Main chain thermotropic liquid crystal esters, ester-imides, and ester-amides were prepared from AA, BB, and AB type monomeric materials and were end-capped with phenylacetylene, phenylmaleimide, or nadimide reactive end-groups. The resulting reactive end-capped liquid crystal oligomers exhibit a variety of improved and preferred physical properties. The end-capped liquid crystal oligomers have broad liquid crystalline melting ranges and exhibit high melt stability and very low melt viscosities at accessible temperatures. The fully cured products are rubbers above their glass transition temperatures. The resulting thermosets display many properties that are superior to their non-end-capped high molecular weight analogs.
OTHER PUBLICATIONS


* cited by examiner
FIG. 1

FIG. 2
1. Acetic Anhydride/KOAc
2. $\Delta T$
3. \( E \rightarrow Y \) (End-Cap Groups)

\[
\text{FIG. 5}
\]

1. Acetic Anhydride/KOAc
2. $\Delta T$
3. \( E \rightarrow Y \) (End-Cap Groups)

\[
\text{FIG. 6}
\]
1. Acetic Anhydride/KOAc
2. ΔT
3. (End-Cap Groups)

FIG. 7
FIG. 8

Bleeder/Breather Cloth
Bleeder/Breather Cloth
IM-7 Plain Weave Cloth
LaRC - (6HBA/4HNA-5PE) LCR
Release Film

FIG. 9

Temperature, °F

Pressure, Psi

0.5 hrs @ 716°F
1 hrs @ 482°F
Vacuum 20" Hg
Vacuum 30" Hg
Vacuum 5" Hg
FIG. 10
1 LIQUID CRYSTALLINE THERMOSETS
FROM ESTER, ESTER-IMIDE, AND ESTER-AMIDE OLIGOMERS

This application claims the benefit of U.S. provisional application No. 60/232,504, filed Sep. 13, 2000.

ORIGIN OF THE INVENTION

This invention was made by employees of the United States Government and may be manufactured and used by or for the Government for governmental purposes without the payment of any royalties thereon or therefor.

1. Field of the Invention

The present invention relates generally to liquid crystalline polymers and liquid crystal thermosts. Specifically, the invention relates to liquid crystalline ester, ester-imide, and ester-amide oligomers and the improved physical properties of such species when they are end-capped with phenylacetylene, phenylmaleimide, or nadimide terminated monofunctional reactants. The invention also relates to the ability to process liquid crystal polymers and their use in melt process shape forming and blending techniques such as film extrusion, fiber spinning, reactive injection molding (RIM), resin transfer molding (RTM), resin film injection (RFI), powder molding, pultrusion, injection molding, blow molding, and thermo-forming.

2. Description of the Related Art

High molecular weight linear ester-based thermotropic liquid crystalline polymers (TLCPs) are known in the literature. Non-ends-capped TLCP copolymers are taught by Kohluss and Jackson in U.S. Pat. No. 3,778,410 and U.S. Pat. No. 3,804,805. TLCP polymers with non-reactive phenylester and ethylester end-cap groups, that can only be thermost at elevated temperatures via oxidative backbone crosslinking, are taught by Calundann in U.S. Pat. No. 4,067,852 and U.S. Pat. No. 4,161,470 and Calundann et al. in U.S. Pat. No. 4,083,829. McCarthy et al. in U.S. Pat. No. 5,319,064 and Plotzker et al. in U.S. Pat. No. 5,688,895 teach high molecular weight liquid crystalline poly(ester-amide)s, Alanko et al. teach in U.S. Pat. No. 5,843,541, high molecular weight poly(ester-imide), and Hisgen et al. teach high molecular weight poly(ester-imide) in U.S. Pat. No. 4,762,906. The McCarthy et al., Plotzker et al., Alanko et al., and Hisgen et al. patents do not teach polymers with melt viscosities in the range of approximately 1 to approximately 250 poise and the claimed high molecular weight liquid crystalline polymers have neither reactive end-caps nor rubber characteristics above Tg. Kricheldorf et al. in Mol. Cryst. Liq. Cryst., 254, 87 (1994) teach other aliphatic and aromatic liquid crystalline poly(ester-imide)s, while Calundann et al. teach other thermotropoly(ester-amide)s in Mol. Cryst. Liq. Cryst., 157, 615 (1988) and U.S. Pat. No. 4,351,918. All of the above materials are very difficult to melt process due to their high melt viscosities.

Improved melt processability of linear high molecular weight TLCPs was achieved by the addition of small amounts of low molecular weight organic compounds during the melt processing steps of the high molecular weight liquid crystal polymers by the teachings of Froix in U.S. Pat. No. 4,267,289 and Yoon in U.S. Pat. No. 4,581,399. Charbonneau et al. in U.S. Pat. No. 4,746,694 teach liquid crystal polymers with relatively low melt viscosities (200-1000 poise at 345° C. and a shear rate of 100 radians/sec) by disrupting the linear progression of the polymer backbone.

