The invention discloses a semi-ring Fabry-Perot (SRFP) optical resonator structure comprising a medium including an edge forming a reflective facet and a waveguide within the medium, the waveguide having opposing ends formed by the reflective facet. The performance of the SRFP resonator can be further enhanced by including a Mach-Zehnder interferometer in the waveguide on one side of the gain medium. The optical resonator can be employed in a variety of optical devices. Laser structures using at least one SRFP resonator are disclosed where the resonators are disposed on opposite sides of a gain medium. Other laser structures employing one or more resonators on one side of a gain region are also disclosed.

20 Claims, 32 Drawing Sheets
FIG. 1C

FIG. 1D
FIG. 1E

FIG. 1F
FIG. 2B
FIG. 2C
1

OPTICAL RESONATOR

CROSS-REFERENCE TO RELATED APPLICATIONS

This continuation application claims the benefit under 35 U.S.C. §120 of the following co-pending U.S. Patent Application, which is incorporated by reference herein:


STATEMENT OF GOVERNMENT RIGHTS

The invention described herein was made in the performance of work under a NASA contract, and is subject to the provisions of Public Law 96-517 (35 U.S.C. 202) in which the Contractor has elected to retain title.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to optical devices and methods for producing and operating them. Particularly, the present invention relates to optical resonators and their applications in tunable semiconductor lasers.

2. Description of the Related Art

In recent years, the development of optical devices for various applications such as tunable semiconductor lasers has received much attention. For example, fiber optic communication systems employ widely tunable semiconductor lasers in wavelength division multiplexing applications. Accordingly, various forms of tunable semiconductor lasers and related devices have been developed.

Many of the developed tunable semiconductor lasers require relatively complex manufacturing processes and may employ grating structures and/or moving components. In addition, multiple optical couplers in many tunable semiconductor lasers can reduce the overall performance, such as indicated by the mode suppression ratio (MSR).

Two fundamental types of optical resonators are the Fabry-Perot cavity and the ring resonator. The Fabry-Perot cavity comprise two parallel reflective planes separated by a distance. Resonance (constructive interference of the reflected light) occurs for specific wavelengths of light reflected between the reflective planes when the distance between the planes is an even multiple of the light wavelength. Thus, the pattern for resonance is periodic across wavelengths. Reflective gratings have also been used in the place of the reflective planes achieve similar results. In addition, ring resonators establish resonance in a similar manner, but the critical distance is defined by the circumference of circular waveguide rather than the separation between two reflective planes. Both fundamental types of optical resonators have been used in a vast number of various optical devices such as tunable lasers. However, both types present different manufacturing and design difficulties in their use. For example, conventional Fabry-Perot resonators are typically constrained (or are constrained by) other device parameters, e.g., the gain medium length must coincide with the length of the Fabry-Perot cavity. The use of ring resonators is often complicated by the need for multiple coupling regions.

There is a need for optical resonators which are simple to manufacture and can be used in the production of optical devices such as tunable semiconductor lasers. Further, there is a need for optical resonators which can be implemented with fewer manufacturing and design constraints. There is also a need for tunable semiconductor lasers which operate without grating structures or moving components. As detailed hereafter, the present invention possesses these and other advantages.

SUMMARY OF THE INVENTION

The present invention discloses a novel optical resonator that can be employed in new classes of widely tunable semiconductor lasers and other optical devices. Embodiments of the invention have the advantage of requiring only simple planar fabrication technology. Thus, embodiments of the invention require no grating structure or moving parts. Using a complex field approach, it can be demonstrated that relatively wide tunability, high optical power and a large mode suppression ratio (MSR) can be achieved through a careful design employing this simple architecture. The MSR exhibited by embodiments of the invention (even in the case of low, e.g. approximately 3 dB, coupling between the gain chip and the tunable mirror) is still higher than that obtained with standard designs of tunable lasers based on interferometer techniques. Such standard designs exhibit typical MSRs around 30 dB to 40 dB.

The novel optical resonator of the present invention, hereafter referred to as a semi-ring Fabry-Perot (SRFP) resonator comprises a medium including an edge forming a reflective facet and a waveguide within the medium, the waveguide having opposing ends formed by the reflective facet. The performance of the optical resonator can be further enhanced by including a Mach-Zehnder interferometer in the waveguide. The SRFP exhibits its own reflection spectra having a substantially uniform peak transmission at all resonant peaks. The free spectral range of a SRFP is related to its optical length. Accordingly, tuning can be achieved by shifting the peaks by an adjustment of the index of refraction in at least a portion of the SRFP waveguide through current injection.

The SRFP can be employed in a variety of optical devices, such as a semiconductor laser where the resonator is coupled through a coupling region to a gain medium within a Fabry-Perot cavity. A typical laser embodiment of the invention comprises a gain chip including at least one tunable filter element including the novel resonator. There are different acceptable techniques for coupling the gain medium to the tunable feedback element. However, the nature of the coupling is not important for an analytical study of the device.

Some advantages of the SRFP resonator over a conventional ring resonator are that the SRFP resonator supports standing waves and a larger waveguide bending curvature can be used, reducing potential bending losses. Also, the SRFP resonator uses only one coupling region in order to couple back to the gain medium. In addition, one advantage of the SRFP over a conventional Fabry-Perot cavity resonator is the use of only one plane mirror for both reflecting
facets. This eases the fabrication of the resonator; the length of the SRFP resonator can greatly differ from that of the chip and the SRFP resonator can be tuned for optimum frequency selection. This yields the further advantage that the FSR of the SRFP resonator is not strongly dictated by fabrication requirements, as it is in the case of conventional Fabry-Perot resonators.

