International Space Station Carbon Dioxide Removal Assembly (ISS CDRA) Concepts and Advancements

Dina El Sherif
Honeywell International, Torrance CA 90504

James C. Knox
NASA Marshall Space Flight Center

ABSTRACT

An important aspect of air revitalization for life support in spacecraft is the removal of carbon dioxide from cabin air. Several types of carbon dioxide removal systems are in use in spacecraft life support. These systems rely on various removal techniques that employ different architectures and media for scrubbing CO₂, such as permeable membranes, liquid amine, adsorbents, and absorbents. Sorbent systems have been used since the first manned missions. The current state of key technology is the existing International Space Station (ISS) Carbon Dioxide Removal Assembly (CDRA), a system that selectively removes carbon dioxide from the cabin atmosphere. The CDRA system was launched aboard UF-2 in February 2001 and resides in the U.S. Destiny Laboratory module. During the past four years, the CDRA system has operated with varying degrees of success. There have been several approaches to troubleshooting the CDRA system aimed at developing work-around solutions that would minimize the impact on astronaut time required to implement interim solutions.

The paper discusses some of the short-term fixes applied to promote hardware life and restore functionality, as well as long-term plans and solutions for improving operability and reliability.

The CDRA is a critical piece of life support equipment in the air revitalization system of the ISS, and is demonstrated technology that may ultimately prove well-suited for use in lunar or Mars base, and Mars transit life support applications.

INTRODUCTION

The existing International Space Station (ISS) Carbon Dioxide Removal Assembly is part of the ISS air revitalization system, providing continuous CO₂ removal from the cabin atmosphere. CDRA is a regenerative system whose principal operation utilizes 4 beds. Each bed ORU contains a desiccant bed and a CO₂ sorbent bed—hence desiccant/adsorbent bed ORU. The system relies on one desiccant bed to condition the air prior to entry into the adsorbent bed. The adsorbent bed selectively removes the CO₂, and the air travels through the second desiccant adsorbent bed to replace the humidity.

The CDRA system is a water-save system in contrast to the 2-bed Skylab system, which vented adsorbed water overboard. The U.S. Skylab Program successfully demonstrated the use of zeolite molecular sieves in regenerative CO₂ removal by using a two-bed subsystem that performed for over 4100 hours without failure. (1).

While cabin air processing, one carbon dioxide removal bed is in the process of regeneration. Regeneration is accomplished using pressure/thermal swing methodology. First, the two-stage pump removes the free air from the adsorbent bed and returns it to the cabin, reducing oxygen ullage. Then Kapton heaters integrated within the adsorbent bed raise the zeolite temperature, and space vacuum creates a low, partial pressure driving the carbon dioxide gas overboard. Daylight and continuous day power cycle is overlapped with the operating cycle. In the day/night power cycle, the carbon dioxide adsorbent bed heaters are only allowed to be powered on during the day portion of the cycle.

In the current open-loop configuration, carbon dioxide is removed from the cabin and discharged overboard. The gases lost during venting must be replaced, and thus represent a consumable. By comparison, a closed-loop CDRA system could selectively remove carbon dioxide from the cabin air supply, and the concentrated CO₂ would be routed to a carbon dioxide reduction system, where the oxygen would be recovered, thereby reducing the consumables. This is an important aspect of long-term life support necessary to the success of lunar or Mars base or Mars Transit vehicle programs.
Two CDRA systems were produced for the ISS program. One CDRA system resides in the ISS U.S. Destiny Laboratory module. The second CDRA system is schedule for delivery for installation into Node 3. The ISS CDRA system supplements the Russian Vozdukh carbon dioxide removal system when more than three crewmembers are on board. On-board Lithium Hydroxide canisters supplement Vozdukh and CDRA CO₂ removal capabilities when needed. Figure 1 depicts the ISS flight CDRA.

The D/A bed ORU is a critical component of the CDRA system for removing carbon dioxide. There are two D/A bed ORU’s per CDRA system. Each of the ORU’s was verified via system level Protoflight testing. By performing the verification at an integrated level, individual ORU’s need not be tested. To support ORU-level Acceptance testing of the D/A bed spares, the program must develop ORU-level tests to use in lieu of the existing system-level CDRA tests. Figure 2 depicts the D/A bed ORU.

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The CDRA continuously removes 6 person-equivalents of CO₂ when operating with both CO₂ removal beds (dual beds) functioning. The minimum ISS carbon dioxide removal rate is based on the following equation for human equivalent unit (HEU) with the carbon dioxide partial pressure ranging from 2.0 to 3.9 mmHg:

\[ \text{Eq 1 HEU} = 1.723 \times (\text{pp CO}_2, \text{mmHg}) - 0.37975 \]

Where 1 HEU is approximately 1 kg CO₂/day

\[ \text{Eq 2 CO}_2 \text{ removal rate (lb/hr)} = 0.158 \times (\text{pp CO}_2, \text{mmHg}) - 0.035 \]

Each CDRA system includes 6 major orbital replacement units (ORU), including:

- Selector Valve ORU
- Desiccant / Adsorbent (D/A) Bed ORU
- Blower / Precooler ORU
- Two-Stage Pump ORU
- Heater Controller ORU
- Pump Fan Motor Controller (PFMC) ORU

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During the past four years, the ISS CDRA system has operated with varying degrees of success. There have been several approaches to troubleshooting the CDRA system aimed at developing interim solutions that minimize astronaut time required to implement interim operational solutions. Failure analysis of a returned flight D/A bed ORU revealed a failure of the desiccant and sorbent containment design. This seal failure allowed some zeolite particles to be circulated with the movement of process air. While the loss of some zeolite particles does not impact CDRA system CO₂ removal performance, the particulates did affect operations of some downstream components resulting in malfunctions of the air save pump, D/A bed check valve and selector valve. (2) A major D/A bed redesign was implemented to alleviate the containment problem, but the modification requires an extended period of time to implement. As a
result, several interim measures were adopted for on orbit operations to work through this extended redesign period.