This process results in undesirable volatiles. Thermosets have been prepared from thermotropic liquid crystalline polymers. Uryu and Kato teach, in U.S. Pat. No. 4,710,547, thermotropic liquid crystal thermosts (TLCTs) via incorporation of trifunctional cross-link units into the TLCPs in order to immobilize the anisotropic melt. Haider et al. teach, in U.S. Pat. No. 5,216,073, a moldable composition by blending a liquid crystal polyester with an epoxy-functionalized rubber. In U.S. Pat. No. 4,654,412, Calundann et al. teach incorporation of stilbene and tolane type difunctional monomers into the backbone of main chain wholly aromatic liquid crystalline polymers in which cured shaped articles made of these polymers were prepared by backbone crosslinking using a maleic anhydride dippase procedure requiring an undesirable second process step.


Lubowitz et al. teach, in U.S. Pat. Nos. 4,661,604, 4,684, 714, U.S. Pat. No. 4,739,030, U.S. Pat. No. 4,851,501, and U.S. Pat. No. 5,550,204 self-reactive end-cap monomers to prepare oligomeric polymer resins, including polyesters. Lubowitz et al. however, do not teach using the claimed end-caps with liquid crystal oligomers. Lubowitz et al. further, teach the use of end-cap groups that will not survive the melt condensation polymerization conditions. Finally, Lubowitz et al. do not teach materials with melt viscosities in the range of approximately 1 to approximately 250 poise at a shear rate of 100 radians/second.

Bilow et al. teach, in U.S. Pat. No. 3,864,309, polyimide oligomers end-capped with terminal acetylene or cyano groups. Bilow et al.'s use of the term "oligomer" is inconsistent with our present use of the term "oligomer." Bilow et al. teach low molecular weight pure end-capped imides as opposed to low molecular weight polyimide oligomers; the Bilow et al. patent teaches end-capped backbone structures of only one unit wherein an entire sample contains only molecules of the same length and molecular weight. Bilow et al. teach the use of end-cap groups that will not survive melt condensation polymerization conditions. Finally, Bilow et al. teach materials that are neither liquid crystalline nor have melt viscosities in the range of approximately 1 to approximately 250 poise at a shear rate of 100 radians/second.

Reinhardt et al. teach, in U.S. Pat. No. 4,513,131, phenylacetylene end-capped low molecular weight pure aryl ethers as opposed to the polyester, poly(ester-amide), and poly(ester-imide) oligomers. Reinhardt et al teach materials that are not liquid crystals. Reinhardt et al. teach pure low molecular weight polymer samples as opposed to the oligomeric mixtures.

Similarly, Sheppard et al. in U.S. Pat. No. 4,851,495, Kwinkowski et al. in U.S. Pat. No. 3,839,287, Kovar et al. in U.S. Pat. No. 3,975,444, Baudouin et al. in U.S. Pat. No.
The claimed invention of reactive end-capped oligomeric (ester) amide is novel and non-obvious over the prior art.

The present invention relates to a novel family of polyamide oligomers having a reactive end group and a reactive core. The invention includes compositions of matter, methods of making compositions of matter, and methods of using compositions of matter.

SUMMARY OF THE INVENTION

Based on what has been presented above, it is an objective of the present invention to provide a new family of polyamide oligomers having a reactive end group and a reactive core. These end-capped oligomers can be produced by a variety of methods, including, but not limited to, solution polymerization, melt polymerization, or free-radical polymerization. The end-capped oligomers can be used in a variety of applications, such as adhesives, sealants, coatings, and thermosets.
can be identical or different on any given end-cap unit provided they do not interfere with the melt condensation synthesis of the liquid crystal oligomers or the higher temperature curing step. Possible R' substituents include hydrogen, lower allyl groups (preferably containing four or less carbon atoms) such as methyl, ethyl, propyl, and butyl groups, aryl groups (preferably containing six to ten carbon atoms) such as phenyl or naphthyl groups, lower alkoxy groups such as methoxy, ethoxy, and propoxy, lower arloxy groups such as phenoxy or benzoxy, or halogen groups (i.e. fluoro, chloro, bromo, or iodo groups). Other phenylacetylene end-cap derivatives include 4-phenylethynyl-phenol and 4-phenylethynylbenzoic acid.

The present invention end-capped liquid crystal ester, ester-imide, and ester-amide oligomers can be modified by means of conventional additives, used in conventional amounts, of stabilizers, oxidation inhibitors, agents against thermal and ultraviolet light decomposition, lubricants, mold release agents, colorants such as dyes and pigments, fibrous or pulverulent fillers and reinforcing agents, nucleating agents, and/or plasticizers.

**BRIEF DESCRIPTIONS OF THE FIGURES**

FIG. 1 indicates, but does not intend to limit, the structural repeat units of the end-capped liquid crystal ester, ester-imide, and ester-amide oligomers.

FIG. 2 indicates, but does not intend to limit, the R units of the structural repeat units of the end-capped liquid crystal ester, ester-imide, and ester-amide oligomers depicted in FIG. 1.

