An optical path switch divides sample path radiation into a time series of alternating first polarized components and second polarized components. The first polarized components are transmitted along a first optical path and the second polarized components along a second optical path. A first gasless optical filter train filters the first polarized components to isolate at least a first wavelength band thereby generating first filtered radiation. A second gasless optical filter train filters the second polarized components to isolate at least a second wavelength band thereby generating second filtered radiation. A beam combiner combines the first and second filtered radiation to form a combined beam of radiation. A detector is disposed to monitor magnitude of at least a portion of the combined beam alternately at the first wavelength band and the second wavelength band as an indication of the concentration of the substance in the sample path.
OPTICAL PATH SWITCHING BASED DIFFERENTIAL ABSORPTION RADIOMETRY FOR SUBSTANCE DETECTION

This application is a divisional patent application of commonly owned, patent application Ser. No. 09/290,954, filed Apr. 13, 1999, now U.S. Pat. No. 6,057,923.

ORIGIN OF THE INVENTION

The invention described herein was made by an employee of the United States Government and may be manufactured and used by or for the Government for governmental purposes without the payment of any royalties thereon or therefor.

CLAIM OF BENEFIT OF PROVISIONAL APPLICATION

Pursuant to 35 U.S.C. Section 119, the benefit of priority from provisional application 60/082,355, with a filing date of Apr. 20, 1998, is claimed for this non-provisional application.

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention relates to substance detection using optical systems. More specifically, the invention is a method for detecting the presence and/or concentration of a substance in a sample path using polarization-modulated optical path switching and the principles of differential absorption radiometry.

2. Description of the Related Art

Gas filter correlation radiometers (GFCRs) infer the concentration of a gas species along some sample path either external or internal to the GFCR. In many GFCRs, gas sensing is accomplished by viewing alternately through two optical cells the emission/absorption of the gas molecules along the sample path. These two optical cells are called the correlation and vacuum cells. The correlation cell contains a high optical depth of gas species i that strongly absorbs radiation at specific molecular transition wavelengths of the particular gas while passing all other wavelengths. In effect, the correlation cell defines a plurality of spectral notches (i.e., strong attenuation) coincident with the band structure of gas species i. The vacuum cell generally encloses a vacuum or a gas or gas mixture exhibiting negligible or no optical depth, e.g., nitrogen, an inert gas, or even clean dry air. An optical filter (e.g., interference filter) placed in front of the instrument or in front of the detector limits the spectral information to a region coinciding with an absorption band of the gas of interest. The difference in signal strength between these two views of the emitting/absorbing gas species i can be related to the concentration of this gas along the sample path.

A known GFCR for measuring concentration of a single gas is disclosed in U.S. Pat. No. 5,128,797, issued to Sachse et al. and assigned to the National Aeronautics and Space Administration (NASA). In this system each optical path contains one or more cells with each cell having spectral features of one or more gases of interest. The two optical paths are then intersected to form a combined polarization modulated beam which contains the two orthogonal components in alternate order. The combined polarization modulated beam is partitioned into one or more smaller spectral regions of interest where one or more gases of interest has an absorption band. The difference in intensity between the two orthogonal polarization components in each partitioned spectral region of interest is then determined as an indication of the spectral emission/absorption of the light beam along the sample path. The spectral emission/absorption is indicative of the concentration of the one or more gases of interest in the sample path.

Both of the aforesaid systems require the use of gas correlation cells. However, there are instances where gas correlation cells are not practical. For example, some gases are too dangerous and/or require a gas correlation cell construction that is too expensive for a particular application. Further, some gases such as ozone are too reactive to contain in a gas cell. Still further, it may also be desirable to detect/measure a broad category of gases, e.g., hydrocarbons. However, to accomplish this with a GFCR system, many gases would have to be contained within one cell or the beam would have to be passed through multiple gas cells. This complicates construction and adds to overall system expense. Still further, gas correlation cells are not useful for measuring spectral absorption characteristics of solids or liquids because these substances have broad absorption features.

SUMMARY OF THE INVENTION

Accordingly, it is an object of the present invention to detect/measure any type of substances (i.e., gas, liquid or solid) in a non-mechanical optical fashion without the need for gas correlation cells.

