Hydrodynamic Models of Line-Driven Accretion Disk Winds III: Local Ionization Equilibrium

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ABSTRACT

We present time-dependent numerical hydrodynamic models of line-driven accretion disk winds in cataclysmic variable systems and calculate wind mass-loss rates and terminal velocities. The models are 2.5-dimensional, include an energy balance condition with radiative heating and cooling processes, and includes local ionization equilibrium introducing time dependence and spatial dependence on the line radiation force parameters. The radiation field is assumed to originate in an optically thick accretion disk. Wind ion populations are calculated under the assumption that local ionization equilibrium is determined by photoionization and radiative recombination, similar to a photoionized nebula. We find a steady wind flowing from the accretion disk. Radiative heating tends to maintain the temperature in the higher density wind regions near the disk surface, rather than cooling adiabatically. For a disk luminosity $L_{\text{disk}} = L_\odot$, white dwarf mass $M_{\text{wd}} = 0.6M_\odot$, and white dwarf radii $R_{\text{wd}} = 0.01R_\odot$, we obtain a wind mass-loss rate of $\dot{M}_{\text{wind}} = 4 \times 10^{-12}M_\odot \text{yr}^{-1}$, and a terminal velocity of $\sim 3000 \text{ km s}^{-1}$. These results confirm the general velocity and density structures found in our earlier constant ionization equilibrium adiabatic CV wind models. Further we establish here 2.5D numerical models that can be extended to QSO/AGN winds where the local ionization equilibrium will play a crucial role in the overall dynamics.

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1. Introduction

Ultraviolet observations of Cataclysmic Variables (CVs) show that virtually all non-magnetic CVs with high mass accretion rates (\( \geq 4 \times 10^{-10} M \odot \text{yr}^{-1} \)) exhibit P Cygni profiles in the resonance lines (e.g. Córdova & Mason 1982; Greenstein & Oke 1982; Guinan & Sion 1982; Klare et al. 1982; Vitello & Shlosman 1993; Prinja & Rosen 1995; Friedjung, Selvelli, & Cassatella 1997; Gansicke, Beuermann, & Thomas 1997; Knigge et al. 1997; Prinja et al. 2000). These profiles consist of blue-shifted absorption and redshifted emission, with the emission most prominent in high inclination systems (e.g. Hutchings 1980; Krautter et al. 1981; Holm, Panek, & Shiffer III 1982; Córdova & Mason 1985; Mason et al. 1995; Cheng et al. 1997), and the absorption appearing at low and intermediate inclinations. The most straightforward explanation for these observations is in terms of a wind originating from the accretion disk. The wind is driven by radiation pressure from the disk UV continuum absorbed by line transitions, analogous to the radiation driven winds in early type stars. Support for this scenario came from Drew (1987), who calculated theoretical C IV 1549 Å line-profiles from one-dimensional kinematic CV wind models, for a wide variety of wind and disk parameters. Drew (1987) found that the dependence on the form of the UV resonance lines with inclination angle could be accounted for by a bipolar wind emerging from an accretion disk.

One-dimensional dynamical models for line-driven winds (LDW) in CVs were developed independently by Vitello & Shlosman (1988) and Kallman (1988). Further efforts came through two-dimensional kinematic modeling (Shlosman & Vitello 1993; Knigge, Woods, & Drew 1995), which succeeded in showing consistency between the assumed polar geometry of a disk wind and observed profiles; but such models were unable to self-consistently calculate the wind dynamics including the effects of rotation and the anisotropic disk radiation field.

Two-dimensional disk wind dynamical models were developed by Icke (1980), but these did not take into account the radiation pressure due to line absorption. For a typical white dwarf mass of 0.6\( M \odot \) (Leibert 1980; Silvestri et al. 2001) the disk luminosity required to produce such a wind without line radiation pressure (assuming radiation pressure due to continuum scattering only) would require a luminosity of \( \sim 10^5 L \odot \) (Icke 1980), several magnitudes above the observed luminosity of CVs which vary between 0.01\( L \odot \) and 10\( L \odot \) (Patterson 1984). Icke (1980) did find that, for sufficiently high disk luminosities, a biconical disk wind would form. Icke (1981) suggested that biconical winds were a general property
of accretion disk winds independent of the wind driving mechanism.

Two-dimensional dynamical models of isothermal line-driven disk winds were presented by us Pereyra, Kallman, & Blondin (1997, hereafter Paper 1). Results from Paper 1 showed, in analogy with line-driven winds from early type stars, that terminal velocities are approximately independent of the luminosity of the disk, although increments in luminosity produce increments in mass-loss rate, and that rotational forces are important in the study of winds from accretion disks. They cause the velocity streamlines to collide, which reduce the speed and increase the density of the wind producing an enhanced density region. The highest absorption occurs in the enhanced density region where density is increased relative to a spherically diverging wind with the same mass loss rate and the velocity is roughly half the terminal velocity. This density increase is necessary in order to produce at least marginally optically thick lines.

We developed (Pereyra 1997; Pereyra, Kallman, & Blondin 2000, hereafter Paper 2) an adiabatic wind model (rather than isothermal), driven by a standard accretion disk (Shakura & Sunyaev 1973; Lynden-Bell & Pringle 1974) rather than an isothermal disk. The hydrodynamic models developed of line-driven accretion disk winds (LDADWs) in CVs included the radial structure of an optically thick accretion disk with the corresponding radiation fields and surface temperature distributions. The corresponding energy conservation equation was also implemented, including the adiabatic heating and cooling effects due to compression and expansion. From the computational models, assuming single scattering and constant ionization, we calculated theoretical line profiles for the C IV 1550 Å line, and found that the line profiles obtained were consistent with observations in their general form and strong dependence with inclination angle.

Proga, Stone, & Drew (1998) also developed two-dimensional models for these systems, obtaining similar results to the models presented here. They assumed an isothermal wind and constant values for the line radiation parameters throughout the wind. They found similar wind velocities and wind mass loss rates as we do here, although they assumed disk luminosities about an order of magnitude greater. A difference we find with the results of the models presented by Proga, Stone, & Drew (1998) is that they obtain unsteady flows characterized by large amplitude fluctuations in velocity and density, while for our previous models (Paper 1; Pereyra 1997; Paper 2) and in the models presented here we find a steady flow. We note that these large fluctuations (rather than the steady flow we find) could account for the difference in luminosity required by the Proga models, with respect to our models, to obtain similar wind mass loss rates. One possibility suggested by Proga, Stone, & Drew (1998) was that the spatial resolution of the models we presented in Paper 1 was too low to adequately resolve the wind. In paper 2 we increased significantly the spatial
resolution of our models and obtained similar steady results when compared to our earlier spatial resolutions used in Paper 1; thus showing that differences in spatial resolution of the models was not generating the difference between our steady disk wind models and the "intrinsically unsteady" disk winds reported by Proga, Stone, & Drew (1998). Another possibility is that the difference in the unsteady flows of the Proga models with respect to the steady flows we find is due to the boundary condition treatment in the Proga models, which appears to lead to instabilities at the base of the wind and in turn to the strong fluctuations reported.

It is well known that for early type stars, when a Sobolev treatment is used for the line radiation pressure (as we have done in our models and as has been applied by Proga, Stone, & Drew (1998) for accretion disk winds in CVs), a steady wind solution is obtained (e.g. Owocki & Puls 1999). The treatment of boundary conditions in numerical models for line driven winds in early type stars was discussed by Owocki, Cranmer, & Blondin (1994) and Cranmer & Owocki (1996). They find that the treatment of the lower (base of wind) boundary condition is "somewhat problematic". Further they find that if they used an arbitrarily high density, similar to the boundary conditions used by Proga, Stone, & Drew (1998), they would find oscillations at the base of the wind in both density and velocity. In both papers, in addition to other details in the boundary condition treatment (Owocki, Cranmer, & Blondin 1994; Cranmer & Owocki 1996), they lowered the density at the inner boundary until they found steady conditions at the base and were simultaneously able to resolve acceleration in the subsonic region. Therefore a conclusion in the area of numerical modeling that we derive is that by varying the treatment of boundary conditions at the base of a line driven wind, one can obtain strong fluctuations in density and velocity which are not necessarily physically intrinsic but are rather a consequence of the numerical details of the model.

Feldmeier & Shlosman (1999) and Feldmeier, Shlosman, & Vitello (1999) developed two-dimensional stationary models for CV disk winds where they solve the dynamics under the assumption that the wind streamlines lie on straight cones. The values of wind mass loss rates obtained through the models presented by Feldmeier, Shlosman, & Vitello (1999) for an isothermal disk (equation [11] of their paper) are consistent with those found in Paper 1. In addition Feldmeier, Shlosman, & Vitello (1999) find that in an isothermal disk (equations [10]-[11] of their paper) the wind mass loss rate scales as $\dot{M}_{\text{wind}} \propto L_{\text{disk}}^{1/\alpha}$, where $L_{\text{disk}}$ is the disk luminosity and $\alpha$ is line force multiplier parameter. This is the same scaling law reported in Paper 1. Further, the biconical geometry and wind tilt angle in the models of Feldmeier, Shlosman, & Vitello (1999) are roughly consistent with the velocity structures we find through full 2.5D hydrodynamic modeling of our earlier models (Paper 1; Pereyra 1997; Paper 2) and in the models presented here. We further note that
Feldmeier et al. suggest that detailed non-LTE calculations of the line-force multiplier may be important in the modeling of CV disk winds. This work is an additional step in that direction.