FIG. 3 indicates, but does not intend to limit, the Ar units of the structural repeat units of the end-capped liquid crystal ester, ester-imide, and ester-amide oligomers depicted in FIG. 1.

FIG. 4 indicates, but does not intend to limit, the X units depicted in FIG. 3.

FIG. 5 is a sample reaction.

FIG. 6 is a sample reaction.

FIG. 7 is a sample reaction.

FIG. 8 is a composite laminate lay-up configuration of the end-capped liquid crystal oligomers.

FIG. 9 is schematic of the cure cycle for the melt processing of 6HBA/4HNA-5PE into laminate graphite cloth (6HBA/4HNA-5PE)/IM-7).

FIG. 10 is schematic of the cure cycle for the melt processing of 6HBA/4HNA-9PE into a neat resin plaque (6HBA/4HNA-9PE).

FIG. 11 is the mold configuration for the fabrication of a (6HBA/4HNA-9PE) plaque.

**DETAILED DESCRIPTION OF THE INVENTION**

Within the scope of the present invention, the term “oligomer(s)” and “oligomer mixture(s)” designate mixtures of varying backbone length liquid crystal polymers, of maximally 500 repeat units, within the weight range of approximately 1000 to approximately 15,000 grams per mole that are not isolated as discreet molecular weight polymers.

The term “pure” designates liquid crystal compounds in which all molecules of a given sample are of the same length and molecular weight. The terms “high weight” and “high molecular weight” designate polymers and mixtures of polymers in which additional increases in polymer length and weight have no effect on the physical properties, including processability, of the polymers and mixtures.

Linear liquid crystal polymers (LCPs) exhibit higher degrees of molecular order while in the molten state than traditional polymeric species. The ability of these species to maintain molecular order in the molten state has pronounced effects on the solid state physical properties of this class of polymers. Specifically, liquid crystalline polymers exhibit molecular order in the solid state and lower melt viscosities at higher molecular weights. The improved molecular order in the solid state makes liquid crystal polymers desirable for uses in shape molded composite materials. Despite LCPs exhibiting reduced melt viscosities, the melt viscosities have not until now been sufficiently low to make higher weight LCPs amenable to improved melt process shape forming and blending techniques such as film extrusion, fiber spinning, reactive injection molding (RIM), resin transfer molding (RTM), resin film injection (RFI), powder molding, pultrusion, injection molding, blow molding, plasma spraying, and thermo-forming.

Linear thermotropic liquid crystals typically have very high melting points and molecular weights that limit their ability to be melt processed. Once formed, however, the polymers typically have very high melting points and molecular weights that limit their ability to be melt processed. The present invention involves the preparation of liquid crystal oligomers of relatively moderate weight and length via traditional melt state condensation techniques. The liquid crystal oligomers were end-capped in the melt state with phenylacetylene, phenylmaleimide, or nadimide terminated monofunctional reactants. These end-caps are stable in the melt state condensation conditions needed for preparing the liquid crystal oligomers. The end-caps were chosen so as to polymerize with each other at temperatures above the range used for the melt condensation preparation of the oligomers but below that which will induce cross-linking of the liquid crystal backbone.

The resulting end-capped LCTs display many superior and improved properties to their non-end-capped high molecular weight analogs that are non-obvious and unanticipated in the literature. Among these properties are: unusually lowered melt viscosities for these weight polymer species compared to non-end-capped higher molecular weight analogs and comparable and/or superior to previously end-capped lower weight non-oligomeric species (end-capped single pure molecules), stability of melt viscosities at elevated temperatures for extended periods of time relative to previous liquid crystalline products, and reduced brittleness (i.e. rubber behavior) above the glass transition temperature.

The end-capped liquid crystal oligomers exhibit lower melt viscosities than the corresponding non-end-capped high weight analogs. Being polymeric, the end-capped liquid crystal oligomers exhibit superior physical properties relative to well-defined end-capped low weight pure liquid crystal esters. This class of end-capped liquid crystal oligomers, therefore, exhibits improved melt processability relative to higher weight analogs while maintaining the benefits of being polymeric relative to well-defined end-capped low weight pure liquid crystal esters. In many instances, the lowered melt viscosity can be maintained for extended periods of time relative to the non-end-capped higher weight analogs and comparable and/or superior to the end-capped low weight pure liquid crystal esters. Lowered melt viscosities make this class new liquid crystal polymers more amenable to melt processing. For the first time, higher weight liquid crystal oligomers can be used effectively in melt process shape forming and blending techniques.
Once melt processed and shaped, the end-capped liquid crystal oligomers were cured at elevated temperatures (temperatures above that used for the melt state condensation) resulting in liquid crystal thermosets. This second step causes the end-caps to react with one another and further increases the molecular weight of the liquid crystal polymers. Traditionally, heat curing of polymer molds is carried out at temperatures sufficiently high to induce cross-linking of the polymer backbone. Cross-linking of the backbone, however, often makes the cured product brittle. In the present invention, the reactions between the end-caps can be carried out at temperatures below that which would induce significant cross-linking within the liquid crystal oligomer backbone while the degree of end-cap polymerization can be controlled through varying length and temperature of exposure. Unexpectedly, the lack of significant backbone cross-linking produces liquid crystal polymers that behave as rubbers when elevated above their glass transition temperatures rather than becoming brittle.