Another object of the present invention is to provide a method and system for detecting/measuring broad categories of gases using optical path switching techniques. Other objects and advantages of the present invention will become more obvious hereinafter in the specification and drawings.

In accordance with the present invention, a system and method are provided for detecting one or more substances.
An optical path switch receives radiation passing along a measurement or sample path of interest. The switch divides the radiation into a time series of alternating first polarized components and second polarized components that are orthogonal to the first polarized components. The first polarized components are transmitted along a first optical path and the second polarized components along a second optical path. A first gasless optical filter train disposed in the first optical path filters the first polarized components to isolate at least a first wavelength band thereby generating first filtered radiation. A second gasless optical filter train disposed in the second optical path filters the second polarized components to isolate at least a second wavelength band thereby generating second filtered radiation. The first wavelength band and second wavelength band are unique. Further, spectral absorption of a substance of interest is different at the first wavelength band as compared to the second wavelength band. A beam combiner disposed to receive the first and second filtered radiation combines same to form a combined beam of radiation. A detector is disposed to monitor magnitude of at least a portion of the combined beam at the first wavelength band and the second wavelength band as an indication of the concentration of the substance in the sample path.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic representation of one embodiment of a substance detection system according to the present invention;

FIG. 2 is a graphical illustration of the filter characteristics of the bandpass filters used in the FIG. 1 embodiment;

FIG. 3 is a schematic representation of another embodiment of the present invention in which two substances can be detected/measured simultaneously;

FIG. 4 is a graphical illustration of the filter characteristics of the bandpass filters used in the FIG. 3 embodiment;

FIG. 5 is a schematic representation of another embodiment of the present invention in which bandpass filters are used in reflection;

FIG. 6A is a graphical illustration of one filter’s characteristics used in the FIG. 5 embodiment;

FIG. 6B is a graphical illustration of the other filter’s characteristics used in the FIG. 5 embodiment;

FIG. 6C is a graphical illustration of a bracketing bandpass filter’s characteristics used in the FIG. 5 embodiment;

FIG. 6D is a graphical illustration of the spectral information reaching the detector in the FIG. 5 embodiment;

FIG. 7 is a schematic representation of another embodiment of the present invention in which differential absorption measurements and gas filter correlation radiometry (GF CR) measurements are made simultaneously;

FIG. 8 is a schematic representation of another embodiment in which two substances can be detected/measured simultaneously using bandpass filters in reflection;

FIG. 9 is a schematic representation of another embodiment in which three substances can be detected/measured simultaneously; and

FIG. 10 is a schematic representation of another embodiment of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

Referring now to the drawings, and more particularly to FIG. 1, one embodiment of a substance detection system according to the present invention is shown and referenced generally by numeral 10. By way of example, the present invention will be described as it relates to the detection, measurement and/or characterization of substances in the gaseous state. However, the present invention can be used to detect, measure and/or characterize any substance, i.e., gas, liquid or solid, that exhibits spectrally varying absorption characteristics.

System 10 includes an optics system 12, e.g., a telescope or other lens/mirror system, that collects light from a radiation source 11 such as the earth and atmosphere when system 10 is mounted on a satellite or aircraft, a blackbody when system 10 is used as a laboratory or in-situ instrument, the sun, a laser, etc. Radiation from source 11 generally comprises both vertically polarized components V and horizontally polarized components H. The radiation passes between source 11 and system 10 along a sample path SP. The presence of a substance or substances of interest along path SP may affect the radiation in a way that can be detected, measured and/or characterized by system 10.

An optical path switch provided after optics system 12 includes an optical polarizer 14, an optical waveplate 16, a polarization modulator 18 and a polarization beamsplitter 20. Such an optical path switch is disclosed in detail in the afore-mentioned U.S. Pat. No. 5,128,797 to Sachse et al., and will therefore only be described briefly herein.