In one exemplary embodiment, the tunable filter element within the gain chip can be constructed by the combination of a Mach-Zehnder interferometer (MZI) within the SRFP inside a Fabry-Perot cavity. The Fabry-Perot cavity includes a waveguide comprising two opposing ends which conclude at a common high reflection facet, forming the SRFP. A coupling region interrupts the waveguide and couples it to the gain medium within the device. The MZI, having a large free spectral range, is included in the waveguide on one side of the coupling region and selects a particular wavelength region within the gain bandwidth. However, this interferometer does not provide sufficient discrimination between neighboring cavity modes. See e.g., Amann, Markus-Christian et al., "Tunable Laser Diodes", Artech House Publishers, 1998; Kuznetsov, M. et al., "Widely tunable 850 nm TE10 laser diode with improved wavelength access", Electronics Letters, Vol. 30, 1994, pp. 2047–2049. Therefore, the SRFP with a small free spectral range selects a particular cavity mode within the wavelength region selected by the MZI. The frequency tunability is obtained by changing the difference of optical length between the two arms of the MZI; the SRFP defines the finesse of the reflector.

In addition, in further embodiments of the invention detailed hereafter multiple resonators, and particularly SRFP resonators, are used to produce tunable lasers. Further embodiments of the invention include a novel class of tunable semiconductor lasers using the Vernier technique where the two resonators are localized in the same side of the gain medium. These devices can exhibit both high tunability through application of the Vernier technique and high power because the two resonators are localized in the same side of the gain medium.

In still further embodiments of the invention, other novel laser structures are also disclosed which do not employ the semi-ring Fabry-Perot resonator.

BRIEF DESCRIPTION OF THE DRAWINGS

Referring now to the drawings in which like reference numbers represent corresponding parts throughout:

FIG. 1A illustrates a top view of an optical resonator of the invention;

FIG. 1B illustrates a top view of an optical resonator of the invention including a Mach-Zehnder interferometer;

FIG. 1C illustrates a frequency selective mirror device comprising a MZI and a mirror;

FIG. 1D qualitatively illustrates the reflection output of the frequency selective mirror device using the MZI with respect to frequency;

FIG. 1E qualitatively illustrates the reflectance of the SRFP of the present invention;

FIG. 1F qualitatively illustrates the combined response of the MZI and the SRFP resonator;

FIG. 2A illustrates a top view of a tunable laser embodiment of the present invention including a tunable element having two waveguides, a MZI and a reflective facet;

FIG. 2B illustrates a top view of a second tunable laser embodiment of the present invention including a tunable element having a ring resonator and a MZI;

FIG. 2C illustrates a top view of a structural variant of the FIG. 2B embodiment of the present invention including a tunable element having a ring resonator and a MZI;

FIG. 2D illustrates a top view of a third tunable laser embodiment of the present invention including a tunable element having two waveguides, a MZI and a reflective facet;

FIG. 2E illustrates a top view of a fourth tunable laser embodiment of the present invention including a tunable element having three waveguides and a reflective facet;

FIG. 2F illustrates a top view of a fifth tunable laser embodiment of the present invention including a SRFP tunable element having two waveguides, a ring resonator and a reflective facet;

FIG. 3 illustrates the intensity coming back from the tunable frequency element versus frequency of the exemplary embodiment of FIG. 2A;

FIG. 4 is a plot of the Mode Suppression Ration (MSR) versus the current in Amperes for the exemplary embodiment of FIG. 2A;

FIG. 5 is a plot of the output power in Watts versus the input current in Amperes for the exemplary embodiment of FIG. 2A;

FIG. 6A illustrates a laser class including two optical resonators on opposing sides of a gain medium;

FIG. 6B illustrates a laser including two SRFP optical resonators on opposing sides of a gain medium;

FIG. 6C–6F are exemplary plots of the spectra of the light reflected from the resonator for different values of back reflection coefficients and high facet reflections;

FIG. 6G illustrates a further embodiment where one of the SRFP resonators is replaced by a ring resonator;

FIG. 7A illustrates a laser class including two optical resonators on the same side of a gain medium;

FIGS. 7B–7J illustrate various exemplary laser embodiments of the class of FIG. 7A; and

FIGS. 8A & 8B illustrate hybrid classes of the lasers of FIGS. 6A and 7A.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

In the following description of the preferred embodiment, reference is made to the accompanying drawings which form a part hereof, and in which is shown by way of illustration a specific embodiment in which the invention may be practiced. It is to be understood that other embodiments may be utilized and structural changes may be made without departing from the scope of the present invention.

1. Semi-ring Fabry-Perot Resonator

FIG. 1A illustrates a novel optical resonator of the present invention. The resonator 100, a semi-ring Fabry-Perot (SRFP) resonator 100, comprises a medium 102 (such as a semiconductor material) including an edge forming a reflective facet 106 and a waveguide 104 within the medium, the waveguide having opposing ends 108A, 108B formed by the reflective facet 106. The resonator 100 behaves similar to a Fabry-Perot resonator with some additional advantageous properties. For example, manufacturing of the resonator 100 is simplified because only a single facet 106 is cut to produce
that the MZI 110 can be positioned on either side of the mirror device 120 comprising a MZI 122 and mirror 124, profile, making it possible to have lasing at more than one frequency. In addition, there is no simple technique for tuning over a wide range. In order to better understand the operation of the SRFP resonator 100; conventionally a MZI would be added external to an ordinary Fabry-Perot resonator.

The resonator can be employed as a tunable element by constructing the waveguide 104 (or a portion thereof) such that the optical length is varied by controlled current injection. The current injection changes the index of refraction and therefore the optical length as the device is operated.

FIG. 1B illustrates the optical resonator 100 with the addition of a Mach-Zehnder interferometer (MZI) 110. The addition of the MZI 110 can be used to further enhance the performance and usefulness of the optical resonator 100. The MZI 110 includes an upper arm 112 and a lower arm 114 that are used to establish a path length differential for light entering the MZI 110. The remaining waveguide 116 (which can be considered a continuation of the waveguide 104) is used to couple the light to the reflective facet 106 at its end 108B. Also illustrated is a coupling region 114 which can be used to couple feedback from the resonator 100 to other elements in an optical device. It should be noted that the MZI 110 can be positioned on either side of the coupling region 114 in the resonator 100.