Method of Preparation

The "backbones" of the end-capped liquid crystalline ester, ester-imide, or ester-amide oligomers were prepared from the reaction between varying quantities and combinations of one or more aromatic, heterocyclic or aliphatic dicarboxylic acids, aromatic, heterocyclic or aliphatic diols, aromatic, heterocyclic or aliphatic diamines, hydroxybenzoic acids and aminobenzoic acids. The preferred embodiments of the end-capped ester, ester-imide, and ester-amide oligomers backbones are depicted in FIG. 1 wherein R is the structural units depicted in FIG. 2 and Ar is the structural units depicted in FIG. 3 and X is the structural units depicted in FIG. 4. The preferred general methods of preparation of the end-capped ester, ester-imide, and ester-amide oligomers are presented in FIGS. 5, 6, and 7 wherein R1, R2, and R3 can be identical or different and are the structural units depicted in FIG. 2 and Ar1, Ar2, and Ar3 can be identical or different and are the structural units depicted in FIG. 3 and X is the structural units depicted in FIG. 4. E-Y represents end-cap units I, II, and/or III that can be prepared by methods available in the literature, wherein Y can be a carboxy, hydroxy, amino group or any reactive analog thereof (e.g., acetoxy, propionoxy, butoxy, etc.), or an esterified carboxy group (e.g., methylbenzoate, ethylbenzoate, phenylbenzoate, etc.) and the R' substituents can be identical or different on any given end-cap unit provided they do not interfere with the melt condensation synthesis of the liquid crystal oligomers or the higher temperature curing step. Possible R' substituents include hydrogen, lower alkyl groups (preferably containing four or less carbon atoms) such as methyl, ethyl, propyl, and butyl groups, aryl groups (preferably containing six to ten carbon atoms) such as phenyl or naphthyl groups, lower alkoxy groups such as methoxy, ethoxy, and propoxy, lower aryloxy groups such as phenoxy or benzoxy, or halogen groups (i.e. fluoro, chloro, bromo, or iodo groups). The stoichiometric amounts of each reactant and end-cap group can be varied to prepare oligomers of varying size, weight, characteristic and chemical content. The reactions depicted in FIGS. 5, 6, and 7 are generally performed at between approximately 140°C to approximately 350°C. The melt viscosities of the end-capped ester, ester-imide, and ester-amide oligomers are lower than their non-end-capped analogs.

The present invention end-capped liquid crystal ester, ester-imide, and ester-amide oligomers can be modified by means of conventional additives, used in conventional amounts, of stabilizers, oxidation inhibitors, agents against thermal and ultraviolet light decomposition, lubricants, mold release agents, colorants such as dyes and pigments, fibrous or pulverulent fillers and reinforcing agents, nucleating agents, or plasticizers.

The following specific examples are provided for illustrative purposes. These examples do not serve to limit the scope of the invention.

**EXAMPLES**

**Preparation of Reactive End-Caps**

The following examples illustrate the reaction sequence for the synthesis of the reactive end groups that were used for the preparation of end-capped ester, ester-imide, and ester-amide oligomers.

**Example A**

**Phenylacetylene Terminated Carboxylic Acid; PE-COOH**

Into a 250 mL two-neck round bottom flask equipped with a mechanical stirrer, condenser and a nitrogen gas inlet was placed 4-aminobenzoic acid (8.0 g, 58 mmol), 4-phenylethynylphthalic-anhydride (14.5 g, 58 mmol) and 150 mL glacial acetic acid. This mixture was stirred at 25°C for 1 hour after which the temperature was raised to reflux for 12 hours. The reaction mixture was cooled to 25°C and the precipitated product was collected by filtration, washed twice with hot ethanol and dried under vacuum at 100°C for 8 hours.

**Example B**

**Phenylacetylene Terminated Acetoxy Phenol; PE-OAc**

Into a 250 mL two-neck round bottom flask equipped with a mechanical stirrer, condenser and a nitrogen gas inlet was placed 4-aminophenol (6.3 g, 58 mmol), 4-phenylethynylphthalic-anhydride (14.5 g, 58 mmol) and 200 mL glacial acetic acid. This mixture was stirred at 25°C for 1 hour after which the temperature was raised to reflux for 12 hours. The reaction mixture was cooled to 25°C and the precipitated product was collected by filtration, washed twice with ethanol and dried under vacuum at 50°C for 8 hours.

The dried end-cap products were refluxed in 150 mL acetic anhydride for 5 hours. Yellow crystals precipitated upon cooling and were collected by filtration, washed with ethanol and dried under vacuum at 80°C for 8 hours.