Optical polarizer 14 is provided after the optics system 12 and is aligned to polarize the incoming radiation in the desired fashion, e.g., vertically in the embodiment depicted in FIG. 1. Polarization modulator 18 (e.g., a photo-elastic modulator) then receives the incident vertically polarized beam and rapidly modulates the output beam between vertical and horizontal polarization. Depending on the measurement application and the type of polarization modulator utilized, the polarization modulation frequency may range from near direct current (DC) to radio frequencies (RF). The polarization modulator may be used in conjunction with optical waveplate 16. The output of modulator 18 is a time series of alternating vertically polarized components V and horizontally polarized components H as illustrated in FIG. 1. The switching frequency between V and H is determined by the modulation frequency of modulator 18.

Polarization beamsplitter 20 non-mechanically switches the polarization modulated output beam between two paths by, for example, transmitting the beam along path 101 when it is vertically polarized and reflecting it along path 102 when it is horizontally polarized. Alternatively, beamsplitter 20 may be oriented so as to reflect vertically polarized light and to transmit horizontally polarized light. Thus, beamsplitter 20 rapidly diverts the radiation beam alternately between optical paths 101 and 102 depending on the rapidly time-varying state of polarization which is controlled by modulator 18. Note that although paths 101 and 102 are illustrated as being perpendicular to one another, this need not be the case as will be apparent in other embodiments of the present invention described later below.

The radiation beam transmitted along optical path 101 is incident on a gasless optical bandpass filter 22 configured to transmit only a wavelength band of radiation centered at λa while reflecting other wavelengths. The radiation beam transmitted along optical path 102 is incident on a second gasless optical bandpass filter 24 configured to transmit only a wavelength band of radiation centered at λb while reflecting other wavelengths. Filters 22 and 24 are selected/constructed such that the bands centered at λa and λb are unique as illustrated in FIG. 2. Further, the spectral absorp-
tion of the substance to be detected, measured and/or charac-
terized must be different at the two bands. The greater the
difference in spectral absorption characteristics between
the two bands, the greater the measurement sensitivity of system
10. Accordingly, in an example of the ideal case, spectral
absorption occurs only in the band centered at \( \lambda_A \) (i.e.,
spectral absorption in the band centered at \( \lambda_B \) would be
zero). However, it is to be understood that the present
invention will work as long as there is some difference in
spectral absorption (of the substance of interest) between
the two bands.

The resulting filtered radiation beams passed along optical
paths 101 and 102 are directed/reflected by mirrors 26 and
28, respectively, to a polarization beam combiner 30 (e.g., a
polarization beamsplitter). Beam combiner 30 outputs a
single beam along path 103 in which the beam’s polarization
state varies in time at the fundamental frequency (and
harmonics thereof) of modulator 18. In other words, the
output of beam combiner 30 is essentially a time series that
alternates between the vertically polarized components \( V \)
passed by filter 22 and the horizontally polarized components
passed by filter 24. The combined radiation beam passes
along optical path 103 and is focused by focusing optics
19 onto a detector 34 which is sensitive to the
magnitude of the radiation. Because this radiation is in the
form of an alternating time series, detector 34 is essentially
viewing an amplitude modulated signal. This is because a
gas (or other substance) present along sample path SP absorbs
radiation from radiation source 11 differentially at the
bands centered at \( \lambda_A \) and \( \lambda_B \). Thus, the differential
absorption experienced by the radiation traversing sample
path SP is viewed by detector 34 as an amplitude modulated
signal. The magnitude of the amplitude modulated signal at
the polarization modulation frequency (or its harmonics) is
related to the amount or concentration of the substance of
interest in sample path SP. Note that if system 10 is subject
to changes in the incident radiation due to variations in
strength of radiation source 11, turbulence noise, scattering
along the optical paths, etc., it may be desirable to normalize
the amplitude modulated signal sensed by detector 34. If this is the case, the amplitude modulated signal can be divided by
the DC component sensed by detector 34 as is well
known in the art.