In spite of these encouraging results, a more realistic model which would include a detailed calculation of the UV spectrum from dynamically calculated density and velocity fields is desirable in order to make specific comparisons with observations. For instance, a maximum flux greater than 1.7 times the continuum has been reported for the emission component of P Cygni line profiles of C IV 1550Å from some cataclysmic variables (e.g. Córdova & Mason 1982), while from our previous models (Pereyra 1997; Paper 2) we find that the emission maximum of the C IV lines stays below 1.3 times the continuum flux for those angles where the absorption component is observed. This discrepancy may be due to some of the simplifications in our previous models or it may indicate a C IV line-emitting region other than the disk wind itself. Furthermore, in recent observational results, Froning et al. (2001) find relatively narrow absorption lines ($\lesssim 700$ km s$^{-1}$) in the FUV spectra of the cataclysmic variable U Gem. As Froning et al. (2001) have indicated, such lines cannot arise from the disk photosphere. In their work they suggest the possibility of an outer disk chromosphere to account for these lines, but it is also possible that some of these narrow FUV lines could be accounted for by an accretion disk wind.

An additional motivation for this work is that the models developed here can also be extended to the study of LDADWs in Quasars (QSOs), where the local ionization equilibrium will play an important in the overall dynamics (Murray et al. 1995; Hillier et al. 2002). Evidence for winds in QSOs is found in the broad absorption lines (BALs) observed in approximately 10% of the QSOs (e.g. Weymann 1997). If the wind in QSOs is generated from an accretion disk, then the presence of BALs in only a fraction of QSOs can be accounted for as a viewing-angle effect (Turnshek 1984); similar to the case of CVs where the accretion disk wind produces P Cygni profiles when observed “face-on” and emission lines (without absorption components) when seen “edge-on” (Pereyra, Kallman, & Blondin 2000). The x-ray luminosity in QSOs are generally comparable to the UV/optical luminosities (e.g. Tananbaum et al. 1979; Grindlay et al. 1980; Mushotzky, Done, & Pounds 1993; Laor 1997; George et al. 2000). Drew & Boksenberg (1984) found that such high x-ray luminosities would ionize the wind to a point where the populations of ions responsible for the BAL observed in QSOs would be too low to produce observable absorption lines. Murray et al. (1995) found that, with an appropriate x-ray shielding mechanism, LDADWs can produce wind densities and velocities consistent with BALs observed in QSOs. Strong changes in the ionization balance can produce observable effects in line formation in QSOs; as well as significant changes in the line radiation force parameters which will play an important role in the overall wind dynamics (Hillier et al. 2002).
In our previous models (Pereyra 1997; Paper 2) we had assumed constant ionization equilibrium throughout the wind and single scattering in the line profile calculations. In this work we extend our previous models to include radiative heating and cooling and ionization balance in the wind, and a calculation of the line radiation force parameters at each point in space at each time step. Our results are similar to those of Paper 2, and therefore act to confirm the general results found in our previous simpler models. They are a further step towards a model capable of self-consistently producing theoretical spectrum which may be compared in detail with observations; they can also be extended to the study of LDADWs in QSOs/AGN, where the local ionization equilibrium will play a crucial role in the overall dynamics (Murray et al. 1995; Hillier et al. 2002).

In §2 we discuss the radial structure of the accretion disk and the radiation field as implemented in our models. In §3 we present the ionization balance calculations applied in this work. We derive the expression used for the treatment of the line radiation pressure in §4. The treatment of radiative heating and cooling in this work is discussed in §5. In §6 we present and discuss the hydrodynamic calculations. The results of the models are presented and discussed in §7. We present a summary and the conclusions of this work in §8.

2. Accretion Disk

A key ingredient in the models presented in this work is the radiation field emerging from the accretion disk. The boundary layer where the disk intercepts the white dwarf and the white dwarf photosphere may also contribute to the radiation field. The white dwarf by itself (without considering the effects of the accreting mass) will have a luminosity of the order of $0.01L_\odot$ (Leibert 1980), while the accretion disk will have typical luminosities of the order of $L_\odot$ (Warner 1987). As we indicated in Paper 2, there is still uncertainty concerning the existence and spectrum of the boundary layer (Vrtilek et al. 1994; Mauche, Raymond, & Mattei 1995; Long et al. 1996; Szkody et al. 1999; Mauche & Raymond 2000; Froning et al. 2001). In the models presented here we have chosen not to explore the boundary layer issue in depth, but instead to consider the non-boundary layer scenario. We assume in this work that the radiation field is generated by the accretion disk alone, neglecting any boundary layer or white dwarf radiation. We assume here the standard accretion disk (Shakura & Sunyaev 1973; Lynden-Bell & Pringle 1974). In paper 2 we discussed some of the observational evidence for the existence of an accretion disk in CVs. We note that in this work we study the winds originating in nonmagnetic CVs in which an accretion disk is formed.

In the standard accretion disk model, the disk is assumed to be in a steady state. Shear
stresses transport angular momentum outwards as the material of the gas spirals inwards. Conservation of angular momentum leads to the following expression:

\[ W^2 \pi r^2 - \dot{M}_a \omega r^2 = C \text{ (constant)} \]  

where \( r \) is the radius, \( \dot{M}_a \) is the mass accretion rate, \( \omega \) is the corresponding angular velocity, and \( W \) is defined by:

\[ W = \int_{-z_0}^{z_0} w \phi \, dz \]

where \( z_0 \) is the half thickness of the disk and \( w \phi \) is shear stress between adjacent layers. With the additional assumption that the shear stresses are negligible in the inner disk radius:

\[ W = \frac{\dot{M}_a}{2 \pi r^2} (\omega r^2 - \omega_0 r_0^2) \]

where \( \omega_0 \) is the angular velocity at the inner disk radius \( r_0 \). In CVs the inner disk radius corresponds to the white dwarf radius \( R_{wd} \), i.e. the accretion disk extends from the inner Lagrangian point of the binary system down to the white dwarf surface.

Taking into account the work done by shear stresses, and assuming that, as the mass accretes inwards, the gravitational energy lost is emitted locally:

\[ Q = \frac{1}{4 \pi r} \frac{d}{dr} \left[ \dot{M}_a \left( \frac{\omega^2 r^2}{2} - \frac{GM}{r} \right) - W^2 \pi r^2 \right] \]

where \( Q \) is the radiated energy per area of the disk surface. Assuming that the disk material follows Keplerian orbits, i.e.

\[ \omega = \left( \frac{GM_{wd}}{r^3} \right)^{1/2} \]

where \( G \) is the gravitational constant and \( M_{wd} \) is the white dwarf mass; from equations (3)-(4) one finds:

\[ Q = \frac{3 \dot{M}_{accr} GM_{wd}}{8 \pi r^3} \left[ 1 - \left( \frac{r_0}{r} \right)^{1/2} \right] \]

The function \( Q(r) \) (equation [6]) was originally derived by Shakura & Sunyaev (1973) for binary systems with an accretion disk about a black hole. Popham & Narayan (1995) developed detailed models of boundary layers and accretion disks in cataclysmic variables and found that their models supported the same function \( Q(r) \) for the accretion disk in CVs.

Further, assuming that the disk is emitting locally as a blackbody, the radial temperature distribution of the disk will be given by:

\[ T = \left\{ \frac{3 \dot{M}_{accr} GM_{wd}}{8 \pi r^3} \left[ 1 - \left( \frac{r_0}{r} \right)^{1/2} \right] \right\}^{1/4} \]
where $\sigma_s$ is the Stefan-Boltzmann constant. Equation (6) is implemented in our model in the calculation of radiation flux throughout the wind, and consequently in the calculation of the continuum and line radiation pressure force. We assume local blackbody radiation. In our model we also assume that the temperature at the base of the wind is equal to the disk surface temperature for each radius. We wish to note here that the blackbody assumption of equation 7 will not strictly hold. Radiative diffusion of the energy from the inner parts of the disk to the disk photosphere will produce deviations from the blackbody assumption, limb darkening effects will produce deviations from the projected area in the angular dependence of the emitted flux, line scattering and electron scattering will produce deviations from the blackbody emission, the relatively high velocity gradients in the rotational shears as well as the wind velocity gradients will affect the line scattering; thus a detailed calculation of the spectrum emitted from the accretion disk would requires a 2.5D radiative transfer calculation of the disk atmosphere coupled with the corresponding velocity gradients.