Other end groups were made using similar procedures. The yields and thermal analysis results (differential scanning calorimetry) of all compounds are summarized in Table 1.
<table>
<thead>
<tr>
<th>Molecular Structure</th>
<th>Name</th>
<th>Yield (%)</th>
<th>Tm (°C)</th>
<th>ΔH_mol (kJ mol⁻¹)</th>
<th>Exotherm range (°C)</th>
<th>ΔH_exo (kJ mol⁻¹)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>PE—COOH</td>
<td>92</td>
<td>347.8</td>
<td>36.21</td>
<td>363–421</td>
<td>-67</td>
</tr>
<tr>
<td></td>
<td>PE—OAc</td>
<td>93</td>
<td>236.6</td>
<td>38.71</td>
<td>340–426</td>
<td>-115</td>
</tr>
<tr>
<td></td>
<td>PM—COOH</td>
<td>92</td>
<td>261.2</td>
<td>30.2</td>
<td>311–407</td>
<td>-23</td>
</tr>
<tr>
<td></td>
<td>PM—OAc</td>
<td>94</td>
<td>155.6</td>
<td>29.3</td>
<td>302–421</td>
<td>-54</td>
</tr>
<tr>
<td></td>
<td>NOR—COOH</td>
<td>77</td>
<td>233.1</td>
<td>30.61</td>
<td>290–360</td>
<td>-21</td>
</tr>
<tr>
<td></td>
<td>NOR—OAc</td>
<td>90</td>
<td>191.4</td>
<td>27.2</td>
<td>310–388</td>
<td>-32</td>
</tr>
</tbody>
</table>

Preparation of End-Capped Liquid Crystal Oligomers

Example 1

A 100 mL 3-neck round bottom flask was charged with 4-acetoxybenzoic acid (45.1 g, 0.25 mol), 6-acetoxy-2-naphthoic acid (38.4 g, 0.17 mol), PE—COOH (2.43 g, 6.6 mmol), PE—OAc (2.52 g, 6.6 mmol) and 4 mg potassium acetate. The flask was equipped with a sealed glass paddle stirrer, a nitrogen inlet tube and an insulated distillation head. The flask was purged with nitrogen gas, and the reaction mixture was heated over a 3 hour period on a woods metal bath, under a slow stream of nitrogen, with the reaction temperature being increased from 150° C. to 300° C. At this point the temperature was increased to 310° C. over 30 minutes and a vacuum was slowly applied for 25 min. The opaque melt was cooled to room temperature and the product (6HBA/4HNA-9PE) was broken from the flask and ground into a fine powder.
A 100 mL 3-neck round bottom flask was charged with 4-hydroxybenzoic acid (20.72 g, 0.15 mol), 6-hydroxy-2-naphthoic acid (18.82 g, 0.1 mol), NOR-COOH (1.17 g, 3.2 mmol), PE-COOH (0.49 g, 1.3 mmol), PE-OAc (0.5 g, 1.5 mmol) and 3 mg potassium acetate. The flask was equipped with a sealed glass paddle stirrer, a nitrogen inlet tube and an insulated distillation head. The flask was purged with nitrogen gas, and the reaction mixture was heated over a 1 hour period on a woods metal bath, under a slow stream of nitrogen, to 140°C and held for 1 hour at this temperature. The reaction temperature was increased to 250°C in 100 min. and held at this temperature for 50 min. The reaction temperature was increased from 250°C to 275°C in 30 min. and a vacuum was slowly applied for 20 min. The opaque melt was cooled to room temperature and the product (6HBA/4HNA-9PE) was broken from the flask and ground into a fine powder.

Example III

A 100 mL 3-neck round bottom flask was charged with 4-hydroxybenzoic acid (20.72 g, 0.15 mol), 6-hydroxy-2-naphthoic acid (18.82 g, 0.1 mol), PM-COOH (1.17 g, 3.2 mmol), PM-OAc (1.23 g, 3.2 mmol), and 5 mg potassium acetate. The flask was equipped with a sealed glass paddle stirrer, a nitrogen inlet tube and an insulated distillation head. The flask was purged with nitrogen gas, and the reaction mixture was heated over a 1 hour period on a woods metal bath, under a slow stream of nitrogen, to 140°C and held for 1 hour at this temperature. The reaction temperature was increased to 250°C in 100 min. and held at this temperature for 50 min. The reaction temperature was increased from 250°C to 275°C in 30 min. and a vacuum was slowly applied for 20 min. The opaque melt was cooled to room temperature and the product (6HBA/4HNA-9PE) was broken from the flask and ground into a fine powder.

