A system of coupling optical energy in a waveguide mode, into a resonator that operates in a whispering gallery mode. A first part of the operation uses a fiber in its waveguide mode to couple information into a resonator e.g. a microsphere. The fiber is cleaved at an angle $\theta$ which causes total internal reflection within the fiber. The energy in the fiber then forms an evanescent field and a microsphere is placed in the area of the evanescent field. If the microsphere resonance is resonant with energy in the fiber, then the information in the fiber is effectively transferred to the microsphere.
FIG. 1

FIG. 2
ELECTRO-ABSORPTION MODULATOR SECTION

705
RF OUTPUT
GAIN SECTION
700
MICROSPHERE
OPTICAL OUTPUT
710
A GAP TO INDUCE REFLECTION
PHOTODETECTOR (REVERSELY BIASED ELECTRO-ABSORPTION MODULATOR)

FIG. 7

OUTPUT FROM MICROSPHERE WITH SURFACE GRATING

422
420
DFB LASER

OUTPUT FROM PRISM

426
428

FIG. 8
1

COUPLING SYSTEM TO A MICROSPHERE CAVITY

CROSS-REFERENCE TO RELATED APPLICATIONS


STATEMENT AS TO FEDERALLY-SPONSORED RESEARCH

The invention described herein was made in the performance of work under a NASA contract, and is subject to the provisions of Public Law 96-517 (U.S.C. 202) in which the Contractor has elected to retain title.

BACKGROUND

Microsphere resonators have certain desirable characteristics including exceptionally high quality (“Q”) factors, and small dimensions. Optical systems often use microsphere resonators as a building block for fiber optic systems. However, it is often necessary to couple optical energy from an optical fiber into the microsphere cavity. The existing couplers often suffer from certain drawbacks.

SUMMARY

This application teaches new ways of launching energy into a resonator device such as a microsphere resonator. A first way of doing this is by operating using a direct fiber coupling to a resonator, e.g. a microsphere using a hybrid of a waveguide and prism coupler formed on the fiber itself. Another aspect of the disclosure describes using a surface grating on the resonator in a way that disrupts the evanescent field and used to form a model.

BRIEF DESCRIPTION OF THE DRAWINGS

These and other aspects will now be described in detail with respect to the accompanying drawings, wherein:

FIG. 1 shows an angle polished fiber coupler system for coupling a microsphere;
FIG. 2 shows a model of sphere radius versus fiber characteristic;
FIGS. 3A and 3B show single mode fibers and a resonator;
FIGS. 4A and 4B show an embodiment using this waveguide to whispering mode technique for coupling between different waveguides;
FIGS. 5A-5D show an embodiment for forming the waveguides on a chip and forming a resonator near the waveguides;
FIGS. 6A-6C show details of a system for doing this using optical waveguides;
FIG. 7 shows an embodiment of carrying out electro-optical absorption on a chip;
FIG. 8 shows an embodiment which couples light into a resonator using a surface grating; and
FIGS. 9A-9C shows steps of formation of a improved resonator.

DETAILED DESCRIPTION

FIG. 1 shows the basic schematic embodiment of a first fiber coupler system. A single mode fiber 100 has an end 110 which will be used to couple propagating light 112 into a resonator 120 which can be a microsphere resonator. The single mode fiber 100 is formed with its end area 110 having an angled portion 114. The angled portion 114 forms an angle ω=180-Φ with the direction of the axis of the fiber, as shown. The angle ω is controlled as described herein. The light is coupled in the direction 112 and incident on the angled surface. Upon incidence, the light propagating inside the core comes into contact with the angled region 114. The light undergoes total internal reflection and then forms an evanescent field around the fiber end 110. Effectively the light escapes the fiber in this way. The microsphere 120 is placed in the area of the evanescent field. The energy from the evanescent field is efficiently exchanged in a resonant mode of the microsphere. Effectively, therefore, the information is resonantly transitioned between the “waveguide” mode of the single mode fiber and the whispering gallery mode in the microsphere.

The angle 101 is selected to satisfy a phase matching requirement. The angle is selected according to the relationship Φ=arcsin[(n_sphere/n_fiber)]^2, n_sphere represents the effective refractive index that describes the guided wave in the fiber core truncation area 110. n_sphere represents the effective refractive index that describes the azimuthal propagation of waveguide modes. These can be considered as closed waves, undergoing total internal reflection in the microsphere.

The linear dimensions of the angle-cut core area can match to the area of evanescent field overlap. This allows the system to operate similarly to a prism coupler with illuminated collimation focusing objects.

The effective refraction index can be used to define the azimuthal propagation of the waveguide modes near the surface of the sphere. These can be calculated based on asymptotic expressions for waveguide mode frequencies ω_p, where n_p=cl/α_0 p. l and q are respectively azimuthal and radial mode indexes, a is the radius of the sphere and c is the speed of light. Different indices can be calculated and used to form a model.