To describe intuitively the tunability mechanism one may look at the performance of the unbalanced MZI 110 and the SRFP resonator 100 individually and then in combination. For an ordinary Fabry-Perot cavity in a laser device, lasing occurs near the top of the gain profile of the gain medium. The cavity typically has a relatively broad gain envelope. The next section presents the theoretical analyses of an exemplary device supporting the foregoing discussion.

FIG. 1C qualitatively illustrates a frequency selective mirror device 120 comprising a MZI 122 and mirror 124, such as a 100% mirrored facet. The MZI 122 alone produces a periodic frequency selectivity to the gain chip 126. Frequency tunability is obtained by changing the difference in optical length between the two arms 128, 130 of the MZI 122, which shifts the mode filtering spectrum of the MZI 122, and consequently changes the lasing mode of the laser 122. The change of the optical length can be induced altering the index of refraction of one or both of the waveguide arms 128, 130 through current injection. Alternately (or in conjunction with tuning by current injection) tuning may be achieved by changing only the phase of the coupling coefficient. Thus, the resonant frequencies of the device to tune the device. So in order to tune the device, it is not required to change the optical length of the resonator. Tuning of the device can also be obtained by techniques which change the phase of the coupling coefficient.

FIG. 1D qualitatively illustrates the reflection output of the frequency selective mirror device 120 using the MZI 122 with respect to frequency. The cavity modes of the laser 132 are also illustrated. However, the MZI 122 has very low finesse. For a given device length, larger free spectral range (FSR) results in a larger tuning range, but at the expense of the selectivity between the main and the side modes. It should noted that devices similar to the one shown in FIG. 1C do not have high MSR due to the low finesse of the MZI (e.g., as in a known Y-branch laser). The MZI 122 used alone therefore does not often provide adequate selectivity. To significantly improve performance, an increase in the MSR while maintaining the wide tuning range is necessary. To obtain this, requires a more selective filtering method. The combination of the SRFP resonator 100 with an MZI 110 as shown in FIG. 1B provides the needed selectivity.

FIG. 1E illustrates the reflectance of the SRFP resonator 100. The SRFP is analyzed in detail in the next section. The behavior of the SRFP resonator 100 can be simulated by a Fabry-Perot cavity. However, the SRFP resonator 100 has the advantage over a standard Fabry-Perot cavity resonator due to the use of only single facet 106 reflectivity. This eases the fabrication of the resonator 100 because the length of the SRFP resonator 100 is disassociated from that of the chip. The FSR of the SRFP resonator 100 is not constrained by fabrication requirements, as it is in the case of a standard Fabry-Perot cavity resonator.

The SRFP resonator 100 also possesses advantages over a standard ring resonator through its support of standing waves. This allows the SRFP resonator 100 to use only one coupling region 114 in order to couple light from the SRFP resonator 100 back to a gain medium in an optical device.

FIG. 1F qualitatively illustrates the combined response of the MZI 110 and the SRFP resonator 100. As shown in FIGS. 1D–1F, the SRFP resonator 100 parameters can be chosen such that the peaks of the SRFP resonator 100 correspond to the peak of the MZI 110 filter, which also corresponds to a cavity mode of the SRFP resonator 100. This main mode, mode 0, will be the lasing mode. Notably, the benefit of the MZI 110 is enhanced by its inclusion within the SRFP resonator 100; conventionally a MZI would be added externally to an ordinary Fabry-Perot resonator.

In order to better understand the operation of the SRFP resonator 100 and MZI 110 filter combination, a worst case can be visualized in which even one of the SRFP resonator 100 peaks correspond to a cavity mode (although other cavity modes may also exist at frequencies between the resonator peaks). The SRFP resonator 100 should be designed in a manner to reduce the strength of all the cavity modes between the main mode and the next SRFP resonator peak. The MZI 110 parameters are now selected to ensure that the next SRFP peak becomes the side mode. Referring to FIG. 1E, we note that for the SRFP, if mode 0 is the lasing mode, mode 1 the next cavity mode and mode 4 the cavity mode which is aligned with the next peak of the ring, after adding the MZI filter inside cavity, mode 4 becomes the side mode of the combined device, as shown in FIG. 1F. In the case of the MZI alone, mode 1 is the side mode as shown in FIG. 1D. With this implementation, therefore the MSR is no longer a function of the ratio of mode 0 over mode 1 but it is a function of the ratio of mode 0 over mode 4, making the MSR is a function of the SRFP resonator FSR and MZI gain envelope. The next section presents the theoretical analyses of an exemplary device supporting the foregoing discussion.

2. Exemplary Embodiments of a Laser Using an SRFP Resonator

FIG. 2A illustrates a top view of a tunable laser embodiment of the present invention including a SRFP tunable element having two waveguides, a MZI and a reflective facet. The tunable laser device 200 comprises a tunable feedback element 202 within a Fabry-Perot cavity 204.
tunable feedback element 202 comprises an optical resonator as described above, a semi-ring Fabry-Perot resonator. The cavity 204 can be defined by the gain (active) medium 206 within a waveguide bounded by reflective facets, a rear facet 208 and a front 210 at opposing ends of the gain medium 206. The rear facet 208, bounding one end of the cavity 204, can include an anti-reflection coating. The front facet 210, bounding the opposing end of the cavity 204, comprises the output of the tunable laser device 200.