Example IV

A 100 mL 3-neck round bottom flask was charged with 4-acetoxybenzoic acid (19.8 g, 0.11 mol), 6-acetoxy-2-naphthoic acid (2.3 g, 0.01 mol), 2,6-diacectoxyphthalene (9.77 g, 0.04 mol), terephthalic acid (6.65 g, 0.04 mol), PE-COOH (1.17 g, 3.2 mmol), PE-OAc (2.21 g, 3.2 mmol) and 4 mg potassium acetate. The flask was equipped with a sealed glass paddle stirrer, a nitrogen inlet tube and an insulated distillation head. The flask was purged with nitrogen gas, and the reaction mixture was heated over a 3 hour period on a woods metal bath, under a slow stream of nitrogen, to 140°C and held for 1 hour at this temperature. The reaction temperature was increased to 250°C in 110 min. and held at this temperature for 50 min. The reaction temperature was increased from 250°C to 300°C in 30 min. and a vacuum was slowly applied for 20 min. The opaque melt was cooled to room temperature and the product (6HBA/4HNA-9PM) was broken from the flask and ground into a fine powder.

Example V

A 100 mL 3-neck round bottom flask was charged with terephthalic acid (8.31 g, 0.05 mol), ethylene bis(4-hydroxybenzoate) (13.33 g, 0.044 mol), 4-acetoxyphenylethynyl (2.77 g, 0.012 mol), and 4 mg potassium acetate. The flask was equipped with a sealed glass paddle stirrer, a nitrogen inlet tube and an insulated distillation head. The flask was purged with nitrogen gas, and the reaction mixture was heated over a 3 hour period on a woods metal bath, under a slow stream of nitrogen, with the reaction temperature being increased from 150°C to 260°C. After three hours the temperature was increased to 280°C over 30 minutes and a vacuum was slowly applied for 15 min. The opaque melt was cooled to room temperature and the product (50TA/25HBA/25ES-9PE) was broken from the flask and ground into a fine powder.

Example VI

A 100 mL 3-neck round bottom flask was charged with terephthalic acid (7.62 g, 0.046 mol), ethylene bis(4-acetoxyanilide) (18.85 g, 0.049 mol), PE-COOH (2.32 g, 6.3 mmol) and 4 mg potassium acetate. The flask was equipped with a sealed glass paddle stirrer, a nitrogen inlet tube and an insulated distillation head. The flask was purged with nitrogen gas, and the reaction mixture was heated over a 3 hour period on a woods metal bath, under a slow stream of nitrogen, with the reaction temperature being increased from 150°C to 300°C. At this point the temperature was increased to 310°C over 30 minutes and a vacuum was slowly applied for 15 min. The opaque melt solidified and was cooled to room temperature. The product (50TA/25AB/25EG-9PE) was broken from the flask and ground into a fine powder.

Characterization of End-Capped Liquid Crystal Oligomers

The end-capped liquid crystal oligomers were characterized using melt rheology, thermogravimetric analysis (TGA) and differential scanning calorimetry (DSC). All results are summarized in Tables 2 and 3.
TABLE 2
Optical microscopy and melt rheology results.

<table>
<thead>
<tr>
<th>Example</th>
<th>Name</th>
<th>Phase type (</th>
<th>Phase Behavior at 250°C</th>
<th>Phase hold at 370°C for 1 h)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>(g(P)) at 100 rad.s⁻¹</td>
<td></td>
<td></td>
</tr>
<tr>
<td>I</td>
<td>6HBA4HNA</td>
<td>N</td>
<td>N</td>
<td>(1E5-9E5)/250</td>
</tr>
<tr>
<td>I1</td>
<td>6HBA4HNA-1PE</td>
<td>N</td>
<td>N</td>
<td>(200-900)/250</td>
</tr>
<tr>
<td>II</td>
<td>6HBA4HNA-9PE</td>
<td>N</td>
<td>N</td>
<td>(30-9)/250</td>
</tr>
<tr>
<td>II1</td>
<td>6HBA4HNA-13PE</td>
<td>N</td>
<td>N</td>
<td>(30-3)/250</td>
</tr>
<tr>
<td>III</td>
<td>6HBA4HNA-9NOR</td>
<td>N</td>
<td>N</td>
<td>(4E4-1E5)/250</td>
</tr>
<tr>
<td>IV</td>
<td>6HBA4HNA-9PE</td>
<td>N</td>
<td>N</td>
<td>(5E3-1E4)/250</td>
</tr>
<tr>
<td>V</td>
<td>6HBA4HNA-9PM</td>
<td>N</td>
<td>N</td>
<td></td>
</tr>
<tr>
<td>VI</td>
<td>55HBA20TA/5HNA20N D-9PE</td>
<td>N</td>
<td>65</td>
<td></td>
</tr>
<tr>
<td>VI1</td>
<td>50TA/25HBA/25EG-5APE</td>
<td>N</td>
<td>65</td>
<td></td>
</tr>
<tr>
<td>VI11</td>
<td>50TA/25HBA/25AP-9PE</td>
<td>N</td>
<td>65</td>
<td></td>
</tr>
<tr>
<td>VII</td>
<td>50TA/25AB/25EG-9PE</td>
<td>N</td>
<td>65</td>
<td></td>
</tr>
<tr>
<td>VIII</td>
<td>6HBA4HIM-9PE</td>
<td>N</td>
<td>N</td>
<td></td>
</tr>
</tbody>
</table>

N = nematic
I = isotropic

TABLE 3
Thermal properties of the LC oligomers.