Early attempts to calculate deviations of the actual disk spectrum from the local-blackbody assumption, applied locally spectra from stellar atmosphere codes (Herter et al. 1979; Kiplinger 1979, 1980; Mayo, Wickramasinghe, & Whelan 1980; Kolykhalov & Sunyaev 1984). More recently, local plane parallel radiative transfer models implementing disk vertical structure have been developed (Diaz, Wade, & Hubeny 1996; Hubeny & Hubeny 1997, 1998; Wade & Hubeny 1998; Hubeny et al. 2000). However, to our knowledge a self-consistent 2.5D radiative transfer model coupled with velocity shears of an accretion disk atmosphere has not yet been developed. Also, there still remains uncertainties regarding the variation of viscosity in the disk which in turn effects the vertical structure. Thus, due to its simplicity, the assumption of local blackbody spectrum has often been used to model accretion disk and their spectra (e.g. Shlosman & Vitello 1993; Knigge, Woods, & Drew 1995; Proga, Stone, & Drew 1998; Pereyra, Kallman, & Blondin 2000). In future work we shall consider the radiative transfer effects that deviate the disk spectrum from an ideal local-blackbody, and attempt to couple them with hydrodynamic calculations.

It is generally accepted that the mechanism for producing the shear stress in accretion disks is magnetic turbulence generated by the Balbus-Hawley magnetorotational instability (MRI) (Balbus & Hawley 1991). Three-dimensional magnetohydrodynamic simulations (e.g. Armitage 1998; Machida, Hayashi, & Matsumoto 2000; Hawley, Balbus, & Stone 2001; Hawley & Krolick 2001) suggest that the standard assumptions (e.g. Keplerian orbits; zero stress at inner radii) may not hold and that therefore corrections to equation (6) may arise. We believe that the standard Shakura-Sunyaev disk includes much of the physics involved in accretion disks, such as: gravity from a large central mass determining the average velocity fields in the disk, angular momentum transport, conversion of gravitational energy to radiative emission, and monotonic increase of temperature with decreasing radius.
(except of radius close to the inner disk radii) and local blackbody emission which accounts for the relatively “flat” continuum spectrum observed in systems where accretion disk are inferred. We also believe that it is important to explore “simple” models where the number of free parameters is small. More realistic disk models and radiation fields will be introduced at a later date.

3. Ionization Equilibrium and Line Opacity

The main wind driving mechanism in our model is the line radiation force generated as the disk emission encounters ionized gas above the disk. The wind material is thus driven from the disk photosphere achieving velocities of the order of a few thousand of \( \text{km} \, \text{s}^{-1} \). The line radiation force will depend on the available line opacity distribution of the wind material, which in turn is a direct function of the ion populations. Therefore the ion populations become an important ingredient in our models. In our previous work (Paper 1, Pereyra 1997, Paper 2), in an approach similar to that presented by Castor, Abbott, & Klein (1975) for OB star winds, we had assumed constant ionization equilibrium throughout the wind. Further we had assumed that the ion populations were similar to those of early type stars. These two assumptions allowed us to apply typical OB star line radiation force parameters (Abbott 1982) throughout the wind, significantly simplifying the numerical treatment. In this work we include the local ion population calculations simultaneously with the hydrodynamics as we describe below.

The ion populations of the wind material is initially at local thermodynamic equilibrium (LTE), since the wind starts at the disk photosphere. As the wind material rises, the ion populations are no longer in LTE. The material is irradiated by the disk, which is a non-Plank source (equations [6]-[7]). Due to the relatively low wind density, the ion populations above the disk are largely determined by photoionization and radiative recombination processes, which in turn are dependent on the incoming disk radiation. It is difficult to model the collisional and radiative processes which determine the ion populations, varying in space and time, while simultaneously solving the hydrodynamics of the system. In this work we assume that the ion populations in the disk wind are determined by photoionization and radiative recombination processes, similar to a photoionized nebula irradiated by an accretion disk. To illustrate the validity of this approximation we shall estimate the ratio between the radiative photoionization rate \( R_{ij} \) and the collisional ionization rate \( C_{ij} \). Under the condition that \( h\nu_o \gg kT_R \) and \( h\nu_o \gg kT_e \), where \( h \) is Planck’s constant, \( h\nu_o \) is the minimum energy required to ionize an atom from state \( i \) to state \( j \), \( k \) is Boltzmann’s constant, \( T_R \) is the temperature of the ionizing radiation, and \( T_e \) the electron temperature, the ratio can be approximated by
(Mihalas 1978):

$$\frac{R_{ij}}{C_{ij}} \approx \frac{4(2\pi^2 k)^{1/3} h\nu_o^2}{3 m_e^4 e^2 c^5} \left( \frac{W T_R}{n_e T_e} \right) \exp \left[ \frac{h\nu_o}{kT_e} \left( \frac{1}{kT_e} - \frac{1}{kT_R} \right) \right]$$

where $m_e$ is the electron mass, $e$ the electron charge, $c$ the speed of light, $W$ the dilution factor of the radiation from its source, and $n_e$ is the electron density. Taking for the CV case: $n_e \sim 10^8$ (this density is a typical value for the CV disk wind models we presented in Paper 2), $T_R \sim T_e \sim 30,000$ K, $W \sim 1/2$, and $h\nu_o \sim 13.6$ ev, from equation (8) we find:

$$\frac{R_{ij}}{C_{ij}} \sim 1.4 \times 10^8 .$$

As we have indicated above, in order to calculate the force due to line scattering, one in principle must consider the contribution to all lines which in turn will depend on the ion populations at a particular point in space in a particular time. In the calculation of ion population and line opacity we follow a similar scheme as that applied by Abbott (1982) for OB stars. In this work we assume that photoionization and radiative recombination processes determine the ion populations, therefore the ionization balance in the wind is determined through Saha’s equation for a gas photoionized by an external source:

$$\frac{N_{j+1} n_e}{N_j} = 2 W \frac{U_{j+1}}{U_j} \left( \frac{2\pi m_e kT_e}{h^2} \right)^{3/2} \frac{T_R}{T_e} \exp \left( - \frac{X_{IJ}}{kT_R} \right)$$

where $N_j$ and $N_{j+1}$ are the atom densities at stage $j$ and at the following ionization stage $j + 1$, $U_j$ and $U_{j+1}$ are the partition functions for the corresponding ionization stages, and $X_{IJ}$ is the ionization potential for the atom at stage $j$. Equation (10) has been applied to several astrophysical systems, e.g. stellar winds (Abbott & Lucy 1985; Schmutz et al. 1990; Lucy & Abbott 1993).

In the work presented here, we have assumed that the radiation is primarily coming from the accretion disk which presents a temperature dependent on radius (equation [7]). Equation (10) assumes that the photoionization rates are much greater than collisional ionization rates, thus:

$$N_j I_j \approx N_{j+1} R_{j+1}$$

where $I_j$ is photoionization rate for an atom at ionization stage $j$, and $R_{j+1}$ is the radiative recombination rate for the atom at ionization state $j + 1$. Therefore, from equation (10):

$$I_j = R_{j+1} \frac{2 W U_{j+1}}{n_e U_j} \left( \frac{2\pi m_e kT_e}{h^2} \right)^{3/2} \frac{T_R}{T_e} \exp \left( - \frac{X_{IJ}}{kT_R} \right).$$
In the accretion disk, the radiation is emitted at different temperatures (equation [7]), thus the total photoionization rate $I_{Tj}$ due to the disk radiation must equal the sum of all the contributions of photoionization rates due to the radiation emitted at each section of the disk surface:

$$I_{Tj} = R_{j+1} \frac{2}{n_e} U_{j+1} \left( \frac{2\pi m k T_e}{h^2} \right)^{3/2} \frac{1}{T_e} \int_{\text{disk}} W(r, \phi) T_R(r) \exp \left( -\frac{X_{lj}}{k T_R(r)} \right) r \, d\phi \, dr$$

(13)

where $W(r, \phi)$ is the dilution factor per source area, given by:

$$W(r, \phi) = \frac{1}{4\pi} \frac{\hat{z} \cdot (\vec{r}_p - \vec{r})}{|\vec{r}_p - \vec{r}|} \frac{1}{||\vec{r}_p - \vec{r}||^2}$$

(14)

i.e.:

$$W(r, \phi) = \frac{1}{4\pi} \frac{z}{(R^2 - 2R r \cos \phi + r^2 + z^2)^{3/2}}$$

(15)

where $\vec{r}_p \equiv (R, 0, z)$ is the position where the dilution factor is evaluated and $\vec{r} \equiv (r \cos \phi, r \sin \phi, 0)$ is the radiation source position on the disk.

Therefore, under the assumption that the photoionization and radiative recombination processes dominate over the collisional processes, we have:

$$\frac{N_{j+1} n_e}{N_j} = 2 \frac{U_{j+1}}{U_j} \left( \frac{2\pi m k T_e}{h^2} \right)^{3/2} \frac{1}{T_e} \int_{\text{disk}} W(r, \phi) T_R(r) \exp \left( -\frac{X_{lj}}{k T_R(r)} \right) r \, d\phi \, dr$$

(16)

which is the equation that we implement in this work for the calculation of ionization balance for the line radiation force.