The coupling region 212 couples the gain medium 206 and the tunable feedback element 202. In the exemplary embodiment shown, the coupling region 212 is disposed within the gain medium 206 and provides an input and output normalized complex field amplitude from each side of the coupling region 212 to the gain medium 206 toward rear facet 208 on one side and toward front facet 210 on the opposite side. Similarly, the tunable feedback element 202 also receives an input and output normalized complex field amplitude from each side of the coupling region 212 to a first waveguide 214 on one side and to a second waveguide 216 on the opposite side.

In this first exemplary embodiment, the tunable feedback element 202 comprises a Mach-Zehnder interferometer (MZI) 218. The first waveguide 214 of the tunable feedback element 202 provides a path from the coupling region 212 to a high reflection rear facet 220 of the passive medium. The second waveguide 216 of the tunable feedback element 202 provides a path from the coupling region to a first end of the MZI 218. The MZI 218 includes an upper arm 222 and a lower arm 224 that are used to establish a path length differential for light entering the MZI 218. The opposite end of the MZI 218 is coupled to a third waveguide 226 that provides a path from the MZI 218 to the high reflection rear facet 220 of the passive medium. It should be noted that the two waveguides of the described embodiment refer to the first waveguide 214 on one side of the coupling region 212 and the combination of the second and third waveguides 214, 226 that are interrupted by the MZI 218 on opposite of the coupling region 212. Alternately, the tunable feedback element 202 can be structured with the MZI 218 positioned on the first waveguide 214 and the second waveguide 216 coupled directly to the rear facet 220.

It should be noted that facets 208, 210 and 220 are generally formed from each entire respective surface of the device 200. This greatly simplifies the manufacturing process. Thus, rear facet 220 of the passive medium can be formed from the edge surface of the device 200 adjacent to both the surfaces of rear facet 208 of the active medium and front facet 210 of the active medium of the cavity 204. Similarly, the front facet 228 of the passive medium can be formed from the entire edge surface opposite the rear facet 220.

The coupling region 212 between the gain medium 206 and the tunable feedback element 202 can be modeled as follows using a similar approach as in A. Yariv, “Universal relations for coupling of optical power between micro resonators and dielectric waveguides”, Electronics Letters, vol. 36, page 321, 2000, which is incorporated by reference herein, the gain-tunable element coupling region 212 as shown in FIG. 2A, where a, and b, are the input and output, respectively, normalized complex field amplitudes entering and leaving the coupling region 212. Under the condition of lossless coupling, that is, 

\( |K(f)|^2 + |\phi(f)|^2 = 1 \)  

The complex field amplitudes satisfies the following set of equations,

\[
\begin{align*}
& b_1 = za_1 + a_1 + a_2 (b_1 + b_2) \\
& b_2 = za_2 + a_2 + a_3 (b_1 + b_2) \\
& b_3 = a_3 + b_3 (b_1 + b_2) \\
& b_4 = a_4 + b_4 (b_1 + b_2)
\end{align*}
\]

where \( f \) is the frequency of the field, \( t_1(f), t_2(f) \) and \( K_1(f), K_2(f) \) are the transmission and coupling coefficients of the complex field region, respectively. The set of equations (2) can be also written in the matrix form,

\[
\begin{pmatrix}
0 & 0 & t_1(f) & K_1(f)
\end{pmatrix}
\begin{pmatrix}
a_1 \\
a_2 \\
a_3 \\
a_4
\end{pmatrix}
= \begin{pmatrix}
0 & 0 & t_2(f) & K_2(f)
\end{pmatrix}
\begin{pmatrix}
a_1 \\
a_2 \\
a_3 \\
a_4
\end{pmatrix}
\]

The tunable feedback element 202 shown in FIG. 2A can be analyzed as follows. In the structure of FIG. 2A,

\[
\begin{align*}
A &= e^{-j2\pi n_a l_a} e^{j2\pi n_b l_b} e^{j2\pi n_c l_c} e^{j2\pi n_d l_d} e^{j2\pi n_e l_e} \\
\alpha_1 &= 1 - r_1 e^{j2\pi n_a l_a} e^{j2\pi n_b l_b} e^{j2\pi n_c l_c} e^{j2\pi n_d l_d} e^{j2\pi n_e l_e} \frac{1}{z_1}
\end{align*}
\]

where \( \alpha, n_a, n_b, \) and \( \alpha_1 \) are respectively, the loss per unit length, the refractive index and the length of the waveguide 216 and \( \alpha_2, n_c, n_d, \) and \( \alpha_2 \) are the corresponding quantities for the waveguide 224, \( n_e, l_e, \) and \( \alpha_3 \) are respectively the refractive index and the length of the upper arm 222 of the MZI 218 and \( n_f, l_f, \) and \( \alpha_4 \) are the corresponding quantities for the lower arm 224 of the MZI 218. \( r_1 \) is the field reflectivity of the front facet 226 of the passive medium and \( r_4 \) is that of the rear facet 220 of the passive medium.

Since in the rear facet 208 of the active medium is an anti-reflection coating, \( a_1 = 0. \) From equations (3), (4), and (5), one can determine,

\[
\begin{align*}
\frac{b_2}{a_3} &= t_2(f) R_1 + K_2(f) R_{2245} + K_5(f) R_{2245} - t_2(f) R_{2245} \\
\text{where,} \quad R_1 &= -r_1, \\
R_{2245} &= \frac{R_2(K_2, f) R_1 t_2(f) + t_2(f) R_2(K_2, f)}{1 - R_2(K_2, f) R_1 t_2(f) - R_2(K_2, f) R_1 t_2(f)} \\
A &= e^{-j2\pi n_a l_a} e^{j2\pi n_b l_b} e^{j2\pi n_c l_c} e^{j2\pi n_d l_d} e^{j2\pi n_e l_e} \frac{1}{z_1}
\end{align*}
\]

In the case of a tunable laser for WDM applications, one can neglect the frequency dependence of the coupling region over the working frequency range to obtain a rough approximation. Accordingly, it follows that,
The resonant frequency \( f_r \) of the tunable element has to satisfy equation (11), which implies,

\[
\cos^2 \left( \frac{E}{c} f_r (n_u L_u - n_d L_d) \right) = 1,
\]

where

\[
D = \Phi_f - \Phi_2.
\]

Equation (12)

and the resonator length.