<table>
<thead>
<tr>
<th>Example</th>
<th>Name</th>
<th>5% wt. loss in N₂ (% C.)</th>
<th>5% wt. loss in air (% C.)</th>
<th>Tg (°C.)</th>
<th>Tm (°C.)</th>
<th>Heat 1</th>
<th>Heat 2</th>
<th>Heat 3</th>
</tr>
</thead>
<tbody>
<tr>
<td>I</td>
<td>6HBA4HNA</td>
<td>414</td>
<td>401</td>
<td>91</td>
<td>91</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>I1</td>
<td>6HBA4HNA-1PE</td>
<td>431</td>
<td>411</td>
<td>100</td>
<td>205</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>II</td>
<td>6HBA4HNA-5PE</td>
<td>458</td>
<td>454</td>
<td>85</td>
<td>245</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>III</td>
<td>6HBA4HNA-9PE</td>
<td>454</td>
<td>449</td>
<td>80</td>
<td>84</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>IV</td>
<td>6HBA4HNA-13PE</td>
<td>409</td>
<td>393</td>
<td>393</td>
<td>393</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>IX</td>
<td>6HBA4HNA-9NOR</td>
<td>433</td>
<td>401</td>
<td>401</td>
<td>231</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>V</td>
<td>55HBA20TA/5HNA20N D-9PE</td>
<td>394</td>
<td>361</td>
<td>361</td>
<td>361</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>VI</td>
<td>50TA/25HBA/25EG-5APE</td>
<td>438</td>
<td>400</td>
<td>400</td>
<td>400</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>VII</td>
<td>50TA/25AB/25EG-9PE</td>
<td>427</td>
<td>400</td>
<td>400</td>
<td>400</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>VIII</td>
<td>6HBA4HIM-9PE</td>
<td>385</td>
<td>408</td>
<td>138</td>
<td>317</td>
<td>210</td>
<td>294</td>
<td></td>
</tr>
</tbody>
</table>

Note: The heating rate for TGA experiments was 2.5°C min⁻¹ and a heating rate of 10°C min⁻¹ was used for DSC experiments. The TGA samples were cured at 350°C for 1 h, prior to the measurement. The DSC samples were heated to 350°C and held for 1 h, prior to the second heat.

With exception of the ester oligomers with aliphatic spacers, all oligomers formed films that did not flow under stress and appeared nematic in nature after curing. Films that have a low concentration of reactive end groups behave more elastic above their Tg, while the films with high concentrations of reactive end groups are more brittle in nature. Isotropization temperatures could not be observed for the wholly aromatic oligomer series. Mechanical test data are shown in Tables 4 and 5.

TABLE 4
Film tensile test results at room temperature

<table>
<thead>
<tr>
<th>Example</th>
<th>Name</th>
<th>Strain at break (%)</th>
<th>Modulus (GPa)</th>
<th>Yield stress (MPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>7HBA3HNA-9PE</td>
<td>mean</td>
<td>2.635</td>
<td>2.700</td>
<td>55.187</td>
</tr>
<tr>
<td></td>
<td>Std. dev.</td>
<td>0.088</td>
<td>0.144</td>
<td>2.760</td>
</tr>
</tbody>
</table>

TABLE 5
Film 3-point bending test results [ASTM D790] at room temperature

<table>
<thead>
<tr>
<th>Example</th>
<th>Name</th>
<th>Strain at peak (%)</th>
<th>Modulus (GPa)</th>
<th>Max stress (MPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>7HBA3HNA-9PE</td>
<td>mean</td>
<td>3.215</td>
<td>3.925</td>
<td>91.5</td>
</tr>
<tr>
<td></td>
<td>Std. dev.</td>
<td>0.787</td>
<td>0.409</td>
<td>10.0</td>
</tr>
</tbody>
</table>

Melt Processing Examples of End-Capped Liquid Crystal Oligomers

Thin films were prepared by heating 7HBA3HNA 9PE, heated with 10°C/min. to 370°C and were held at this temperature for 1 hour to allow the reactive end groups to react. The norbomene and phenylmaleimide end groups react at temperatures between 250°C and 400°C. The phenylacetylene end groups are more stable in the melt and no significant end group chemistry could be observed below 310°C, i.e. no increase in melt viscosity could be observed.