By way of illustrative example, the present invention will be
described briefly for its use in the measurement of
hydrocarbons. In this case, filter 22 is chosen so that the
band centered at \( \lambda_A \) coincides with the carbon-hydrogen
bond absorption typical of hydrocarbons (i.e., \( \lambda_A \) is approxi-
mately 3.4 microns). Filter 24 is chosen so that the band
centered at \( \lambda_B \) coincides with a wavelength band that is
relatively free from hydrocarbon absorption (i.e., \( \lambda_B \) is approximately 5.0 microns). By monitoring the magnitude
of the amplitude modulated signal sensed by detector 34, the
absorption by hydrocarbons present in sample path SP can be
detected and measured in a simple fashion, i.e., multiple
GC/IR devices with multiple gas filter correlation cells (e.g.,
one for each hydrocarbon of interest) are not required.

Although described relative to the embodiment in FIG. 1,
the present invention is not so limited. For example, another
embodiment of a substance detection system in accordance
with the teachings of the present invention is shown and
referenced generally by numeral 200 in FIG. 3. Like reference
d numerals will be used for those elements that are the
same as those used in the FIG. 1 embodiment. The embodiment
in FIG. 3 is similar to that in FIG. 1 except that filters
22 and 24 are replaced with dual bandpass filters 220 and
224, respectively. Specifically, filter 220 passes unique
wavelength bands centered at \( \lambda_A \) and \( \lambda_B \) to mirror 26
with other wavelengths being reflected. Filter 224 passes unique
wavelength bands centered at \( \lambda_A \) and \( \lambda_B \) to mirror 28
with other wavelengths being reflected. The bandpass character-
istics of filters 220 and 224 are illustrated in FIG. 4. As in
the previous embodiment, filter 220 can be configured so
that the bands centered at \( \lambda_A \) and \( \lambda_B \) coincide with radia-
tion bands at which first and second substances of interest
are respectively absorbed. Filter 224 can then be configured
so that bands centered at \( \lambda_A \) and \( \lambda_B \) coincide with radiation
bands at which the first and second substances are relatively
free from absorption.

After the radiation beams are combined at beam combiner
30, the combined beam is directed along optical path 103 to
a partitioning or edge filter 226 configured, for example, to
reflect wavelength bands centered at \( \lambda_A \) and \( \lambda_B \) through
focusing optics 32 onto a detector 34 which is sensitive to the
differential absorption experienced by the radiation traversing
sample path SP and is focused by focusing optics 30 onto a detector 34 which is sensitive to the
wavelength bands centered at \( \lambda_A \) and \( \lambda_B \) through focusing optics 30 onto a detector 34 which is sensitive to the
wavelength bands centered at \( \lambda_A \) and \( \lambda_B \) through focusing optics 30 onto a detector 34 which is sensitive to the
diffusion band pass filter 326 having a band pass characteristic that spans the two wavelength bands isolated by filters 320 and
324. The bandpass characteristics of filters 320 and 324 are illustrated in FIG. 4. The diffusion band pass filter 326 having a band pass characteristic that spans the two wavelength bands isolated by filters 320 and
324. The transmission characteristics of bracketing bandpass
filter 326 are illustrated in FIG. 6C. Note that bracketing
filter 326 could be replaced with a dual bandpass filter.
Either way, focusing optics 32 and detector 34 receive a
signal magnitude affected by absorption in the two bands
illustrated in FIG. 6D. Since each band is alternately
received by detector 34, an amplitude modulated signal is
monitored. The advantages of the FIG. 5 embodiment
include fewer components and the preservation of the major-
ty of the radiation for further processing as will now be
described with the aid of FIG. 7. The present invention could also be practiced by using dual (or triple) bandpass filters (in
place of filters 320 and 324) and wavelength partitioning
The embodiment illustrated in FIG. 7, and referenced generally by numeral 400, is used to make differential absorption and gas filter correlation measurements simultaneously. As before, like reference numerals are used for elements that are common with the FIG. 5 embodiment. System 400 is useful in measurement applications that require both high measurement specificity for certain gas species and the measurement of a broad class of gases. An example is the remote measurement of carbon dioxide. In this measurement, high gas specificity is needed to accurately measure NO because of the overlap of a strong water vapor band at 5.2 microns. At the same time, a "total hydrocarbon" measurement is desired in the 3.4 micron carbon-hydrogen absorption region. In other words, the measurement of a specific hydrocarbon is not desired. Rather, the measurement of the net differential absorption in this C-H stretch region is desired as some indication of "total hydrocarbons". Such conflicting types of simultaneous measurements are possible in the present invention. That is, the present invention makes it possible to use the GFCR technique for the NO measurement and the differential absorption technique for the "total hydrocarbon" measurement.