The ring resonator provides another set of resonator frequencies. The combined resonant frequency of the tunable element has to equal \( f = \frac{f_i + f_s - f_r}{2} + \Delta f \).

The following result is obtained,

\[
\frac{b_3}{a_1} = K_1 - K_2, \quad G = e^{2(\alpha_3 L_3 + \alpha_4 L_4)}, \quad H = \frac{b_3}{a_1} \cdot L_3 \cdot \cos \left( \frac{\pi f_i}{c} (n_u L_u - n_d L_d) \right).
\]

If \( \Delta f \) is defined through the relation,

\[
f = f_i + f_s - f_r + \Delta f,
\]

the following result is obtained,

\[
K_i = |K_i| e^{i \Phi_i}, \quad f_s = |f_s| e^{i \Phi_s}
\]

\[
f_r = \Phi_f - \Phi_2.
\]
produce a widely tunable single-mode laser as described in FIG. 2A. Although embodiments of the invention can be constructed as hybrid devices with distinct elements separately fabricated and integrated together, the invention can advantageously be used to form optical devices through monolithic fabrication, in a simpler, cost-effective manner.

One can examine a specific design in which the active medium is a III-V material system operating at approximately 1.55 µm wavelength. For this specific exemplary numerical application, a 111-V material system operating at approximately 1,248 GHz (equivalent to a tunability range of approximately 1,248 GHz (10 nm)) is chosen. A fine wavelength selection of approximately 50 GHz is considered. This is the frequency difference between two consecutive frequencies of the laser channels and, in turn, corresponds to the total combined length of waveguide 114, waveguide 116 and waveguide 124 of approximately 1 mm.

It can also be assumed that the gain medium is substantially removed from the tunable filter so that the waveguide loss reaches a maximum value of approximately 10 dB/cm, r1, r2 and r3 are substantially equal and equal to approximately 0.97, and K1 and K2 are substantially equal and equal to 0.7. The main reflection of the tunable filter is taken to correspond to a cavity mode, which is the laser mode. The 10 dB/cm loss is applied as a worst-case estimate for evaluation purposes; realistic losses are significantly lower in many applications, depending upon manufacturing and other considerations.

Referring to FIG. 2A, it is also assumed that the separation of the cavity modes is such that the reflection of the adjacent cavity mode from the tunable filter element 202 is lower than that of the cavity mode, coinciding with the next strongest reflection peak of the tunable filter element 202. In the calculation of the MSR, a worst-case scenario is assumed in which both the strongest and next strongest field reflection peak spectrum of the tunable filter element 202 correspond to a cavity mode. The contribution of the filter reflection to the energy stored in each mode only is included in order to calculate the single contribution of the tunable filter element 202 in the MSR. This means that these calculations represent a pessimistic view where the same gain is present both for the main and side mode.

FIG. 3 illustrates the intensity coming back from the tunable frequency element versus frequency of the exemplary embodiment of FIG. 2A. A fine wavelength selection FSR of approximately 50 GHz and a MZI FSR of approximately 1,248 GHz are applied. In addition, an intensity coupling between the gain-tunable element of approximately 0.49 and a waveguide loss of approximately 10 dB/cm are also used.

The considered gain medium parameters of the exemplary embodiment of FIG. 2A are approximately 0.2 µm thickness, 3 µm width, 300 µm length and a material loss of approximately 80 cm⁻¹. The gain versus carrier density characteristic of the active medium is associated with a transparency carrier of approximately 5x10⁻¹⁵ cm⁻³.

According to L. Coldren et al., "Diode Lasers and Photonic Integrated Circuits", p. 45, 1995, which is incorporated by reference herein, the threshold current is given by,

\[ I_{th} \approx \frac{2V_{FB}^{2}}{\eta_{0}} \exp \left( \frac{2(\alpha_{s} + \alpha_{m})}{\eta_{0}} \right). \]

where \( V \) is the volume of the device, \( \eta_{0} \) the quantum efficiency (in our case its value is approximately 0.7), \( N_{0} \) is the transparent carrier density, \( \alpha_{s} \) is the gain medium intrinsic loss, \( 2 \times 10^{9} \text{ cm}^{-1} \), \( B \) the bimolecular recombination coefficient (usually \( B = 10^{-10} \text{ cm}^{-3} \text{s}^{-1} \) for most III-V materials of interest). A passive waveguide loss of approximately 10 dB/cm, a confinement factor \( r \) of approximately 0.7 and a differential gain \( g_{o} \) of approximately \( 5 \times 10^{-16} \text{ cm}² \) are also used. The mirror loss \( \alpha_{m} \) is given by the following

\[ \alpha_{m} = \frac{1}{\text{length of medium}} \log \left( \frac{1}{r} \right). \]

where,

\[ r_{s} = \left| \frac{b_{j}}{a_{j}} \right| \]

\( r_{s} \) is the reflectivity from the strongest peak of the tunable frequency mirror, \( r \approx 0.3922 \) is the output facet field reflectivity of the tunable laser 100.