Example IX
Composite Laminates Film

One ply of kapton film was placed on a metal plate and 25 grams of 6HBA4HNA-5PE) was spread evenly on top of the kapton film. Four plies of plain weave IM-7 graphite cloth was placed above the powder, followed by two plies of 0.0025” Teflon bleeder/breather cloth. FIG. 8 is a composite laminate lay-up configuration of the end-capped liquid crystal oligomers. The entire lay-up was contained in a metal dam and was vacuum bagged utilizing a standard vacuum
The bagging process for high temperature polyimides. The (6HBA/4HNA-9PE)/IM-7 cloth was heated to 482°F with 5 Hg of vacuum and held for one hour. During the hour hold, the viscosity of the resin decreased and was forced up through the plain weave cloth via the 5 Hg of vacuum. After 60 minutes at 482°F, the vacuum was increased to 20 Hg and the temperature was ramped to the final cure temperature of 700°F. As the temperature reached 600°F, the part was held for 30 minutes to allow the reactive end groups (PE) to react and then the laminate was cooled to ambient temperature while maintaining full vacuum. At ambient temperature, the mold was removed from the vacuum bag and the laminate was removed from the metal dam. FIG. 9 is schematic of the cure cycle for the processing of 6HBA/4HNA-9PE into laminate graphite cloth (6HBA/4HNA-9PE)/IM-7. Upon visual and ultrasonic examination, the laminate was determined to be of good quality. This result indicates that the low zero shear melt viscosity of the thermotropic LC precursors leads to excellent wet-out of the carbon fiber reinforcement.

Example X
Resin Plaque

(6HBA/4HNA-9PE) was fabricated into a neat resin plaque by the process shown in FIG. 10. The neat resin plaques were fabricated in order to test mechanical properties such as; KIC (opening mode fracture toughness), flexure strength and modulus, and compressive strength and modulus. A conceptual drawing of the mold that was used to fabricate the neat resin plaques is depicted in FIG. 11. The mold was 3.5”x3.5” and was restricted to a maximum height of 0.5”. The height was restricted by placing steel spacers in the mold to ensure the final dimensions of the plaque were at least 3”x3”x0.5”. Two steel spacers with dimension, 1.5”x0.25”x0.5”, were placed in the mold. A piece of Kapton film was placed into the base of the mold and onto the film was poured 100 grams of (6HBA/4HNA-9PE). This material was compacted in a hydraulic press and another piece of Kapton film and the steel plunger were inserted into the mold. The entire mold was placed in a vacuum hydraulic press. The (6HBA/4HNA-9PE) was heated to 572°F with no pressure or vacuum and held for 30 min. During this hold, the (6HBA/4HNA-9PE) began to react which was evident by an increase in viscosity and the production of acetic acid. After 30 min. at 572°F, the temperature was increased to 608°F and 30 Hg of vacuum was applied. The polymer was held at 608°F for 30 min. and the temperature was increased to its final holding temperature of 675°F. As the temperature approached 675°F, pressure (100 psi) was applied. The plaque was held at 675°F for 1 hour and was cooled to room temperature under full vacuum and pressure. The plaque was removed from the mold and visual inspection indicated a well consolidated neat resin plaque with a density of 0.86 g/cm³.

Example XI
Foam Structure

A foamed structure was fabricated by using (6HBA/4HNA-9PE) that was not fully polymerized. The process was the same as described in Example X. During the high temperature vacuum step the released acetic acid acts as a blowing agent and a plaque was obtained that has a well defined porous density (0.43 g/cm³) and shows good mechanical properties.

Example XII
Adhesive Resin

To test adhesive bonding, an adhesive scrim cloth was saturated with molten (6HBA/4HNA-9PE) at 280°C. The resulting cloth contained 28 wt % resin and was placed between two titanium coupons to form a lap joint with a surface area of 2.54x1.27 cm (1x0.5 inch). The titanium coupons were sand blasted, treated with Pasa-Gel 1072, washed, and dried prior to use. The lap joints were bonded in a heated press for 1 h. at 350°C and 15 psi. The resulting bonded lap joints were tested at room temperature according to ASTM D 1002. The results are summarized in Table 6.

<table>
<thead>
<tr>
<th>Sample Set</th>
<th>Bond Press (MPa)</th>
<th>Bondline (μm)</th>
<th>Area of overlap (in²)</th>
<th>Length of overlap (inch)</th>
<th>Shear Str. (psi)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0.1 (15)</td>
<td>28 (1.1)</td>
<td>0.5</td>
<td>0.5</td>
<td>1998</td>
</tr>
<tr>
<td>2</td>
<td>0.1 (15)</td>
<td>20 (0.8)</td>
<td>0.5</td>
<td>0.5</td>
<td>1863</td>
</tr>
</tbody>
</table>

We claim:
1. An oligomer mixture with self-reactive end-caps comprising the general structure

   E

   Z

   E'

   wherein E and E' are

   Z is

   \[ \begin{array}{c}
   O
   \end{array} \]

   wherein Ar is

2. An oligomer mixture with self-reactive end-caps comprising the general structure
wherein
E and E' are

Z is

wherein Ar₁ and Ar₂ are

3. An oligomer mixture with self-reactive end-caps comprising the general structure

and Z is selected from the group consisting of

where Ar₁ and Ar₂ are

and Ar₃ is