic transducer was used to transmit a 5 MHz signal through the blades. The signal was generated by a system designed for nonlinear acoustics, with a 5 MHz, three-cycle tone burst, and passed through a 5 MHz low pass filter. The fundamental signal was detected with a 10 MHz single crystal, non-resonant lithium niobate transducer, passed though a 20 dB pre-amplifier and the nonlinear acoustics system receiver with 22 dB gain. The second harmonic signal was detected with the same 10 MHz lithium niobate transducer, passed through a 9.8 MHz high pass filter, a 40 dB preamplifier and the system receiver with 22 dB gain. One thousand samples of each of the fundamental and second harmonic signals were captured and averaged by a digital oscilloscope. The amplitudes were recorded from the oscilloscope display. The measurements were made at three locations on each of several turbine blades: near the outer tie wire, on the boss at the inner tie wire, and midway between the two tie wires. These are the areas of highest stress that we can reach, and where failures are most likely to occur. The measurement was repeated four or more times at each location. The blade root is another region of high stress and likely failures, but it is not accessible for this measurement. Figure 1 is a photograph of the turbine blades, showing the inner and outer tie wires and the region between them.

The measurement technique was replicated in the laboratory on specimens of aluminum 2024 and 410Cb stainless steel on which $\beta$ had previously been measured. This allowed the nonlinearity parameter of the turbine blades to be calculated by the substitutional technique. The 410Cb stainless steel specimen, with $\beta=7.2$, was used as a reference for subsequent measurements because its structure and acoustic impedance are similar to the 403 stainless steel used in the turbine blades.

The measured amplitude of the acoustic wave is dependent upon the angle between the wave and the surface of the transducer, and the surface roughness. Therefore, a series of specimens with varying angles between the surfaces were fabricated of 410Cb stainless and finished to a surface roughness of about 63 rms, the roughness of the blades at installation, in order to study these effects. The acoustic nonlinearity parameter was measured in these canted specimens and the results are shown in Figure 2. A retired blade from another unit at the Chesterfield power station was cut at the measurement location and used to measure the angle between the surfaces at the boss near the tie wire, and at an area comparable to the midsapn region where measurements were taken on the Chesterfield-5 blades. In both cases the angle between the surfaces was about 120°. The correction factor for this angle and...
surface roughness was determined from the data in figure 1 to be 201% and was applied to the data. The measurements for other angles and surface finishes are reported elsewhere.

The nonlinearity parameter was also measured in ten-year old blades of 17-4Ph stainless steel at the Mt. Storm, West Virginia Power Plant for comparison with the data from the Chesterfield plant.

![Figure 1. Turbine blades at Chesterfield plant. Measurements were taken near tie wires and midway between them. Turbine blades are approximately 85 centimeters long; tie wires are about 20 centimeters apart.]

![Figure 2. The effect of surface canting on the nonlinearity parameter of 410Cb stainless steel at a surface finish of rms 63.]

\[ y = 0.083x^2 - 0.427x + 5.365 \]
EXPERIMENTAL RESULTS

The nonlinearity parameter was measured for 14 blades. The results are shown in figures 3-4. Figure 3 shows $\beta$ for fourteen blades, corrected for the angle between the transducers. Five or more measurements at each location on each blade were taken, and the standard deviations calculated with two exceptions: only one measurement was taken at the inner tie wire on blade 44, and none on blade 98 due to limited access to the measurement location. The standard deviations are shown by the error bars. In most cases, the standard deviations were small, demonstrating the measurement is repeatable. The standard deviations on blades 2 and 29 at the inner tie wire were larger than most of the other measurements, indicating most likely an instability in transducer mounting. This measurement was taken on the boss at the tie wire. Placing the transducers near the edge of or on the radius of the boss causes some of the uncertainty in this measurement. A high standard deviation was seen in blade 1 at the point midway between the two tie wires. This is an area where the curvature of the blade is greatest and there is no distinguishing physical characteristic guiding placement of the transducers. In this case, the measurements may not have been taken exactly at the same location on the blade.