More specifically, the effective index to describe the azimuthal propagation of the WG modes can be calculated as n_0=cl/α_0 p on the basis of asymptotic expressions for WG mode “positions” as follows:

\[ \omega_p = \frac{m \pi}{\alpha} + \frac{\pi}{2} \frac{\alpha_{0p}^{(1/3)}}{(\alpha^{(1/3)})^2} \left( \frac{2}{10} \frac{1}{\alpha_{0p}^{(1/3)}} - \frac{2}{10} \frac{1}{\alpha_{0p}^{(1/3)}} \right) \]

Again, l, q are azimuthal and radial mode indices respectively; a is the sphere radius; c is the speed of light; n is the refraction index of the sphere material (n=1.4440 (1.4469) for silica at the wavelength λ=1550 nm (1300 nm)); P=1/n for TE modes and P=1/n for TM modes; V=1+1/2; and α_0p is the q-th root of the Airy function, Ai(-z), equal to 2.338, 4.088, 5.521 for q=1, 2, 3 respectively. Results of calculation of n_sphere (at both wavelengths 1550 nm and 1300 nm) for silica spheres of different radii are given in FIG. 2. The calculation is made for three lowest radial order modes TE (TM)_per p, q=1,2,3.

Since the guided wave in the core no longer exists after reflection, precise calculation of n_sphere is a non-trivial task implying the explicit computation of the evanescent field in the truncation area. However, as confirmed by the experiments below, a consistent recipe for a functional coupler can be based on a straightforward approximation that assumes n_sphere equal to the effective mode index in a regular fiber.
In a specific embodiment, the standard Corning SMF-28 fiber is used with a germanium-doped core of diameter $2a = 8.3 \mu m$ and index difference of 0.36%. The material index of the core was $n_{1} = 1.4505$; the material index of the cladding $n_{2} = 1.4453$ at the wavelength $\lambda = 1550 \text{ nm}$, and correspondingly $n_{1} = 1.4535$ and $n_{2} = 1.4483$ at $\lambda = 1300 \text{ nm}$ (Corning Inc Product Information sheet PI036, 1998). As known from the theory of step-index fibers (see e.g. L. B. Jonnhomme, Single-Mode Fiber Optics (Marcel Dekker, N.Y., 1983)), propagation constant $\beta$ for the core-guided mode can be approximated as follows:

$$\beta = k_0 n_1 [1 + \Delta(n_2/n_1)^2]$$

where $k_0 = \frac{\pi}{\lambda}$ is the free-space wave vector; $\Delta(n_1 - n_2)/n_2$ — the relative index difference; $\beta$ is the normalized transverse decay constant; $V = k_0 n_2 (2\Delta)^{1/2}$ — the normalized frequency. Using standard solution $\varphi(V)$ for the fundamental LP01 mode of the fiber and the parameters of our fiber, the effective index relevant to the phase-matching condition is $n_{\text{guide}} \beta k = 1.4476$ at 1550 nm and $n_{\text{fiber}} \beta k_0 = 1.4509$ at 1300 nm. A short exemplary model is shown in FIG. 2. In this model, different results of calculations are presented for different q values, at the frequency and for different resonators of different characteristics.

Another issue comes from the way in which the fiber and the modes operate after reflection from the truncation plane. After this reflection, the guided wave in the fiber no longer exists. Precise calculation of $n_{\text{guide}}$ becomes difficult. This value is assumed to be equal to the effective index $n_{\text{guide}}$ of the guided wave and the regular fiber, although the precise value may be difficult to obtain.

The specific way in which the system is used is shown in FIGS. 3A and 3B. A close up view of the assembly has two fiber couplers 300, 310, each with cleaved ends as described herein. The polishing angles of the fibers are about 12.1 degrees and 13.3 degrees respectively or $\theta = 77.9^\circ$ and $7.6^\circ$. A fused silica rod 320 supports the microsphere 322 at a radius 235 $\mu m$ between two angled conical fiber couplers. The optical information can be updated between the fibers, via the sphere.

Another issue has described one way of coupling optical energy into such a microsphere. Since evanescent waves are used for the energy coupling, this is effectively near-field coupling.

The principle implemented in the above description of a single mode optical fiber coupler can also be extended to use integrated optic waveguides.

FIG. 4A shows a total internal reflection mirror on a SO edge of a substrate as shown in FIG. 4A. The throughput truncation area, the phase-matched coupling can still be achieved, with adjustment or experimental trimming of the truncation angle.

A corner reflector, or truncated guide can be formed on the edge of a substrate as shown in FIG. 4A. The throughput configuration, which is the analog of FIG. 3B, can be achieved by assembling two chips at 500, 502. The sides of a microsphere 504 can be arranged as shown in FIGS. 5A and 5B. Alternatively, the couplers can be formed in the central part of the chip 510, next to a through hole or a micromachined depression 512 that will house a microcavity 504 as shown in FIG. 5C.

In any of FIGS. 5A–5C, the sphere 504 is arranged relative to the chip 500 as shown in FIG. 5D. Preferably the central diameter line of the sphere 500 is at or around the chip surface. This can facilitate holding the chip into place.