Once the ion populations at different stages is calculated for each atom through the resolution of equation (16), the population for each energy level for a given ion stage of a given atom is obtained through Boltzmann’s equations:

$$\frac{N_{ij}}{N_{0j}} = \frac{g_{ij}}{g_{0j}} \exp \left( -\frac{X_{ij}}{k T_e} \right)$$

(17)

where $N_{ij}$ and $N_{0j}$ are the densities of a given atom at a given ionization stage $j$ at energy level $i$ and at the lowest energy level respectively, $g_{ij}$ and $g_{0j}$ are the degeneracies of energy level $i$ and at the lowest energy level respectively, and $X_{ij}$ is the difference in energy between level $i$ and the lowest energy level. We wish to note here that the LTE excited population assumption in equation (17), while allowing the local ionization equilibrium calculations to stay numerically manageable, will tend to be more accurate for the lower energy ion states which are the most crucial for the line radiation force. For early type stars Abbott (1982) found that roughly 90% of the line radiation force was due to lines arising from ground or metastable states.
After the ion populations at different stages at different energy levels for a given atom have been obtained, the line opacity of a given line for a given atom is calculated by the expression:

$$\kappa_L = \frac{\pi e^2}{m_e c} g_{ij} f_{luj} \left( \frac{N_{ij}/g_{ij} - N_{uj}/g_{uj}}{\rho} \right) \frac{1}{\Delta \nu_D}$$

(18)

where $g_{ij}$ and $g_{uj}$ are the degeneracies of the lower energy level $l$ and the upper energy level $u$ of ionization stage $j$ for a given line of a given atom, $f_{luj}$ is the absorption oscillator strength corresponding to the transition between lower energy level $l$ and upper energy level $u$ of ionization stage $j$ for a given line of a given atom, $N_{ij}$ and $N_{uj}$ are the ion densities of ionization stage $j$, lower energy level $l$, and upper energy level $u$ respectively, $\rho$ is the total mass density of the gas, and $\Delta \nu_D$ is the Doppler width of the given line. The Doppler width of the line is given by:

$$\Delta \nu_D = \frac{v_{th}}{c} \nu_L$$

(19)

where $v_{th}$ is the thermal velocity and the line frequency $\nu_L$ is given by:

$$\nu_L = \frac{X_{uj} - X_{lj}}{h}.$$  

(20)

4. Radiation Force

Once the line opacity $\kappa_L$ has been calculated through the above expressions for each atomic line at each ionization stage, the line radiation force is given by:

$$f_{rad} = \sum_{\text{lines}} \frac{\kappa_L \Delta \nu_D}{c} \int \left[ \frac{1}{\tau_L(\hat{n})} \int_{\tau_L(\hat{n})}^{\infty} e^{-\tau'} d\tau' \right] I(\hat{n}) \hat{n} d\Omega$$

(21)

where $I(\hat{n})$ is the radiation intensity, and $\tau_L(\hat{n})$ is the line optical depth.

The line optical depth $\tau_L(\hat{n})$ for a given line at a given direction $\hat{n}$, under the Sobolev approximation, is given by (Rybicki & Hummer 1978):

$$\tau_L(\hat{n}) = \frac{\rho \kappa_L v_{th}}{|\hat{n} \cdot \nabla (\hat{n} \cdot \vec{v})|}.$$  

(22)

As in Paper 1 and Paper 2, we assume in this work that the velocity gradient is primarily in the “z” direction and approximate the line optical depth by:

$$\tau_L(\hat{n}) \approx \frac{\rho \kappa_L v_{th}}{|\hat{n} \cdot \partial / \partial z|}.$$  

(23)
Integrating equation (21) in optical depth:

\[ \tilde{f}_{\text{rad}} = \sum_{\text{lines}} \kappa_L \frac{\Delta \nu D}{c} \left( \int \left[ 1 - \exp \left(-\tau_L(\hat{n}) \right) \right] I(\hat{n}) \hat{n} \, d\Omega \right) \]  
\[ \text{where } \tau_L(\hat{n}) = \text{Thomson cross section per unit mass.} \]  

therefore:

\[ \tilde{f}_{\text{rad}} = \int \left[ \frac{\sigma}{c} \int_{\infty}^{\infty} I(\hat{n}) \, d\nu \right] \left( \sum_{\text{lines}} \int_{\infty}^{\infty} \frac{I(\hat{n}) \Delta \nu D}{c} \left( 1 - \exp \left(-\frac{\kappa_L}{\sigma} \frac{\sigma}{\kappa_L} \tau_L(\hat{n}) \right) \right) \right) \hat{n} \, d\Omega \]  
\[ \text{where } \sigma \text{ is Thomson cross section per unit mass.} \]

In their work on radiation driven winds in OB stars, Castor, Abbott, & Klein (1975) and Abbott (1982), found that the sum over lines in equation (25) could be approximated by the following expression:

\[ \sum_{\text{lines}} \frac{I(\hat{n}) \Delta \nu D}{c} \left( 1 - \exp \left(-\frac{\kappa_L}{\sigma} \frac{\sigma}{\kappa_L} \tau_L(\hat{n}) \right) \right) \approx k'(\hat{n}) \left( \frac{\sigma}{\kappa_L} \tau_L(\hat{n}) \right)^{-\alpha'(\hat{n})} \]  
\[ \text{where the } k'(\hat{n}) \text{ and } \alpha'(\hat{n}) \text{ are constants for a given direction } \hat{n}. \]  

Defining \( t = \frac{\sigma}{\kappa_L} \tau_L(\hat{n}) \)

we have:

\[ \sum_{\text{lines}} \frac{I(\hat{n}) \Delta \nu D}{c} \left( 1 - \exp \left(-\frac{\kappa_L}{\sigma} \frac{\sigma}{\kappa_L} \tau_L(\hat{n}) \right) \right) \approx k'(\hat{n}) t^{-\alpha'(\hat{n})} . \]

From equation (28) we obtain the \( k'(\hat{n}) \) and \( \alpha'(\hat{n}) \) in a form similar to the Abbott (1982) calculations for OB stars. We calculate the left hand side of equation (28) varying the \( t \) parameter from \( 10^{-1} \) to \( 10^{-7} \), using the line opacity \( \kappa_L \) calculated in the form described in the previous section for each line, and using the disk emission described by equations (6)-(7) to calculate the intensities. From these values, the parameters \( k'(\hat{n}) \) and \( \alpha'(\hat{n}) \) are obtained through linear regression by varying the \( t \) parameter over two order of magnitudes at a time within the fore mentioned interval, and taking the highest values found for each parameter. We note here that the selection of the highest values within intervals of two orders magnitudes is somewhat arbitrary. To our knowledge this is the first attempt to include the spatial and time dependence of the line radiation force parameters coupled consistently with the hydrodynamics of accretion disk winds, and we believe that the process includes much of the physics involved in line driving from a distributed radiation source: line-scattering, photon momentum generating force on gas, dilution factor, line optical depth in a moving
media, line-opacity distribution, energy distribution in spectrum, and ion populations. This approach allows us to explore the effect of variable ion populations on the disk wind rather than assuming a constant ionization equilibrium as we did in Paper 2. In future work we shall develop a more accurate treatment for the line radiation force parameters, including a systematic determination of the appropriate intervals in $t$ in which to derive the line force parameters, as well as a study of the directional dependence of these parameters, rather than assume them isotropic as we do in this work (see equation [30]).

From equation (25) and equation (28), we have:

$$\tilde{f}_{\text{rad}} \approx \oint \left[ \frac{\sigma \int_0^\infty \tilde{I} \tilde{n} d\nu}{c} \tilde{k}'(\tilde{n}) \tilde{t}^{-\alpha'(\tilde{n})} \right] \tilde{n} d\Omega. \quad (29)$$

As mentioned above, in this work we use values of the force multiplier parameters $k$ and $\alpha$ which vary in time and space but are independent of direction. As we see below this will allow us to implement the numerical integrations on intensity $I(\tilde{n})$ at each spatial point of the computational grid before implementing the hydrodynamic calculations rather than during the implementation of the hydrodynamic calculations, thus maintaining the computations manageable.

The values of $k$ and $\alpha$ used in this work are calculated through the expression:

$$k \tilde{t}^{-\alpha} \approx \frac{\oint \left[ \int_0^\infty \tilde{I} \tilde{n} d\nu \tilde{k}' \tilde{n} t^{-\alpha'(\tilde{n})} \right] \tilde{n} d\Omega}{\oint \left[ \int_0^\infty \tilde{I} \tilde{n} d\nu \right] \tilde{n} d\Omega}. \quad (30)$$

We calculate the right hand side of equation (30) varying the $t$ parameter from $10^{-1}$ to $10^{-7}$, using the values of $k'(\tilde{n})$ and $\alpha'(\tilde{n})$ calculated through equation (28) and using the disk emission described by equations (6)-(7) to calculate the intensities. From these values, the parameters $k$ and $\alpha$ are obtained through linear regression. We note here that the angle averaging is done in an ad hoc manner in order to reduce computational complexity. As we indicated above, we believe that this approach includes much of the physics of line driving within an accretion disk wind. In future work, we shall develop a more systematic treatment of the line radiation force parameters that will include a study of the directional dependence of these parameters, rather than assume averaged angle values as we do here.