Figure 4a shows the average of all measurements made on the fourteen blades, with error bars indicating one standard deviation. The average $\beta$ near the outer tie wire is 41.3, an increase of 474% over $\beta$ of the virgin material. Near the inner tie wire, $\beta$ is 27.3 and midway between the two tie wires $\beta$ is 32.2, increases of 280 and 347% over the original value. This indicates that the region around the outer tie wire has experienced more fatigue induced damage than have the other two regions. The tie wires reduce the amount of flexural bending in the turbine blades during operation. The region around the inner tie wire would experience less bending due to constraints by the rest of the blade. In addition, the boss area around the tie wire is of greater thickness, increasing the flexural stiffness and further reducing bending. The area between the two tie wires is slightly less restrained and able to bend more, and would, therefore, see more fatigue loading. The standard deviations of these measurements indicate that the values of $\beta$ at the inner tie wire and the midspan may be even closer than the mean values indicate.

The measurements from blades at Mt. Storm are shown in figure 4b. The nonlinearity parameter in these ten-year old blades was found to have increased by about 242% when compared to unfatigued material.
Figure 3. Beta measured at three locations on each of fourteen blades. Error bars indicate one standard deviation.
DISCUSSION

Precise placement of the transducers for measurement of $\beta$ was found to be difficult. The physical space between blades is very small, making it difficult to hold the transducers in place. The amplitude of the ultrasonic signals will be greatest when the wave has a direct path from one transducer to the other. The transducers must be positioned on opposite sides of the blade with centers aligned. Because the blade surfaces are not flat, compensation must be made for the curvature of the blades. In most cases, several measurements were made while attempting to hold the transducers in the same locations. For these measurements, the amplitudes were repeatable. In cases where the transducers were removed from the blade surfaces and repositioned, the standard deviations are higher, and the measurements less repeatable. This indicates that the reproducibility in location of the transducers on the blade surface is the more critical factor, implying that we have a transducer positioning error or that we have a substantial point-to-point variation in $\beta$.

The data were corrected for the effect of the angle between the surfaces of the transmitting and receiving transducers. This angle was measured on a retired blade from another unit at Chesterfield, and was of a different design than those on the Chesterfield-5 unit. In the future, the angle will be measured at the time and location the beta measurements are made.

Figure 4. a. Average beta at three locations in 34-year old Chesterfield blades. b. Beta measured in 10-year old turbine blades at Mt. Storm Power Plant. Error bars indicate one standard deviation.
CONCLUSIONS

The acoustic nonlinearity parameter $\beta$ was measured on fourteen L-0 turbine blades at the Chesterfield Power Station Unit 5 and eleven blades at Mt. Storm Unit 3. $\beta$ was found to have increased in the Chesterfield turbine blades from that of the virgin material by as much as 474%. $\beta$ is greatest at outer tie wire, less at inner tie wire. Midway between tie wires, $\beta$ is slightly greater than at inner tie wire. This suggests that the region of the blade near the outer tie wire has been subjected to higher fatigue loads and experienced more fatigue damage than have the other two regions where measurements were taken. These values must be compared to values in failed blades to determine residual life. The increase in $\beta$ for the Mt. Storm blades was 242%. These blades have been in service for only ten years, whereas the Chesterfield blades are 34 years old, and have been subjected to many more fatigue cycles.

The effects of surface angle and surface roughness were included in the measurements. The surface angle was estimated from measurements on a blade of similar, though not identical, design. The thickness of the blades, corresponding to the distance between the transducers, was measured with a micrometer. This measurement is not accurate because of the curvature of the blades. A more precise measure is needed for accurate measurement of $\beta$. It was assumed that the surface roughness of the blades had not changed since installation. This needs to be validated. The difficulty of making the measurements repeatably due to limited access and manual placement of the transducers needs to be addressed by designing and implementing a mechanical device that will also measure thickness and surface angle.

REFERENCES

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Yolanda L. Hinton, Jeong K. Na, William T. Yost, and Gregory L. Kessel

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- NASA Langley Research Center
  Hampton, VA 23681-2199
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Nonlinear acoustics techniques were used to measure fatigue in turbine blades in a power generation plant. The measurements were made in the field using a reference based measurement technique, and a reference sample previously measured in the laboratory. The acoustic nonlinearity parameter showed significant increase with fatigue in the blades, as indicated by service age and areas of increased stress. The technique shows promise for effectively measuring fatigue in field applications and predicting subsequent failures.

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