In-Space Repair of Reinforced Carbon-Carbon
Thermal Protection System Structures

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Advanced repair and refurbishment technologies are critically needed for the thermal protection system of current space transportation system as well as for future Crew Exploration Vehicles (CEV). The damage to these components could be caused by impact during ground handling or due to falling of ice or other objects during launch. In addition, in-orbit damage includes micrometeoroid and orbital debris impact as well as different factors (weather, launch acoustics, shearing, etc.) during launch and re-entry. The GRC developed GRABER (Glenn Refractory Adhesive for Bonding and Exterior Repair) material has shown multiuse capability for repair of small cracks and damage in reinforced carbon-carbon (RCC) material. The concept consists of preparing an adhesive paste of desired ceramic with appropriate additives and then applying the paste to the damaged/cracked area of the RCC composites with adhesive delivery system. The adhesive paste cures at 100-120°C and transforms into a high temperature ceramic during simulated entry conditions. A number of plasma torch and ArcJet tests were carried out to evaluate the crack repair capability of GRABER materials for Reinforced Carbon-Carbon (RCC) composites. For the large area repair applications, integrated system for tile and leading edge repair (InSTALER) have been developed. In this presentation, critical in-space repair needs and technical challenges as well as various issues and complexities will be discussed along with the plasma performance and post test characterization of repaired RCC materials.
In-Space Repair of Reinforced Carbon-Carbon Thermal Protection System Structures

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Outline

• Background and Introduction
• Need for In-Space Repair and Inspection
• Technical Challenges
  – *Space Environment*
  – *EVA, Tools, Materials Issues*
  – *Inspection, Verification, and Validation*
• Repair Technologies
  – *Crack Repair: GRABER*
  – *Large Area Repair: InSTALER*
• Testing and Characterization
  – *Plasma Performance (ArcJet Testing, Torch Testing, etc)*
  – *Microstructural Characterization*
• Summary and Conclusions
Damage Possibilities to Thermal Protection System (TPS)

- Impact damage during ground handling
- Damage due to falling of ice or other objects during launch
- Micrometeoroid and orbital debris impact
- Damage caused by different factors during launch and reentry (weather, launch acoustics, shearing, etc.)

Launch Pad Debris  Accent EFT Foam Damage  On-Orbit MMOD Damage
CAIB Recommendation R6.4-1

• For missions to the ISS, develop a practicable capability to inspect and effect emergency repairs to the widest possible range of damage to the Thermal Protection System, including both tile and RCC, taking advantage of the additional capabilities available when near to or docked at the ISS.

• For non-station missions, develop a comprehensive autonomous (independent of Station) inspection and repair capability to cover the widest possible range of damage scenarios.

• Accomplish an on-orbit Thermal Protection System inspection, using appropriate assets and capabilities, early in all missions.

• The ultimate objective should be a fully autonomous capability that an ISS mission fails to achieve the correct orbit, fails to dock successfully, or is damaged during or after undocking.

http://www.nasa.gov/columbia/home/CAIB_Vol1.html
Leading Edge Structural Subsystem (LESS)

RCC Components

- Nose Cap, Chin Panel, and Seals
- Forward External Tank Attachment “Arrowhead” Plate
- Wing Leading Edge Panels and Seals
Reinforced Carbon-Carbon (RCC) Composite

Cracks - some through thickness
Sodium Silicate Glass
Short SiC fibers, particles
SiC (~1.5 mm)
-Vacuum infiltrate with Tetra Ethyl Orthosilicate (TEOS)
-Fills cracks with SiO₂

Carbon/Carbon - 2 dimensional lay-up

Dr. Nathan Jacobson, NASA GRC
Cross Sectional View Showing Carbon/Carbon, SiC, and Type A Sealant

Dr. Nathan Jacobson, NASA GRC
STS-45 Impact Damage on Atlantis WLE Panel 10R

Overall View of Impact Sites

Detail of Surface Damage

Detail of Backface Damage
Damage to Leading Edges During Impact Testing on Ground

IML Damage Surface Panel 9L

OML Damage Surface Panel 9L2

Foam Blasts 16-inch Hole in Final Shuttle Test @SWRI, TX, July 7, 2003
Performing Repair in Space Environment

Technical and Operational Challenges

• EVA is like floating in the large pool of water, in a pressurized and only partially form fitting balloon.
• Normal EMU pressure is 4.3 psi.
• Thermal environments of the repair poses a significant challenge (temperature changes from -175 F (-115°C) to +250 F (121°C) and the back again in the span of 90 minutes.
• In some areas, the temperature changes from extreme cold to extreme hot in about 20 minutes time.
• Space vacuum is quite high (10^{-7} or 10^{-8} Torr).
EVA Considerations and Concerns for In Space Repair

- **EVA Access to the damage site** – getting the EVA crewmember there
- **EVA Worksite Restraint** – keeping the crewmember in place and in a stable orientation to effect the repair and react the loads associated with the repair
- **EVA Tools Design and Development** – designing, certifying and manufacturing the tools required for access, restraint, repair and cleanup
- **EVA Repair Techniques Development** – developing and validating the particular techniques required to accomplish access, restrain the crewmember and effect the repair

Nancy Patrick, JSC
Space Shuttle Re-entry Conditions are Quite Harsh and Extreme

- Temperature to 2000 K
- Reduced pressure--0.005 to 0.010 atm
- Gases--O₂, N₂, CO₂
  - Shock leads to O, N and ions
- Short times ~15 minutes/re-entry
- Best simulated with arc-jet
Typical High Temperature Testing Steps for Evaluation of Repair Materials