FIG. 4 is a plot of the Mode Suppression Ratio (MSR) versus the current in Amperes for the exemplary embodiment of FIG. 1B. According to L. Coldren et al., p. 107, Ibbid., the Mode Suppression Ratio (MSR) can be given by,

\[ \text{MSR(dB)} = 10 \log_{10} \left[ \frac{\Delta \alpha + \Delta \gamma}{\Delta G} + 1 \right]. \]

where \( \Delta \gamma \) is the separation between the mirror loss and the net modal gain for the main mode and is given by,

\[ \Delta \alpha = 9.1 \text{ m}^{-1} \text{ is the loss margin and } \Delta \gamma = 0 \text{ is the modal gain margin. Proceeding in this way, } I_{th} = 0.2 \text{ mA.} \]

FIG. 5 is a plot of the output power in Watts versus the input current in Amperes for the exemplary embodiment of FIG. 1A. The output power is given by L. Coldren et al., p. 42, Ibbid.

\[ P_{th} = \frac{g_{o}}{g_{m} + \alpha_{m}} \left( \frac{h}{q} \right) (1 - I_{th}) \text{ for } I > I_{th}. \]

where \( h \) is Planck’s constant.
as three or four optical resonators used in combinations on opposing sides of a length of gain medium. As with the single SRFP and other laser embodiments above, these embodiments can be monolithically fabricated.

5.1 Using at Least One SRFP Resonator With Resonators on Opposite Sides of the Gain Medium

FIG. 6A illustrates a class of laser 600 including two optical resonators 602A, 602B on opposing sides of a length of gain medium 606, i.e. the towards the left and right ends of the gain medium 606. Previous lasers have employed a gain medium bounded by optical resonators such as gratings. However, in embodiments of the present invention, at least one of the optical resonators 602A, 602B comprises a SRFP resonator as previously described. This defines a novel class of monolithic tunable semiconductor lasers. The lasers use the Vernier effect for the tunability. The lasing mode is the one that is a mode of both resonators 602A, 602B. The tunability of the laser 600 can be obtained by shifting the resonator modes at least one of the two resonators 602A, 602B.

In addition, further embodiments of the invention, the optical resonators 602A, 602B can be disposed on opposing sides of a width of gain medium 606. In the case of SRFP resonators, which employ side facets 608A, 608B, this allows separate adjustment and design of each resonator 602A, 602B. Some exemplary embodiments of the class of lasers of FIG. 6A are shown in FIGS. 6B-6G as follows.

As discussed above, further embodiments of the invention include a new type of tunable semiconductor laser using an optical resonator on each side of a gain medium. At least one of the optical resonators comprises a SRFP resonator as previously described. The tunable laser can be visualized as the combination of a gain medium bounded two reflectors, i.e., the resonators. One of the reflectors can be envisioned as a tunable filter element. As before, the nature of the coupling between the gain medium and the two resonators is not critical for the study of the device. For example, the nature of the coupling region can be evanescent coupling or multi mode couplers etc.

FIG. 6B illustrates a top view of an exemplary laser embodiment 620 of FIG. 6A where both resonators comprise SRFP resonators 622A, 622B. The resonant frequencies of the laser 620 are those that correspond to the resonant frequencies of the two SRFP resonators 622A, 622B and to a cavity mode of the gain medium 606. The frequency tunability of the laser 620 is obtained by changing the difference of optical path length of one of the SRFP resonators 622A, 622B to employ a Vernier effect.

As with the underlying SFRP resonators 622A, 622B, a laser 620 according to the embodiment of FIG. 6B employs relatively simple fabrication technology and does not require any grating structure or moving parts. When compared with a known double ring resonator coupled laser (DR-RCL), the waveguides 624A, 624B of the SFRP resonators 622A, 622B obtain lower curvature. See e.g., Bin Liu, Ali Shakouri, E. Bowers “Wide Tunable Double Ring Resonator Coupled Lasers”, IEEE Photonics Technology Letters, Vol. 14, No. 5, May 2002 which is incorporated by reference herein. This not only better facilitates fabrication but also reduces the losses related to the bending of the waveguides 624A, 624B. Also, because the FSR of resonators in general is inversely proportional to the length of the cavity, if a high FSR resonator is desired, the length of the resonator should be decreased. In the case of ring resonators, the minimum affordable length of the resonator will be substantially determined by the waveguide’s bending loss. Because the waveguide’s bending loss is lower in the present SRFP resonators 622A, 622B than in ring resonators, a higher resonator FSR should be obtainable with the laser 620 shown in FIG. 6B.

The laser 620 comprises three main regions, a gain medium 606 and two passive SRFP resonators 622A, 622B. There are different techniques for coupling the gain medium to the SRFP resonators as previously discussed. However, the nature of the coupling is not critical for the analytical study of the laser 620. The gain medium 606 provides light amplification. Each SRFP resonator 622A, 622B cavity includes waveguides \( \{q\} \) and \( \{q+2\} \) with \( q=\{2,5\} \). These correspond to the left and right portions of each of the waveguides 624A and 624B from their respective coupling regions 604A and 604B. Each respective facet is the high reflection facet \( q 626A, 626B \). Each SRFP resonator 622A, 622B has a uniform peak transmission at all resonant peaks. Their FSR is related to their optical length.

The two SRFP have slightly different optical lengths, thus providing the mode selection and the wavelength tuning mechanism. Therefore, the two SRFP resonator 622A, 622B tuning technique (which is based on the Vernier technique) is achieved by aligning the peaks in the two sets of resonator combs with the adjustment of index in one or both SRFP resonators 622A, 622B.

The proposed device can be compared to both the known sampled grating-distributed Bragg reflector (SG-DBR) laser and to the double ring resonator coupled laser (DR-RCL). However, in the laser 620 uses SRFP resonators 622A, 622B on opposing sides of the length of gain medium 606. In contrast, SG-DBR lasers employ sampled gratings on opposite sides of a length of gain medium and DR-RCL uses ring resonators on opposite sides of a length of gain medium.

One advantage of the SRFP resonator over the standard ring resonator is its support of standing waves (and larger waveguide bending curvature as previously discussed). This allows the device to use the only one coupling region in order to couple light from the SRFP resonator back to the gain medium. Further, the advantage of the SRFP resonator over the standard Fabry-Perot resonator is the use of only one facet. This eases the fabrication constraints on the SRFP resonator, the length of the SRFP may greatly differ from that of the chip.