With these values of $k$ and $\alpha$, we approximate the line radiation force by:

$$\tilde{f}_{\text{rad}} \approx \oint \left[ \frac{\sigma \int_0^\infty \tilde{I} \tilde{n} d\nu}{c} k \tilde{t}^{-\alpha} \right] \tilde{n} d\Omega. \quad (31)$$
Therefore, from equation (27):

\[
\tilde{f}_{\text{rad}} = \int \left[ \frac{\sigma}{c} \int_{0}^{\infty} I(\hat{n})d\nu \frac{k}{\kappa_{L}(\hat{n})} \left( \frac{\sigma}{c} \tau_{L}(\hat{n}) \right)^{-\alpha} \right] \hat{n} d\Omega .
\]  

(32)

Substituting equation (23):

\[
\tilde{f}_{\text{rad}} = \int \left[ \frac{\sigma}{c} \int_{0}^{\infty} I(\hat{n})d\nu \frac{k}{\rho \sigma v_{th}} \left( \frac{1}{\rho \sigma v_{th}} \left| \hat{n} \cdot \hat{z} \frac{dv_{z}}{dz} \right| \right)^{\alpha} \right] \hat{n} d\Omega .
\]  

(33)

Thus:

\[
\tilde{f}_{\text{rad}} = \frac{\sigma}{c} k \left( \frac{1}{\rho \sigma v_{th}} \left| \frac{dv_{z}}{dz} \right| \right)^{\alpha} \int \left[ \hat{n} \cdot \hat{z} \int_{0}^{\infty} I(\hat{n})d\nu \right] \hat{n} d\Omega .
\]  

(34)

We wish to note that the \( k \) and \( \alpha \) parameters in the above equation depend on the line opacity distribution (equations [26]-[30]), which in turn depends on density and temperature (equations [15]-[18]). Since the density and temperature will vary in space and time, the \( k \) and \( \alpha \) parameters will also depend on space and time. Also, we wish to note here that in this work we assume azimuthal symmetry and thus have only two independent spatial coordinates \( \text{"r"} \) and \( \text{"z"} \).

In equation (34) we substitute the \( \alpha \) parameter inside the integral by a fiducial value of 0.7, which is the value we assumed in our previous models presented in Paper 1 and Paper 2. Varying the number density from \( 10^{6} \text{ cm}^{-3} \) to \( 10^{10} \text{ cm}^{-3} \) at spatial points throughout our computational grid, and applying the values of disk luminosity \( L_{\text{disk}} = L_{\odot} \) and white dwarf radii of \( R_{wd} = 0.01R_{\odot} \) which we use throughout this work, by the way of equation (30) we find values for the \( \alpha \) parameter which vary from 0.55 to 0.85. We do not expect that the application of the fiducial value for \( \alpha \) inside the integral of equation (34) will produce a significant difference in the density and velocity wind structures, and further it will allow the evaluation of the integral at all spatial grid points before solving the hydrodynamic equations described in §6, maintaining the computations manageable. Thus,

\[
\tilde{f}_{\text{rad}} = \frac{\sigma}{c} k(r, z, t) \left( \frac{1}{\rho \sigma v_{th}} \left| \frac{dv_{z}}{dz} \right| \right)^{\alpha(r, z, t)} \int \left[ \hat{n} \cdot \hat{z} \int_{0}^{\infty} I(\hat{n})d\nu \right] \hat{n} d\Omega .
\]  

(35)

We wish to also note that although equation (35) takes into account the line radiation pressure in the \( \text{"r"} \) direction, we have included only the derivative in the \( \text{"z"} \) direction of the \( v_{z} \) component. As we found in Paper 2, the accretion disk winds in CVs tend to flow in the direction perpendicular to the disk, particularly in the region near the surface of the disk, thus justifying the assumption that the derivatives of the \( v_{r} \) component are negligible. In this
work we also assume negligible the radial derivatives of the "$v_z$" component and the vertical and radial derivatives of the "$v_\phi$" component in the calculation of the line radiation force. We note here that the disk wind streamlines are "helical" in nature; the wind flow starts out at the base of the wind with a non-zero "$v_\phi$" component due to disk rotation. The "$v_\phi$" component of the velocity fields is calculated throughout our hydrodynamic calculations under the assumption of azimuthal symmetry (see Appendix). We note that even under azimuthal symmetry, line radiation force may have non-zero components along the the "$\phi$" direction; e.g., Gayley & Owocki (2000) for the case of OB stars, assuming azimuthal symmetry, showed that the $\phi$ component of the line radiation force, although presenting modest modifications in the overall wind dynamics, could lead to observable effects. Even though, on one hand, the inclusion of the additional terms in the velocity gradient for the line radiation pressure in the accretion disk wind may possibly produce interesting results, on the other we do not believe that it will significantly affect the overall results currently being implemented. In future work we shall include the effects of the derivatives along both the "$z$" and "$r$" directions for the different velocity components in the line radiation force, rather than assume "$dv_z/dz$" as the dominant term as we have done in this work and in Paper 1 and Paper 2.

Defining $\vec{S}(r, z)$:

$$\vec{S}(r, z) = \int \left[ |\vec{n} \cdot \vec{z}|^{0.7} \int_0^\infty I(\nu) d\nu \right] \vec{n} d\Omega . \quad (36)$$

Taking the source of radiation to be the accretion disk, we have:

$$S_z(r, z) = \int_{r_o}^{r} \int_{0}^{2\pi} \frac{Q(r')}{\pi} \frac{z^{2.7}}{[(r^2 + r'^2 + z^2 - 2rr' \cos \phi)^{1/2}]^{4.7}} r'd\phi dr' \quad (37)$$

and

$$S_r(r, z) = \int_{r_o}^{r} \int_{0}^{2\pi} \frac{Q(r')}{\pi} \frac{z^{1.7}(r - r' \cos \phi)}{[(r^2 + r'^2 + z^2 - 2rr' \cos \phi)^{1/2}]^{4.7}} r'd\phi dr' \quad (38)$$

where $S_z$ and $S_r$ are the corresponding components of the vector $\vec{S}$ defined in equation (36) (the $S_\phi$ component is zero due to the axial symmetry of the accretion disk) and $Q(r')$ is the radiation emission per area of the disk calculated through equation (6).

Thus we have

$$\vec{f}_{rad} = \frac{\sigma}{c} k(r, z, t) \left( \frac{1}{\rho \sigma \mathcal{v}_{th}} \frac{dv_z}{dz} \right)^{a(r, z, t)} \left[ S_z(r, z) \hat{z} + S_r(r, z) \hat{r} \right] \quad (39)$$

where $S_z$ and $S_r$ are given by equations (37) and (38).
We also account for the fact that, as discussed by Castor, Abbott, & Klein (1975) for OB star winds, if the velocity gradient increases to sufficiently high values, or the density of the wind decreases to sufficiently low values, the contribution for the radiation pressure due to lines arrives at a maximum value. Similar to the case of OB stars (Abbott 1982), we found that the maximum value of the line radiation pressure was obtained when \((1/\rho \sigma v_{th}) \, dv_z/dz \lesssim 10^7\). In this work we have assumed that the maximum possible value of the line radiation pressure is obtained when \((1/\rho \sigma v_{th}) \, dv_z/dz = 10^7\) (rather than \(10^8\) as we did in Paper 2).

Therefore the expression for the total line radiation force per mass for disk winds which we adopt is

\[
\vec{F}_{rad} = \frac{\sigma}{c} \, k(r,z,t) \left( \max \left[ \frac{1}{\rho \sigma v_{th}} \left| \frac{dv_z}{dz} \right| , \, 10^7 \right] \right)^{\alpha(r,z,t)} \left[ S_z(r,z) \hat{z} + S_r(r,z) \hat{r} \right]. \tag{40}
\]

In order to calculate the \(k(r,z,t)\) and \(\alpha(r,z,t)\) functions self consistently throughout the hydrodynamic calculations described below and simultaneously keep the computation manageable the numerical code was written such that the spatial distribution of the \(k\) and \(\alpha\) are calculated for values of number density varying from \(10^6\, \text{cm}^{-3}\) to \(10^{10}\, \text{cm}^{-3}\) at each computational spatial grid point. A fiducial temperature is taken for these calculations, since as we find in the models presented here, in inner disk region where the line radiation force is most crucial, the temperature does not change significantly due to radiative heating and cooling. During the hydrodynamic calculations, the actual values of \(k\) and \(\alpha\) are obtained through geometric interpolation from the above values and the current value of density at each computational grid point.

For the continuum radiation pressure the total radiation flux is calculated throughout the disk wind:

\[
\vec{F} = \oint \left[ \int_0^\infty I(\hat{n}) d\nu \right] \hat{n} d\Omega. \tag{41}
\]

Taking the source of radiation to be the accretion disk, we have

\[
F_z(r,z) = \int_{r_o}^{\infty} \int_0^{2\pi} Q(r') \frac{z^2}{\pi \left[ (r^2 + r'^2 + z^2 - 2rr' \cos \phi)^{1/2} \right]^4} r' d\phi dr' \tag{42}
\]

and

\[
F_r(r,z) = \int_{r_o}^{\infty} \int_0^{2\pi} Q(r') \frac{z(r - r' \cos \phi)}{\pi \left[ (r^2 + r'^2 + z^2 - 2rr' \cos \phi)^{1/2} \right]^4} r' d\phi dr' \tag{43}
\]

where \(F_z\) and \(F_r\) are the corresponding components of the radiation flux vector \(\vec{F}\) originating from the disk (the \(F_\phi\) component is zero due to the axial symmetry of the accretion disk) and \(Q(r')\) is the radiation emission per area of the disk calculated through equation (6).
5. Radiative Heating and Cooling

Radiative heating and cooling are computed in our model assuming an optically thin disk spectrum. A local balance between heating and cooling is assumed, subject to the constraint of particle number conservation for each element. The ionization processes included in the calculation are photoionization, charge transfer ionization, and collisional ionization. Recombination processes include radiative and dielectronic recombination and charge transfer. The heating terms include photoionization heating, Compton heating, charge transfer, and collisional de-excitation. Cooling terms include radiative and dielectronic recombination, bremsstrahlung, collisional ionization, collision excitation of bound levels, and (endothermic) charge transfer. Details of the radiative heating and cooling calculations are described in detail by Kallman & McCray (1982).