FIG. 5 shows the embodiments incorporating a microsphere cavity. The described method of coupling is applicable to all types of waveguide mode cavities *(including disks, rings etc.). It also provides a tool to achieve efficient coupling between integrated optics components of different materials and substrates.

FIG. 6 shows a filter element including a waveguide microcavity within a case collinear input and output fibers/ waveguides 605, 610 using a sphere for filtering non-resonant paths.

FIG. 6 shows an embodiment of device integration of a novel waveguide coupler element for waveguide modes in microspheres. A coupled optoelectronic oscillator (COEO) is based on a high-Q microsphere. COEO is a variant of a microwave optoelectronic oscillator, OEO (X.S. Yao, L. Maleki, JOSAB, Vol.13, No.8, pp.1725–35, 1996), which is a microwave oscillator that uses optical energy storage elements to achieve high spectral purity signals at frequencies ranging from hundreds of MHz to above 100 GHz. These devices, normally have a laser, optical modulator, detector, microwave amplifier and fiber-optic delay, optoelectronic oscillator. Each of these devices can be implemented on a single chip except for the relatively bulky delay element. By using a miniature optical cavity such as a microsphere, the entire device can be placed on a chip.

The waveguide coupling element described herein facilitates the incorporation of a microsphere in the OEO-on-chip, thereby simplifying the setup. To operate with an optical cavity, the laser in the OEO requires locking to one of the modes of the cavity. Oscillation will occur as the microwave feedback loop will ensure microwave oscillation. This is described in, “coupled OEO,” (X. S. Yao, L. Maleki, Opt. Lett., Vol.22, No. 24, pp.1867–9, 1997).

The embodiment of COEO-on-chip, is shown in FIG. 7. When activated by a current source, the active waveguides 700, 702 provide gain for the laser system. Electroabsorption modulators 705 are fabricated at the ends of waveguides by etching out the insulating gap to separate electrodes of gain sections from modulator sections. The
upper electroabsorption modulator is coated with a high-reflectivity coating to induce pulse colliding in the modulator and thus enhance the mode locking capability. At the lower section 702, the gap 710 between the electroabsorption modulator and the waveguide is etched deeper to induce optical separation. The gap interface acts as a partial mirror to reflect light back to the lower guide and form a laser cavity together with high-Q microsphere and the upper waveguide terminated by a high reflectivity mirror. The lower electroabsorption modulator is reverse biased so that it acts as a photodetector. The output from the photodetector is connected to the upper electroabsorption modulator via a relatively simple matching circuit, to induce microwave oscillation. Because the photodetector and the E/A modulator are essentially the same device, they have similar impedances to the order of few K-Ohms. Thus, these devices are essentially impedance matched. Taking typical values of a 2 Volt modulator switching voltage, a 1 kOhm of modulator, and photodetector impedance, and 0.5 A/W of photodetector responsivity, the optical power required for sustained RF oscillation can be estimated at only 1.28 mW. Such an optical power is easily attainable in semiconductor lasers. This avoids the need for an RF amplifier, which can be a source of the proposed COEO design.

A second embodiment describes far field coupling, using a refractive index grating that is written onto the sphere surface. The grating can be written by shining a pattern of ultraviolet light onto a doped surface. This avoids the need for an RF amplifier, which can be a source of the proposed COEO design.

A method as in claim 1 wherein said cylindrical cavity preform has walls with a diameter 100 to 200 µm, a thickness of 20 to 40 µm, and are on a relatively flat substrate.

The vertical surface of the vertical walls is next re-shaped to provide removal of the mode field from the flat boundaries as shown in FIG. 9B. This is done by removing the edge portions 700 forming a complex shape shown in FIG. 9B. After that, further thermal and mechanical treatment is used to approach ellipsoidal geometry. The edges, e.g. 510, are rounded and smoothed to minimize surface roughness and reduce radiation loss. By rounding these surfaces, curvature confinement and fire polish grade surface can be obtained, obtaining a Q approaching 10^6.

The cylindrical preform described in FIG. 9A can be produced by wet/dry etch as well as ion milling techniques using appropriate crystal orientation. Other techniques such as RTA laser treatment, ultraviolet treatment and infrared treatment can also be used.

Other modifications are contemplated. What is claimed is:

1. A method comprising:
   forming a cylindrical cavity preform with vertical walls;
   re-shaping said vertical walls in a way that removes a mode field from flat boundaries of the vertical walls;
   treating the resulting shape to form an ellipsoidal geometry; and
   rounding and smoothing edges of the ellipsoidal geometry to reduce radiation loss and to form a dielectric resonator body.

2. A method as in claim 1 wherein said cylindrical cavity preform has walls with a diameter of 100 to 200 µm, and a thickness of 20 to 40 µm.

3. A method as in claim 1 wherein said treatment comprises one of wet/dry etching, ion milling techniques, RTA laser treatment, ultraviolet treatment or infrared treatment.

4. A method as in claim 1 wherein said preform is formed of a silica material.