In FIG. 7, a gas correlation cell 440 is disposed in optical path 101 and a vacuum cell 444 is disposed in optical path 102. Cells 440 and 444 enable a GFCR measurement while filters 320 and 324 enable the differential absorption measurement as described above with reference to FIG. 5. More specifically, the radiation beams are combined at beam combiner 30. The combined beam is partitioned at edge filter 426 which, for example, transmits the wavelength region associated with the GFCR measurement to a GFCR bandpass filter 446, focusing optics 432 and detector 434 so that a standard GFCR measurement can be made as is well known in the art. Edge filter 426 reflects other wavelengths to bracketing or bandpass filter 326 which functions as in the previous embodiment of FIG. 5.

Another way to detect or measure two substances simultaneously using bandpass filters in reflection is shown and referenced generally by numeral 500 in FIG. 8. That is, system 500 is an alternative construction that achieves the results described above with respect to FIG. 3. In optical path 101, a first bandpass filter 520 reflects all wavelengths except those in a first band centered at $\lambda_{A1}$ towards one side of a two-sided mirror 526. Mirror 526 reflects the radiation to a second bandpass filter 521 that reflects all wavelengths except those in a second band centered at $\lambda_{A2}$. In a similar fashion, bandpass filters 524, 525 and mirror 526 cooperate to remove wavelength bands centered at $\lambda_{B1}$ and $\lambda_{B2}$ in optical path 102. The single beam output from beam combiner 30 can then be processed as described in the FIG. 3 embodiment. Detection optics may include bracketing filters 326 as needed.

Still another embodiment of the present invention is shown in FIG. 9 and is referenced generally by numeral 600. System 600 is similar to system 500 except that mirror 526 is replaced with a two-sided bandpass absorber 626. Absorber 626 is configured on side 626A to absorb radiation in a third wavelength band centered on $\lambda_{A3}$ while reflecting all other wavelengths. This can be accomplished by designing a bandpass filter stack that transmits the band centered at $\lambda_{A3}$, which is then absorbed internally. For example, the substrate material could strongly absorb this wavelength band. On the other side 626B of absorber 626 is a second filter stack that selectively transmits/absorbs a wavelength band centered at $\lambda_{B3}$. After being combined at beam combiner 30, a system of partitioning filters/focusing optics/detectors 632, similar to the systems disclosed in the embodiments of FIGS. 3, 7 and 8, are used to partition the single beam so that the differential absorption between each wavelength band pair (i.e., wavelength band pairs centered at $\lambda_{A1}$ and $\lambda_{B1}$, $\lambda_{A2}$ and $\lambda_{B2}$, and $\lambda_{A3}$ and $\lambda_{B3}$) can be individually and simultaneously sensed.

In still another embodiment of the present invention, system 700 illustrated in FIG. 10 is an alternative construction for the FIG. 5 embodiment. System 700 is a compact configuration of the present invention in which optical path 103 exits a combination beamsplitter/combiner 750 at an acute angle thereto. A single optical element can be used for beamsplitting and beam combining by, for example, configuring the device's wire grids (not shown) to transmit horizontal polarization in the beamsplitter portion and to transmit vertical polarization in the beam combiner portion. The advantages of the present invention are numerous. Substance detection and measurement can be achieved without using gas cells. However, the present invention can be configured to provide for simultaneous differential absorption and GFCR measurements. Further, multiple differential absorption measurements associated with multiple substances can be made simultaneously.

Although the invention has been described relative to a specific embodiment thereof, there are numerous variations and modifications that will be readily apparent to those skilled in the art in light of the above teachings. It is therefore to be understood that, within the scope of the appended claims, the invention may be practiced other than as specifically described.