Disk models have succeeded in accounting for the observed continuum spectrum in many CVs (e.g. Herter et al. 1979; Kiplinger 1979, 1980; Bath, Pringle, & Whelan 1980; Mayo, Wickramasinghe, & Whelan 1980; Krautter et al. 1981; Hassall 1985; Wade 1988; la Dous 1989; Diaz, Wade, & Hubeny 1996; Wade & Hubeny 1998). The form of the spectrum applied in this work for the radiative heating and cooling calculations is obtained by integrating contributions over the disk surface calculated from equation (6), assuming local blackbody emission, and viewing the disk at infinity. In Figure 1 we show the disk spectrum used for the radiative heating and cooling calculations. We note that an assumption made in the radiative cooling and heating calculations is that the form of the spectrum is position independent, and thus the rates calculated here will be more accurate higher above the disk. In the future we will introduce more accurate heating and cooling rates into our models.

In Figure 2 and Figure 3 the radiative heating and cooling are shown respectively as a function of temperature for different values of the ionization parameter \( \xi \) defined as:

\[
\xi \equiv \frac{4\pi|\vec{F}|}{n}
\]  

(44)

where \( F \) is the radiation flux and \( n \) the number density.

From Paper 2 we found that the wind temperature of CV winds range in values of up to \( \sim 40,000 \) K. Thus in our work here we have approximated the heating and cooling rates the results presented in Figure 2 and Figure 3 by analytical expressions that agree with the detailed calculation within 20% for the heating rates and within 30% for the cooling rates for temperatures of up to 50,000 K.

For the radiative heating rate we implemented the following expression (in units of
erg cm$^3$ s$^{-1}$):

$$\Gamma = 1.6 \times 10^{-21} T^{-1/2} \left(1 - \frac{T}{1.3 \times 10^5}\right) \quad (45)$$

where $T$ is the absolute temperature, valid for temperatures of up to 50,000 K.

For the radiative cooling rate we implemented the following expression (in units of erg cm$^3$ s$^{-1}$):

$$\Lambda = 1.9 \times 10^{-29} T^{3/2} \quad (46)$$

where $T$ is the absolute temperature, valid for temperatures of up to 50,000 K.

6. Hydrodynamic Model

Our hydrodynamic model uses the Piece-Wise Parabolic Method (PPM) numerical scheme (Colella & Woodward 1984). We use the 2.5-dimensional hydrodynamic equations of the wind in cylindrical coordinates; i.e., the three-dimensional hydrodynamic equations are reduced to two-dimensional equations by assuming that the derivative of any physical variable with respect to $\phi$ is zero. The origin of the coordinate system is located at the center of the accretion disk and the “$z=0$” plane is located to coincide with the accretion disk midplane. The hydrodynamic equations are presented in the Appendix.

In this treatment we have implemented the energy equation self consistently. In particular, the adiabatic heating and cooling effects are implemented through the first and second term on the right hand side of equation (A6), and the radiative heating and cooling rates are implemented through the last term on the right hand side of equation (A6).

As discussed in section 4, our treatment of the line radiation pressure assumes negligible the $\phi$ component of the line radiation force, and therefore the specific angular momentum is conserved within our models. We note that strictly, the azimuthal component of the line radiation force is not required to be zero, and thus the angular momentum is not necessarily conserved, but this is likely a small correction.

As we discovered in Paper 1 and Paper 2, care must be taken with the boundary conditions to avoid numerical instabilities. In this work we treat the boundary conditions in a form equivalent to that discussed in Paper 2. Our spatial grids are also equivalent to those explored and discussed in Paper 2.

In the models presented here we solve the hydrodynamic equations over a range of radii from 0.02$R_\odot$ ($2R_{wd}$ in our models) to 1.5$R_\odot$. From equation (6) it is found that the energy emission per area $Q$ will increase slightly as radius decreases from $2R_{wd}$ down to $\approx 1.36R_{wd}$
and will decrease strongly as radius decreases from \( \approx 1.36R_{\text{wd}} \) down to the white dwarf radii \( (R_{\text{wd}}) \). In Paper 1 we showed that the wind density tends to decrease with decreasing radiation flux. Thus the mass loss rate for radii less that \( 2R_{\text{wd}} \) will not alter significantly the total mass loss rate of the wind. Also, in Paper 2, we presented models with spatial grids with “r” down to \( R_{\text{wd}} \) and found essentially the same results with models with “r” down to \( 2R_{\text{wd}} \) with model parameters otherwise identical.

7. Results

In Table 1 we present the wind mass loss rates from our previous models and for the models presented here. The second column indicates the dimension of the model, 2.5D are the full 3D hydrodynamic equations under azimuthal symmetry; i.e. the derivatives with respect to the azimuthal angle are assumed zero. 2.5D models allow a consistent treatment of the 3D equations (under azimuthal symmetry) while mathematically having only two independent spatial directions, keeping the calculations more manageable. The third column indicates the radial disk structure assumed. In all models a steady disk is assumed. An “I” indicates an isothermal disk (no radial dependence). An “S” indicates the radial dependence of disk radiation emission and temperature of a standard Shakura-Sunyaev disk. The third and fourth columns indicate the values of the \( k \) and \( \alpha \) parameters used in each model. In our previous models (A-F) we had assumed constant ionization equilibrium throughout the wind, and therefore constant values for these two parameters. In our current work, as described above, we implement the spatial dependence (Model G) and the spatial and time dependence (Model H) of these two parameters and find values that vary throughout our spatial grids (and in time for Model H) within the intervals indicated in Table 1.

In implementing local ionization equilibrium in our models, we first run models that include the spatial dependence of the radiation field above the disk but assume a fiducial number density of \( 10^8 \text{ cm}^{-3} \) (Model G). From this we obtain the values of the “\( k \)” and “\( \alpha \)” line radiation parameters for each point of the computational grid. Results from these runs are presented in Figure 5. The values of \( k \) we found varied from 0.03 to 0.5 and values of \( \alpha \) varying from 0.6 to 0.8. The higher values of both \( k \) and \( \alpha \) are obtained in the lower inner region of the wind (lower left hand side of Figure 5). The lower values of both \( k \) and \( \alpha \) are obtained in the lower outer region of the wind (lower right hand side of Figure 5). At \( z = R_{\odot} \), the \( k \) parameter was found to vary from 0.16 to 0.26 and the \( \alpha \) parameter was found to vary from 0.66 to 0.70. In this model we find similar terminal velocities with respect to the models presented in Paper 2, but densities values increased by a factor of 2. We find steady wind flows coming from the disk. Wind-mass loss rates calculated in this work are
obtained by integrating the mass flux at the start of the wind, at the lower boundary of the spatial computational grid. The total wind mass loss rate we find for this model is $2 \times 10^{-11} \text{M}_\odot \text{yr}^{-1}$. This increase in the wind mass loss rate is due to the increase of the $k$ in the lower inner region where the radiation flux is stronger.

In order to calculate the $k(r, z, t)$ and $\alpha(r, z, t)$ functions self consistently throughout the hydrodynamic calculations, as we described in §5, the spatial distributions of the $k$ and $\alpha$ are calculated in a similar manner as in the model presented in Figure 5, but now for values of number density varying from $10^6$ cm$^{-3}$ to $10^{10}$ cm$^{-3}$ at each computational spatial grid point (Model H). A fiducial electron temperature of 30,000 K is taken for these calculations. During the hydrodynamic calculations, the actual values of $k$ and $\alpha$ are obtained through geometric interpolation from the above values and the current value of density at each computational spatial grid point. Results from these models are presented in Figure 6. For the above range of densities at each spatial grid point, we find values of $k$ varying from 0.03 to 0.6 and values of $\alpha$ varying from 0.55 to 0.85. Again we find steady wind flows coming from the disk. In the lower inner region, due to the increase of density the $k$ parameter drops by a factor of $\sim 2$, producing in turn a decrease of total wind mass rate. The wind mass loss rate for this model is $4 \times 10^{-12} \text{M}_\odot \text{yr}^{-1}$. The velocity fields are very similar to the previous models, finding terminal velocities in the order of $\sim 3000$ km s$^{-1}$. We note that the mass loss rate is approximately a factor of two below the values we found in our earlier models in Paper 2. This difference is due to the detailed calculations of the line radiation force parameters, which when the local density values at the inner region are considered, we find slightly lower values of the $k$ line radiation force parameter.