1. Simulated Testing in High Temperature Furnace (1650 C)
2. QARE Rig Testing (GRC)
3. HYMETS (LaRC)
4. ArcJet Testing at ARC and LCAT
Repair Concepts for Wing Leading Edge Damage

- **Wrap**
- **Plug**
- **Crack Repair**

**Damage Characteristics**
- 16” Hole
- 4” Hole
- ½” Hole
- Crack
Glenn Refractory Adhesive for Bonding and Exterior Repair (GRABER) for Crack Repair

- High temperature adhesive based on organic based systems with a number of inorganic constituents.
- Viscosity and curing behavior (time, temperature) can be tailored to suit the needs.
- GRABER has been used to prepreg a wide variety of ceramic fiber weaves (C, SiO₂, SiC).
- It bonds very well with a wide variety of surfaces and cures up to 120°C with heat.
- It can be acid cured at lower temperatures as well.
Reproducibility, Storage, and Shelf Life Characterization
Brookfield PVS Rheometer Used for the Viscosity Measurements

The temperature control bath has capability from –20°C (-4°F) to 180°C (356°F)
Reproducibility of GRABER 5A

Materials made at different times and in varying amounts show consistent viscosity
Materials stored for different times at room temperature show consistent viscosity
## Effects of Storage Times & Temperatures

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Storage Temperature Effects on GRABER 5A
Material Stored in a Refrigerator at 0 C

Materials stored for different times (1-3 months) had similar type of viscosity behavior as freshly prepared materials

Material was Tested under Vacuum
Storage Effects on GRABER 5A

Material Stored in a Freezer at -15 C

Materials stored for different times (1-3 months) had similar type of viscosity behavior as freshly prepared materials.

Material was Tested under Vacuum
Crack Repair, ArcJet Testing, and Post Test Characterization

- GRABER 5 (0.035” and 0.062” wide cracks-ARC)
- GRABER 5A (0.035” and 0.062”-ARC)
- GRABER 12A (0.035”-JSC and 0.035” and 0.062”-ARC)

No failure through repaired cracks was observed during the ArcJet Tests
Arcjet Tests of Damaged RCC Without Any Repair Material

Front-side Pre-Test View of 0.030” Dia. Slot

Front-side Post-Test View of 0.030” Dia. Slot
Pre-Test Photographs of Repaired Specimens

Run 12 – Model 1993
(0.035” or ~0.89 mm wide crack, GRABER-5A)

Percent Argon = 6% @ 2960F condition
Add air = 11.6% @ 2960F condition
Anomaly: water leak from electrode, which allowed water vapor in the stream
ArcJet Testing of Repaired Specimens
Run 12 – Model 1993
(0.035” or ~0.89 mm wide crack, GRABER-5A)

Front View

Side View

Percent Argon = 6% @ 2960F condition
Add air = 11.6% @ 2960F condition
Anomaly: water leak from electrode, which allowed water vapor in the stream
ArcJet Testing of Repaired Specimens
Run 12 – Model 1993
(0.035” or ~0.89 mm wide crack, GRABER-5A)

Post Test- Front Side

Post Test- Back Side
ArcJet Testing of Repaired Specimens
Run 14 – Model RCC 8
(0.062” or ~1.58 mm wide crack, GRABER-12A)

Percent Argon = 6% @ 2960F condition
Add air = 11.6% @ 2960F condition
Temperatures on model face were higher than previous runs (~3100F)
ArcJet Testing of Repaired Specimens
Run 17 – Model RCC 1
(0.062” or ~1.6 mm wide crack, GRABER-5A)

Percent Argon = 6% @ 2960F condition
Add air = 11.6% @ 2960F condition
Anomaly: Edge failure, sample removed after ~130 seconds @ 2960F condition
Microstructural Characterization of ArcJet Tested Specimens
ArcJet Sample 1993 (150-12), Graber 5A, 0.035” Crack Width

Front Side

There are a few large voids where oxidation has taken place. The Graber material appears fairly well adhered to the C/C material even after testing.
ArcJet Sample 150-11, RCC-1, GRABER 5, 0.062” Crack Width

Back side

Front side

Crack filled with Graber material
ArcJet Sample 150-11, RCC-1, GRABER 5, 0.062” Crack

It appears in this sample that oxidation has reached an advanced stage. There is only a skeleton left of the Graber material which appears to be a glassy phase.
Integrated System for Leading Edge and Tile Repair
(InSTALER)

*Flexible Ceramic Overwrap*

QARE Rig Testing (GRC)

HYMETS (LaRC)

ArcJet Testing at JSC, ARC, and LCAT
Integrated System for Leading Edge and Tile Repair (InSTALER)

Flexible Ceramic Overwrap

Test Sample Temperature Response
Sample: GRC-11-1, Run 1588
Pre-Test
Post Test

Excellent Plasma Performance in ArcJet Tests
Summary and Conclusions

• GRABER-based materials have multiuse capability and multifunctionality for a wide variety of repair applications. These systems have shown excellent plasma performance.

• This system can be easily modified to obtain adhesive materials with desired properties (viscosity, composition, curing behavior, etc.).

• These materials have long shelf life and normal handling and storage techniques can be used. In addition, these materials are affordable since the cost of raw constituents is very low (few dollars a pound)

• Flexible ceramic overwraps have shown excellent plasma performance in ArcJet testing conditions.