What is claimed as new and desired to be secured by Letters Patent of the United States is:

1. A method of detecting a substance, comprising the steps of:
   receiving radiation passing along a sample path of interest;
   dividing said radiation into a time series of alternating first polarized components and second polarized components orthogonal to said first polarized components; routing said first polarized components along a first optical path and said second polarized components along a second optical path;
   reflecting all wavelengths of said first polarized components except at least a first wavelength band wherein first filtered radiation excluding said at least first wavelength band is generated;
   filtering said second polarized components to isolate at least a second wavelength band wherein second filtered radiation is generated, wherein said first wavelength band and said second wavelength band are unique and wherein spectral absorption of a substance of interest is different at said first wavelength band as compared to said second wavelength band;
   combining said first filtered radiation and said second filtered radiation to form a combined beam of radiation; and
   monitoring magnitude of said combined beam alternately at said first wavelength band and said second wavelength band as an indication of the concentration of said substance in said sample path.

2. A method according to claim 1 further comprising the step of performing gas filter correlation radiometry using one of said first polarized components and said first filtered radiation, and using one of said second polarized components and said second filtered radiation.
3. A method according to claim 1 wherein all wavelengths of said first polarized components are reflected except a plurality of unique first wavelength bands whereby said first filtered radiation excludes said plurality of first wavelength bands, and wherein said step of filtering said second polarized components comprises isolating a plurality of unique second wavelength bands wherein second filtered radiation is generated, said method further comprising the step of: partitioning said combined beam into a plurality of partitioned beams, each of said plurality of partitioned beams comprising first filtered radiation and second filtered radiation, said first filtered radiation having excluded therefrom one of said plurality of unique first wavelength bands, wherein spectral absorption of a substance of interest is different at said one of said plurality of unique first wavelength bands as compared to one of said plurality of unique second wavelength bands, wherein said step of monitoring comprises the step of monitoring magnitude of each of said plurality of partitioned beams.

4. A method according to claim 1 wherein a plurality of related substances of interest are spectrally absorbed more at said first wavelength band than at said second wavelength band.

5. A method according to claim 4 wherein said plurality of related substances are hydrocarbons.

6. A method according to claim 1 wherein said first polarized components are vertically polarized and said second polarized components are horizontally polarized.

7. A method according to claim 1 wherein said step of monitoring is harmonically synchronized to a frequency at which said time series alternates between said first polarized components and said second polarized components.

8. A method of detecting a substance, comprising the steps of:
   - receiving radiation passing along a sample path of interest;
   - in dividing said radiation into a time series of alternating first polarized components and second polarized components orthogonal to said first polarized components; routing said first polarized components along a first optical path and said second polarized components along a second optical path;
   - reflecting all wavelengths of said first polarized components except at least a first wavelength band wherein first filtered radiation excluding said first wavelength band is generated;
   - reflecting all wavelengths of said second polarized components except at least a second wavelength band wherein second filtered radiation excluding said second wavelength band is generated;
   - combining said first filtered radiation and said second filtered radiation to form a combined beam of radiation; transmitting the combined beam to a filter having a band pass characteristic that spans said excluded first and second wavelength bands; and
   - monitoring magnitude of said combined beam received from the filter alternately at said first wavelength band and said second wavelength band as an indication of the concentration of said substance in said sample path.

9. A method according to claim 9 further comprising the step of performing gas filter correlation radiometry using one of said first polarized components and said first filtered radiation, and using one of said second polarized components and said second filtered radiation.

10. A method according to claim 9 wherein all wavelengths of said first polarized components are reflected except a plurality of unique first wavelength bands whereby said first filtered radiation excludes said plurality of first wavelength bands, and wherein all wavelengths of said second polarized components are reflected except a plurality of unique second wavelength bands whereby said second filtered radiation excludes said plurality of second wavelength bands, said method further comprising the step of:
    - partitioning said combined beam into a plurality of partitioned beams, each of said plurality of partitioned beams having excluded therefrom one of said plurality of unique first wavelength bands and one of said plurality of unique second wavelength bands, wherein spectral absorption of a substance of interest is different at said one of said plurality of unique first wavelength bands as compared to one of said plurality of unique second wavelength bands, wherein said step of monitoring comprises the step of monitoring magnitude of each of said plurality of partitioned beams.