In Figures 7 and 8 we present contour plots of the line radiation force parameter $k$ and $\alpha$ respectively, once the calculations arrive at a steady solution (Model H). These two figures illustrate the coupling between line force parameters, ionization equilibrium, and wind dynamics within an accretion disk wind. We note that, although the ionization structures are coupled with the hydrodynamics, within typical CV parameters ($M_{wd} = 0.6 \text{M}_\odot$; $R_{wd} = 0.01 \text{R}_\odot$; $L_{\text{disk}} = L_\odot$), in the higher wind density areas, the line force parameters do not change significantly; thus justifying the assumption of our earlier models of constant ionization equilibrium (and thus constant line force parameters). We also note that in QSOs/AGN, the presence of strong x-ray emission will generate strong changes in the ionization balance of the wind, and the assumption of constant ionization equilibrium in the wind will no longer hold (Murray et al. 1995; Hillier et al. 2002).

Studies of observed ultraviolet line profiles from CVs have estimated CV wind mass loss rates to be in the order of $10^{-12}$ to $10^{-11} \text{M}_\odot \text{yr}^{-1}$ and found CV wind terminal speeds in the order of $\sim 3000$ km s$^{-1}$ (e.g. Krautter et al. 1981; Córdova & Mason 1982; Greenstein
& Oke 1982; Mauche & Raymond 1987; Prinja & Rosen 1995; Friedjung, Selvelli, & Cassatella 1997) thus the models developed in this work finds values for wind mass loss rates and terminal speeds consistent with observations.

In the models presented in this work we also implement radiative heating and cooling. In Figure 10 we present a velocity field graph superimposed with temperature contours for the local ionization equilibrium disk wind model. Comparing with the results from Paper 2 (Figure 9), we find that radiative heating and cooling tends to maintain the wind temperature in the higher density regions near the disk, rather than cooling due to adiabatic expansion as we had found in our earlier models of Paper 2. Therefore the radiative heating and cooling processes are playing an important role in the temperature structure of the wind. We are finding higher overall temperatures than in Paper 2 where we neglected radiative heating and cooling processes and assumed only adiabatic heating cooling processes.

As a consistency check, in Figure 11 we present the results of models with a computational spatial grid that starts at $r = R_{wd}$ (rather than $r = 2.0R_{wd}$ as in the other models discussed previously in this work). In Figure 12 we present results from models with a computational spatial grid starting at $r = R_{wd}$ and with an initial velocity at the base of the wind of $1\,\text{km}\,\text{s}^{-1}$ (rather than $10\,\text{km}\,\text{s}^{-1}$ as in the other models discussed previously in this work). In both cases we find similar overall results: a steady biconical wind velocity/density structure, with similar velocity and density values. We note that these results although similar, are not identical to those of Figure 6, and thus represent numerical effects since the physical parameters have remained identical. However the deviations from Figure 6 are considerably smaller than the changes of results we have found in earlier work when we physical parameters have been modified as our models have developed (Paper 2), thus we are confident in our overall results. In future work we shall study these numerical effects in greater detail; a precise knowledge of these model limitations may be important to achieve precise comparisons with observations.

As we had found in our earlier models of Paper 1 and Paper 2, rotational forces are important in the study of winds from accretion disks. They cause the velocity streamlines to collide which results in an enhanced density region. In this region the wind speed is reduced and the wind density is increased. The increase in density caused by the collision of streamlines is important because it permits the appearance of blue-shifted absorption lines as observed in P Cygni profiles of low-inclination CVs.
8. Summary and Conclusions

We have developed a 2.5-dimensional hydrodynamic line-driven accretion disk wind model. Our model solves a complete set of adiabatic hydrodynamic partial differential equations, using the PPM numerical scheme and implementing the radial temperature and radiation emission distributions on the surface of an accretion disk. Our models calculate the line radiation force parameters throughout the wind at each computational grid point for each time step through the calculation of line opacities from atomic data, similar to the calculations presented by Abbott (1982) for OB stars. We treat the hydrodynamic equation of energy self consistently including radiative heating and cooling as well as adiabatic expansion and compression.

We find steady wind flows coming from the disk with similar density and velocity structures as our earlier models of Paper 2 in which we had not yet included radiative heating and cooling and in which we had assumed constant ionization equilibrium (therefore constant values for the line radiation force parameters). The steady nature of our solution contrasts with the strong fluctuations in density and velocity found by Proga, Stone, & Drew (1998) for CV winds for physical parameters similar to the ones we used here. A possibility that could account for the difference in results from our models and those of Proga, Stone, & Drew (1998) is the treatment of the lower boundary conditions. In future work we shall explore this possibility in detail.

We note that as our numerical models evolve towards more realistic ones, it may result that a more accurate treatment of the line radiation force (which would include line-overlapping, rather than assuming the Sobolev approximation for all lines) or a more accurate model of the accretion disk (which may result in an unsteady picture of the accretion disk rather than the standard Shakura-Sunyaev disk) may lead to physical instabilities. In our systematic approach to the accretion disk wind problem, we started with an analytic 1D model, which although being our "crudest" one, did allow for an analytic solution which has proven to be invaluable as a test case for our numerical algorithms. From this initial model we have included, on a step by step basis (Paper 1, Pereyra 1997, Paper 2) elements such as a more accurate treatment of the line radiation force (in which we have always applied the Sobolev approximation), radial structure of the accretion disk, adiabatic heating and cooling processes, etc. This approach has allowed us to establish clearly a relationship between the elements we have introduced (both of numerical and physical nature) and our results, as our models have developed into more realistic ones. In this sense we are confident that if intrinsic physical instabilities should appear as we continue our work, we will be able to establish their physical origin.

From our models we calculate wind mass-loss rates and terminal velocities. For typical
cataclysmic variable parameter values of disk luminosity $L_{\text{disk}} = L_{\odot}$, white dwarf mass $M_{\text{wd}} = 0.6M_{\odot}$, and white dwarf radii $R_{\text{wd}} = 0.01R_{\odot}$, we obtain a wind mass-loss rate of $\dot{M}_{\text{wind}} = 4 \times 10^{-12}M_{\odot}\,\text{yr}^{-1}$, and a terminal velocity of $\sim 3000\,\text{km}\,\text{s}^{-1}$. We note that the mass loss rate is approximately a factor of two below the values we found in our earlier models in Paper 2. This difference is due to the detailed calculations of the line radiation force parameters, which when the local density values at the inner region are considered, we find slightly lower values of the $k$ line radiation force parameter.

The results in this work suggest that the details of the ionization equilibrium in CV disk winds, within reasonable parameters, may not have considerable effect over the velocity fields of the wind nor in the wind mass distribution. Although these details have to be taken into account in order to derive an accurate theoretical value of the wind mass loss rate as illustrated by the difference by a factor of two between the models presented here and the earlier ones of Paper 2. The similar wind mass distribution and velocity fields found here with respect to those of Paper 2, would indicate a similar inclination angle dependence of the C IV 1550 Å line. But the decrease in total wind mass loss rate would generate weaker line features. In QSOs, where the ionization balance of the gas material may change significantly, the coupling between the ion populations and the radiative hydrodynamics will have an important effects in the overall wind dynamics; thus a model capable of representing this coupling becomes necessary.

A shortcoming of our models is that, at each spatial point for each time step we assume direction-independent values for the line radiation parameters and we also assume position independent values for the radiative heating and cooling parameters. In future work we plan to include these effects. We also plan to extend our disk wind models to low mass X-ray binaries and QSOs/AGN, where the local ionization equilibrium will play a more crucial role in the overall dynamics.

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A. Hydrodynamic Equations

The hydrodynamic equations implemented in the models presented are, the equation of state:

$$P = (\gamma - 1)\rho e \quad (A1)$$
the mass conservation equation:

\[
\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial (r \rho v_r)}{\partial r} + \frac{\partial (\rho v_z)}{\partial z} = 0
\]  

(A2)

the momentum conservation equations:

\[
\rho \frac{\partial v_r}{\partial t} + \rho v_r \frac{\partial v_r}{\partial r} - \rho \frac{v_\phi^2}{r} + \rho v_z \frac{\partial v_r}{\partial z} =
\]

\[
- \rho \frac{GM_{wd}}{(r^2 + z^2)} \frac{r}{(r^2 + z^2)^{1/2}} \frac{\partial P}{\partial r} + \rho \frac{\sigma F_r(r, z)}{c} + \rho S_r(r, z) k(r, z, t) \left( \max \left[ \frac{1}{\rho \sigma v_{th}} \left| \frac{dv_z}{dz} \right| , 10^7 \right] \right) ^{\alpha(r,z,t)}
\]

(A3)

\[
\rho \frac{\partial v_\phi}{\partial t} + \rho v_r \frac{\partial v_\phi}{\partial r} + \rho v_z \frac{\partial v_\phi}{\partial z} = 0
\]  

(A4)

\[
\rho \frac{\partial v_z}{\partial t} + \rho v_r \frac{\partial v_z}{\partial r} + \rho v_z \frac{\partial v_z}{\partial z} =
\]

\[
- \rho \frac{GM_{wd}}{(r^2 + z^2)} \frac{z}{(r^2 + z^2)^{1/2}} \frac{\partial P}{\partial z} + \rho \frac{\sigma F_z(r, z)}{c} + \rho S_z(r, z) k(r, z, t) \left( \max \left[ \frac{1}{\rho \sigma v_{th}} \left| \frac{dv_z}{dz} \right| , 10^7 \right] \right) ^{\alpha(r,z,t)}
\]