Thus, the FSR of the SRFP resonator is not strongly dictated by fabrication requirements as with conventional Fabry-Perot resonators. As SRFP resonators produce a substantially uniform peak transmission at all resonant peaks, the uniform thresholds and efficiencies between the different operating wavelengths are substantially the same. Consequently, the laser 620 of FIG. 6D and the DR-RCL are nearly analytically equivalent and, accordingly, the laser 620 should exhibit at least the same advantages in term of performance (such as tunability and MSR) as the DR-RCL if manufactured properly. In addition, the laser 620 exhibits additional positive features. For example, the laser 620 allow a reduction in the number of coupling regions as well as the elimination of absorption regions. Indeed, reflection problems related to the discontinuity between the absorption region and the passive waveguide in DR-RCL devices are avoided. The presence of a non perfect high reflection facet (i.e. \( r4=0 \)) does not appreciably deteriorate the resonator response. Also, as previously mentioned, the overall design has the advantage of planar fabrication and does require any grating structure or moving parts.

Analysis and modeling of the coupling between the gain medium and the resonator in the laser 620 build on the analysis related to the SRFP resonator, in section 2 above.
The matrix form normalized complex field amplitude equations for coupling region 604A is as equation (3) in section 2, above. Similarly, the matrix form normalized complex field amplitude equations for coupling region 604B is as follows.

\[
\begin{pmatrix}
 b_4 \\
 b_5 \\
 b_6 \\
 b_7 \\
 b_8 \\
 b_9
\end{pmatrix}
= \begin{pmatrix}
 0 & 0 & b(f) & K_1(f) & b(f) & a_1 \\
 0 & 0 & -K_1(f) & b(f) & 0 & a_1 \\
 b_5 & -K_1(f) & K_1(f) & 0 & 0 & a_1 \\
 -K_1(f) & b(f) & 0 & 0 & a_1 \\
 b_6 & 0 & 0 & 0 & a_1 \\
 b_7 & 0 & 0 & a_1 & 0
\end{pmatrix}
\begin{pmatrix}
 a_1 \\
 a_2 \\
 a_3 \\
 a_4 \\
 a_5 \\
 a_6
\end{pmatrix}
\]

(27)

In the structure of FIG. 6B, from equations (3) and (27),

\[
\begin{align*}
 b_5 &= -K_1 R_1 [n_1 N + K_1] + z_1 R_1 [-K_1 N + \xi_1] \\
 b_6 &= -K_1 z_1 R_1 [n_1 M + K_1] + z_1 R_1 [-K_1 M + \xi_1]
\end{align*}
\]

(28)

where,

\[
\begin{align*}
 R_1 &= e^{-2 \alpha_1 L_1} e^{2 \alpha_1 L_1} \\
 N &= R_1 z_1 R_1 M + z_1 R_1 K_1 & 1 - R_1 z_1 R_1 [K_1 + z_1 R_1 K_1] & 1 - R_1 z_1 R_1 [K_1 + z_1 R_1 K_1]
\end{align*}
\]

(29)

and

\[
M = R_1 z_1 R_1 M + z_1 R_1 K_1 & 1 - R_1 z_1 R_1 [K_1 + z_1 R_1 K_1]
\]

(30)

where \( \alpha_1, n_1 \) and \( L_1 \) are, respectively, the loss per unit length, the refractive index and the length of the waveguide \( \{1\} \) and \( t_1 \) is the field reflectivity of the different facets as shown in FIG. 6B.

In the case of a tunable laser for WDM applications, one can neglect the frequency dependence of the coupling region over the working frequency range to obtain a rough approximation. Accordingly, it follows that,

\[
 K_1 = |K_1| e^{i \phi_1}, \phi_1 = \phi_1 e^{i \phi_1}
\]

(11)

FIGS. 6C–6F are exemplary plots of the spectra of the light reflected from the resonator for different values of the back reflection coefficients \( \{r_1, r_8\} \), and high facet reflections \( \{r_2, r_4, r_5, r_7\} \). These plots demonstrate the effect of the coupling coefficient and the back reflection (that is \( r_1 \) or \( r_8 \)) on the laser 620. FIG. 6C represents \( b_3/a_3 \) versus wavelength in the case where \( K_1 = K_2 = 0.7 \) and \( r_1 = 0 \), and a high reflection facet, \( r_2 = 1 \). FIG. 6D represents \( b_3/a_3 \) versus wavelength in the case where \( K_1 = K_2 = 0.7 \) and \( r_1 = 0 \), and a high reflection facet, \( r_2 = 0.9 \). FIG. 6E represents \( b_3/a_3 \) versus wavelength in the case where \( K_1 = K_2 = 0.7 \) and \( r_1 = 0 \), and a high reflection facet, \( r_2 = 0.9 \). FIG. 6F represents \( b_3/a_3 \) versus wavelength in the case where \( K_1 = K_2 = 0.7 \) and \( r_1 = 0.4 \), and the high reflection facet, \( r_2 = 0.9 \).

Notably, FIG. 6E shows that presence of a non perfect high reflection facet \( r_1 = 0, r_8 = 0 \) does appreciably deteriorate the resonator response. Also, as shown in FIG. 6F, the effect of a back reflection \( r_4 \) is to improve the performance of the resonator in term of reflection \( b_3/a_3 \) and FSR (the spacing between two consecutive peaks of same intensity). Thus, the laser 620 offers the possibility of increasing the FSR of the resonator by merely changing the back reflection \( r_4 \) instead of the resonator length. Also, even if there is a reflection returning to the gain medium directly from the coupling region, the laser 620 will operate correctly up to the point where this is equal to the reflection returning from the filter \( b_3/a_3 \).

FIG. 6G illustrates a further embodiment where one of the SRFP resonators is replaced by a ring resonator 628. Other alternate structures are also possible with at least one SRFP resonator on one side of the gain medium and another resonator form on the opposite side.