The team devised an operational mode that allows continued operation that takes advantage of the system's redundant architecture. A single-bed operation workaround allows a ground controller to isolate a bed from space vacuum during any half-cycle in which that bed is not operating properly, such as when the check valve fails open. During single-bed operation, the system provides 3 person-equivalent removal capabilities. To date, this workaround has been implemented on several half-cycles during CDRA operations, however a majority of the time the CDRA has functioned with 100% capability, i.e., dual bed operation.

As a short-term hardware-based solution, the team decided to install in-line filters to capture any uncontained zeolite particulate material. In-line filters would extend the life of the selector valve ORU's and the two-stage air save pump. Combined filter testing and analysis resulted in an optimal filter design that met system specifications, i.e., flow and pressure drop(3). It also provided the program with an early system hardware protection feature. MSFC supported the development portion of the in-line filter by providing design data to Honeywell International, the manufacturer of the CDRA and filters. The filter design allowed installation without system modifications through placement of in-line filters in locations having relatively easy crew access. To date, astronauts have installed three 0.5-inch filters and three of the four 1.5-inch filters in the CDRA system while on orbit. Figure 3 presents a schematic of the CDRA.

![Figure 3. CDRA Schematic](image-url)
OVERALL REDESIGN APPROACH

In addition to operational workarounds and implementation of in-line filters to protect downstream components from sorbent particles, the long-term modification plan is to yield a solution that improves system operability and reliability. The re-design of the sorbent retainment system within the D/A bed (Figure 4) has been initiated, with plans to refurbish existing flight desiccant adsorbent bed hardware. The redesign and performance testing of the carbon dioxide removal assembly (CDRA) D/A bed ORU will be verified during Node 3 CDRA Performance Testing.

Figure 4. Modified Desiccant/Adsorbent Bed ORU Concept

The development of a new sorbent retainment design includes improvement of the static and dynamic seals and the addition of fixed screens beyond the dynamic seal as an added measure of redundancy for preventing particulate escape from the beds. Figure 5 illustrates the concept.

The redesign involves replacement of the current pan assemblies with new assemblies designed to incorporate an insert. The insert is required to provide a sealing surface for the baffle assembly. The baffle assembly incorporates an o-ring seal. Together with springs, it places the zeolite material under compression and retains the packing to prevent channeling. The dynamic baffle assembly allows for some travel to accommodate thermal growth and material settling. The dynamic baffle can travel a short distance until it comes to rest on the heater core within the adsorbent bed. The pan assembly will incorporate a static seal mounted directly to the hardware via braze. The static seal in the pan assembly serves as a redundant screen to the dynamic baffle.

Bed Pressure Drop Testing

To determine the impact of new sorbent retainment design on packed bed pressure drop, life test 4BMS desiccant and 5A sorbent beds were used to provide comparative check on sensitivity of pressure drop to flow area.

The desiccant bed dynamic baffle and insert were fabricated similar to the flight concept. Pressure drop testing results shows no increase in pressure drop within experimental error.

(Figure 6)

The adsorbent bed dynamic baffle and insert were installed and tested both at a fully packed condition (new) and fully settled condition (when the baffle is resting on the heater core). Pressure drop testing at the fully packed condition shows a slight decrease in pressure drop in the redesign versus the current design. At fully packed, some material must be removed to provide room for the insert.
Material is removed to allow the dynamic baffle to be in
the proper position representing the fully settle state.
Pressure drop testing results shows a decreasing
pressure drop over travel for the current design. In the
redesign case, the pressure drop remains uniform over
baffle travel. This can be explained by the removal of
sorbent is likely offset by obstruction of flow area at end
of travel.

Incorporating the insert and baffle will O-ring will not
adversely affect the pressure drop, the pressure drop
testing suggests the redesign components will lower the
pressure drop across the bed by a small value (5 mmHg) at
nominal flow conditions. The pressure drop results
may be an indication that the CO$_2$ removal performance
impact will also be small.

CONCLUSION

The CDRA is a critical piece of life support equipment in
the air revitalization system of the ISS. This paper
discussed some of the short-term fixes applied to
promote hardware life and restore functionality, as well as
long-term plans and solutions for improving operability
and reliability. Short-term program goals include
completing installation of in-line filters to protect
downstream components from sorbent particles. The
long-term goal is the development and implementation
of a new sorbent retention design that restores 100%
functionality full-time while maintaining reliable system
operability. To date, short-term solutions have restored
CDRA functionality a majority of the time. The long-term
solution will be to improve CDRA functionality to full
capability at all times.

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