(A5)

and the energy conservation equation:

\[
\frac{\partial \rho E}{\partial t} + \frac{1}{r} \frac{\partial r \rho E v_r}{\partial r} + \frac{\partial \rho E v_z}{\partial z} =
\]

\[
- \frac{1}{r} \frac{\partial r P v_r}{\partial r} - \frac{\partial P v_z}{\partial z}
\]

\[
- \rho \frac{GM_{wd}}{(r^2 + z^2)} \frac{r}{(r^2 + z^2)^{1/2}} v_r + \rho \frac{\sigma F_r(r, z)}{c} v_r + \rho S_r(r, z) k(r, z, t) \left( \max \left[ \frac{1}{\rho \sigma v_{th}} \left| \frac{dv_z}{dz} \right| , 10^7 \right] \right) ^{\alpha(r,z,t)} v_r
\]

(A6)

\[
- \rho \frac{GM_{wd}}{(r^2 + z^2)} \frac{z}{(r^2 + z^2)^{1/2}} v_z + \rho \frac{\sigma F_z(r, z)}{c} v_z
\]
$+ \rho \frac{\sigma S_z(r, z)}{c} k(r, z, t) \left( \max \left[ \frac{1}{\rho \sigma v_{th}} \left| \frac{dv_z}{dz} \right|, 10^7 \right] \right)^{\alpha(r, z, t)} v_z$

$+ n^2 (\Gamma(T) - \Lambda(T))$

where $P$ is the pressure, $\gamma$ is the ratio of specific heats, $\rho$ is the density, $e$ is the internal energy per mass, $v_r$, $v_\phi$, and $v_z$ are the corresponding velocity components in cylindrical coordinates, $G$ is the gravitational constant, $M_{wd}$ is the mass of the white dwarf, $\sigma$ is the Thomson cross section per unit mass, $F_r$ and $F_z$ are the corresponding radiation flux components (see equations [42] and [43]), $c$ is the speed of light, $v_{th}$ is the thermal velocity, and $k$ and $\alpha$ are the line force multiplier parameters calculated through equation (30). $S_r$ and $S_z$ are defined through equations (38) and (37) respectively, $E = \frac{v_r^2}{2} + \frac{v_\phi^2}{2} + \frac{v_z^2}{2} + e$ is the total energy per mass, $n$ is the electron number density, $\Gamma$ is the radiative heating rate, and $\Lambda$ is the radiative cooling rate.
Table 1. CV Accretion Disk Wind Mass-Loss Rates for Different Models

<table>
<thead>
<tr>
<th>Model</th>
<th>Dim</th>
<th>Disk</th>
<th>$k$</th>
<th>$\alpha$</th>
<th>Comments</th>
<th>$M(M_\odot , yr^{-1})$</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>A</td>
<td>1</td>
<td>I</td>
<td>1/30</td>
<td>0.7</td>
<td>Isothermal Wind</td>
<td>$2 \times 10^{-14}$</td>
<td>Paper 1</td>
</tr>
<tr>
<td>B</td>
<td>2.5</td>
<td>I</td>
<td>1/30</td>
<td>0.7</td>
<td>Model A extended to 2.5D; radiation pressure in “r” neglected</td>
<td>$2 \times 10^{-14}$</td>
<td>Paper 1</td>
</tr>
<tr>
<td>C</td>
<td>2.5</td>
<td>I</td>
<td>1/3</td>
<td>0.7</td>
<td>Model B with an increased value of $k$</td>
<td>$6 \times 10^{-14}$</td>
<td>Paper 2</td>
</tr>
<tr>
<td>D</td>
<td>2.5</td>
<td>I</td>
<td>1/3</td>
<td>0.7</td>
<td>Model C with a maximum cutoff value for the line pressure implemented</td>
<td>$2 \times 10^{-13}$</td>
<td>Paper 2</td>
</tr>
<tr>
<td>E</td>
<td>2.5</td>
<td>I</td>
<td>1/3</td>
<td>0.7</td>
<td>Model D with an adiabatic wind (rather than an isothermal wind)</td>
<td>$2 \times 10^{-13}$</td>
<td>Paper 2</td>
</tr>
<tr>
<td>F</td>
<td>2.5</td>
<td>S</td>
<td>1/3</td>
<td>0.7</td>
<td>Model E with a standard Shakura-Sunyaev disk (rather than isothermal disk); radiation pressure in “r” included</td>
<td>$8 \times 10^{-12}$</td>
<td>Paper 2</td>
</tr>
<tr>
<td>G</td>
<td>2.5</td>
<td>S</td>
<td>0.03-0.5</td>
<td>0.6-0.8</td>
<td>Model F with spatial dependence of $k$ and $\alpha$ derived from the spatial distribution of radiation field but assuming a fiducial number density of $10^6 , \text{cm}^{-3}$</td>
<td>$2 \times 10^{-11}$</td>
<td>current work</td>
</tr>
<tr>
<td>H</td>
<td>2.5</td>
<td>S</td>
<td>0.03-0.6</td>
<td>0.55-0.85</td>
<td>Model F with spatial and time dependence of $k$ and $\alpha$ derived from the spatial distribution of radiation and the spatial and time distribution of mass density</td>
<td>$4 \times 10^{-12}$</td>
<td>current work</td>
</tr>
</tbody>
</table>
REFERENCES

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This preprint was prepared with the AAS L\TeX macros v5.0.
Fig. 1.— Logarithm of radiation flux vs logarithm of frequency in units of Hz for the accretion disk used in this work. This is the spectrum distribution used for the radiative heating and cooling calculations. The physical parameters used here are $L_{\text{disk}} = L_\odot$ and $R_{\text{wd}} = 0.01R_\odot$. 
Fig. 2.— Logarithm of the radiative heating rate in units of erg cm$^3$ s$^{-1}$ vs the logarithm of the temperature in units of 10$^4$ K. The ionization parameters used are log $\xi = 5.0, 2.3, 0.78$. 

\[^{0}I_{2}3_{4}I_{L}J_{'}I_{'}"]\
Fig. 3.— Logarithm of the radiative cooling rate in units of erg cm$^3$ s$^{-1}$ vs the logarithm of the temperature in units of 10$^4$ K. The ionization parameters used are log $\xi = 5.0, 2.3, 0.78$. 

(log $\xi = 5$
log $\xi = 0.78$)
Fig. 4.— Vector field graph of wind velocity superimposed with density contours for the model assuming constant ionization equilibrium (Model F [Paper 2]). The line radiation force parameters applied are $k = 0.3$, $\alpha = 0.7$. The primary star is at the origin of the graph, and the disk is over the horizontal axis. The contour levels vary uniformly from a value of $3.6 \times 10^{-16}$ g cm$^{-3}$ down to a value of $0.1 \times 10^{-16}$ g cm$^{-3}$. The physical parameters here used are $M_{wd} = 0.6 M_\odot$, $R_{wd} = 0.01 R_\odot$, and $L_{disk} = L_\odot$. 
Fig. 5.— Vector field graph of wind velocity superimposed with density contours for the model assuming an ionization equilibrium varying in space but constant in time. A fiducial number density of $10^8 \text{ cm}^{-3}$ is used for the calculations of the line radiation force parameters (Model G). Parameters are similar to those of Figure 4.
Fig. 6.— Vector field graph of wind velocity superimposed with density contours for the model applying an ionization equilibrium varying in space and time. The current density is applied at each spatial grid point at each time step in the calculation of the line radiation force parameters (Model H). Parameters are similar to those of Figure 4.
Fig. 7.— Contour plot of the line radiation force parameter $k$ in the Model H once it arrives at a steady solution. The physical parameters used are those of Figure 4.
Fig. 8.— Contour plot of the line radiation force parameter $\alpha$ in the Model H once it arrives at a steady solution. The physical parameters used are those of Figure 4.
Fig. 9.— Vector field graph of wind velocity superimposed with temperature contours for the model assuming constant ionization equilibrium and without radiative heating and cooling (Model F [Paper 2]). The contour levels vary uniformly from a value of 22,000 K down to a value of 1,000 K. Parameters are similar to those of Figure 4.
Fig. 10.— Vector field graph of wind velocity superimposed with temperature contours for the model applying local ionization equilibrium and including radiative heating and cooling (Model H). Parameters are similar to those of Figure 9.
Fig. 11.— Vector field graph of wind velocity superimposed with density contours for the model applying local ionization equilibrium varying in space and time. The computational grid starts at $r = R_{wd}$, rather than $r = 2R_{wd}$ as in the results presented in Figure 6. Parameters are similar to those of Figure 4.
Fig. 12.— Vector field graph of wind velocity superimposed with density contours for model disk wind applying local ionization equilibrium varying in space and time. The computational grid starts at $r = R_{wd}$, rather than $r = 2R_{wd}$ as in the results presented in Figure 6. The initial velocity set at the base of the wind is 1 km s$^{-1}$, rather than 10 km s$^{-1}$ as in the results presented in Figure 6. Parameters are similar to those of Figure 4.