5.2 Using Multiple Resonators on One Side of the Gain Medium

FIG. 7A illustrates a laser 700 including two paired optical resonators 702A, 702B on the same side of a gain medium. One of the drawbacks of many prior art lasers comprising resonators bounding a gain medium (excluding those employing at least one SRFP resonator described above) is that they may exhibit relatively low power levels due to the resonators, such as gratings, employed on both sides of the device. In such prior art lasers, each resonator is designed to reflect most of the light coupled into the resonator back to the gain medium. Consequently, the amount of the light coming out of the device is weak. In contrast, the laser 700 employs two paired optical resonators 702A, 702B on one side of the gain medium 706 and leaves the output facet 704 of laser 700 as a cleaved facet.

The Vernier techniques can still employed to provide tuning in the laser 700. Tuning of the class of devices described by FIG. 7A can be obtained by changing the resonator frequencies of at least one of the resonators. However, in order to be able to use the Vernier technique, the field from the gain medium 706 must travel between both resonators 702A, 702B before returning to the gain medium 706. Accordingly, a 3 by 3 coupling region 708 can be employed to accomplish this. The coupling region 708 couples light from the gain medium 706 to the resonators 702A, 702B and the gain medium 706 and from one resonators, e.g. 702A, to the other resonators, e.g. 702B, and the gain medium 706. For example, the coupling region 708 can be for example a 3x3 MMI coupler. The class of lasers of FIG. 7A have the advantage of providing both high MSR, high tunability and high power in a single laser device.

In further embodiments of the invention, either or both the resonators 702A, 702B can be either SRFP resonator. In the case of SRFP resonators, which employ side facets 710A, 710B, this allows separate adjustment and design of each resonator 702A, 702B. Further, each SRFP can optionally include a MZI inside the resonator. In this case, as previously discussed, the free spectral range (FSR) of the resonator is increased because the FSR is substantially equal to that of the included MZI. Tuning can be obtained by changing the difference of optical length of the MZI. In addition, in still further embodiments, either resonator 702A, 702B can be ring resonator. Some exemplary embodiments of the class of lasers of FIG. 7A are shown in FIGS. 7B–7J as follows.

FIG. 7B illustrates a top view of an exemplary laser embodiment 720 where the resonators 702A, 702B comprise SRFP resonators 712A, 712B. In general, the coupling region 708 can be designed to couple light from the two resonators 702A, 702B and the gain medium 706, i.e. light coming from one resonator, e.g. 702A, is coupled to the other resonator, e.g. 702B and the gain medium 706. Only the field which is both a resonator mode of the combination of resonator 702A, resonator 702B and the coupling region 708 is reflected back to the gain medium 706. Tuning can be obtained by changing the resonator modes of resonator 702A or resonator 702B or the modes of both resonators 702A,
What is claimed is:

1. An optical device comprising:
   - a medium including an edge forming a first facet that is reflective;
   - a first waveguide within the medium, the first waveguide having first opposing ends formed by the first facet;
   - a coupling region to the first waveguide; and
   - a second waveguide coupled to the first waveguide by the coupling region where the second waveguide avoids intersecting the first facet and has both of second opposing ends formed by facets other than the first facet.

2. The optical device of claim 1, wherein the optical device is monolithically fabricated.

3. The optical device of claim 1, further comprising a second facet intersecting the second waveguide and adjacent to the first facet.

4. The optical device of claim 3, the second facet is anti-reflective.

5. The optical device of claim 3, further comprising a third facet intersecting the second waveguide and opposite the second facet.

6. The optical device of claim 1, further comprising a second facet intersecting the second waveguide and adjacent to the first facet and a third facet intersecting the second waveguide and opposite the second facet, where the second facet is anti-reflective.

7. The optical device of claim 1, wherein the first waveguide and the second waveguide comprise a substantially symmetrical arrangement about a line normal to the first facet through the coupling region.

8. The optical device of claim 1, wherein the first waveguide includes a Mach-Zehnder interferometer.

9. The optical device of claim 1, wherein current injection is used to adjust an optical length of at least a portion of the first waveguide.

10. The optical device of claim 1, wherein the medium is formed into a Fabry-Perot cavity having opposing Fabry-Perot reflective facets adjacent to the first facet.

11. The optical device of claim 10, wherein the second waveguide intersects both the opposing Fabry-Perot reflective facets.
12. The optical device of claim 1, wherein the first waveguide and the first facet operate as an optical resonator.

13. The optical device of claim 12, wherein the optical resonator comprises a tunable element of the optical device.

14. The optical device of claim 13, wherein current injection is used to adjust an optical length of at least a portion of the first waveguide to tune the tunable element of the optical device.

15. An optical device comprising:
   a first waveguide means for carrying light within a medium including an edge forming a first facet that is reflective, the first waveguide means having first opposing ends formed by the first facet;
   a second waveguide means for carrying the light where the second waveguide means avoids intersecting the first facet and has both of second opposing ends formed by facets other than the first facet; and
   a coupling region means for coupling the light between the first waveguide and the second waveguide.

16. The optical device of claim 15, further comprising a second facet intersecting the second waveguide means and adjacent to the first facet.

17. The optical device of claim 15, wherein the first waveguide means and the second waveguide means comprise a substantially symmetrical arrangement about a line normal to the first facet through the coupling region means.

18. The optical device of claim 15, wherein the first waveguide means includes a Mach-Zehnder interferometer.

19. The optical device of claim 15, wherein current injection is used to adjust an optical length of at least a portion of the first waveguide means.

20. The optical device of claim 15, wherein the medium is formed into a Fabry-Perot cavity having opposing Fabry-Perot reflective facets adjacent to the first facet and the second waveguide means intersects both the opposing Fabry-Perot reflective facets.

* * * * *