Bonding and Integration of C-C Composite to Cu-Clad-Molybdenum for Thermal Management Applications

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Abstract

Two- and three-dimensional carbon-carbon composites with either resin-derived matrix or CVI matrix were joined to Cu-clad-Mo using active Ag-Cu braze alloys for thermal management applications. The joint microstructure and composition were examined using Field-Emission Scanning Electron Microscopy and Energy-Dispersive Spectroscopy, and the joint hardness was characterized using the Knoop microhardness testing. Observations on the infiltration of the composite with molten braze, dissolution of metal substrate, and solute segregation at the C-C surface have been discussed. The thermal response of the integrated assembly is also briefly discussed.

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Overview

• Introduction and Background
• Experimental Procedures
  – Materials and Brazing
  – Characterization (*Microstructure, Microhardness*)
• Results and Discussion
  – Microstructure and Composition of Joints
  – Microhardness
  – Residual Stress and Thermal Considerations
• Concluding Remarks
• Acknowledgments
Thermal Properties of Some Typical Thermal Management Materials

Operating Temperature Can Limit Material Choices

Thermal Management Material Properties
Carbon-Carbon Composites Provide Tremendous Advantage and Excellent Benefits for Thermal Management

Application of Carbon-Carbon Composite Materials in Thermal Management Applications

Thermal conductivity of C/C composites strongly depends on the fiber type, architecture, and composite processing technology.


• High modulus, high conductivity pitch based carbon fibers can be used to improve the thermal properties of C-C composites.

Active Metal Brazing of Titanium to C/C Composites for Heat Rejection Systems

• Recently, we had joined C-C composite to Ti tubes for lightweight heat exchanger applications.
• Both direct bonding using braze layers and indirect bonding using a porous carbon foam (saddle material) and braze layers were employed.
• Excellent bonding of active braze to foam, C-C Composite, and Ti Tube occurred.
• Failure always occurred in Poco HTC (Saddle Material) indicating that bond strength exceeded the fracture strength of foam.

Testing of Brazed Joints in Woven K1100 and P120 C/C Facesheet/Foam/Ti Tube

Specimens with different tube-foam contact areas were fabricated in order to vary braze contact area and stress applied to joints.

- Tube on flat: Lowest contact area, highest stress on joint.
- Tube in shallow trough: Intermediate contact area.
- Tube in deep trough: Highest contact area, lowest stress on joint.


Why Copper Clad Molybdenum was chosen as a Thermal Management Material?

- Copper has excellent thermal conductivity (K for OFHC Cu: 401 W/m.K).
- CTE of Cu is high (16.5 ppm/K). Difficulty in joining to ceramic substrates.
- Low annealing temperature of Cu causes softening at moderate heat input.
- Cladding Mo with Cu lowers CTE and promotes thermoelastic compatibility with ceramics.
- Small weight penalty (density of Cu: 8,900 kg.m⁻³, density of Mo: 10,280 kg.m⁻³).

Objective

- Develop brazing approaches for 2D and 3D C-C composites with resin and CVI matrices to Cu-clad-Mo using active braze alloys.

- Characterize the joint microstructure, composition, and microhardness behavior.

Experimental Procedure: Materials and Properties

- 2-D and 3-D C-C composites (Resin + CVI Carbon matrix) – Goodrich Corp., CA.
- C-C composites (Resin derived matrix) – C-CAT, Inc., TX.
- Cu-clad-Mo plates (Cu-Mo-Cu ratio: 13%-74%-13%) – H.C. Starck, Inc., MA.
- Active braze alloy (ABA) powders – Morgan Advanced Ceramics, CA.

Composition and Properties of Brazes

<table>
<thead>
<tr>
<th>Braze (composition, %)</th>
<th>$T_1$, °C</th>
<th>$T_2$, °C</th>
<th>E, GPa</th>
<th>YS, MPa</th>
<th>UTS, MPa</th>
<th>CTE, $\times 10^{-6}$ C$^{-1}$</th>
<th>% El.</th>
<th>K, W/m.K</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cusil-ABA® (68.8Ag-35.3Cu-1.75Ti)</td>
<td>815</td>
<td>780</td>
<td>83</td>
<td>271</td>
<td>346</td>
<td>18.5</td>
<td>42</td>
<td>180</td>
</tr>
<tr>
<td>Ticusil® (68.8Ag-26.7Cu-4.5Ti)</td>
<td>900</td>
<td>780</td>
<td>85</td>
<td>292</td>
<td>339</td>
<td>18.5</td>
<td>28</td>
<td>219</td>
</tr>
</tbody>
</table>

E: Young’s modulus, YS: yield strength, UTS: tensile strength, CTE: coefficient of thermal expansion, %El: percent elongation, K: thermal conductivity
Experimental Procedure

- Substrates cut into 2.54 cm x 1.25 cm x 0.25 cm plates and ultrasonically cleaned in acetone for 15 min.
- Braze powders mixed with glycerin to dough-like consistency and braze paste manually applied to C-C surface.
- Assembly heated under vacuum (~10^-6 torr) to 15-20°C above braze T_L. After 5 min. soak, slowly cooled (~5°C per min.).
- Brazed joints mounted in epoxy, ground, polished, and examined using optical microscopy and Field Emission Scanning Electron Microscopy (Hitachi 4700) coupled with EDS.
- Microhardness (Knoop indenter) on Struers Duramin-A300 machine (200 g load, 10 s). Four-to-six scans across each joint.

C-C Composite/Cu-Clad-Mo Joints for Thermal Management Applications

- Resin-derived C-C composites brazed to Cu-clad Mo using active braze alloys (ABA).
- Good metallurgical bonding at joints, with some dissolution, diffusion, and solute redistribution.
- Ti segregated at C-C surface. Cu-ABA joints displayed the largest Ti concentrations at joint.
- Microhardness gradients exist at joints.
- C-C/Cu-clad Mo systems may have potential for thermal management applications.

**3-D C-C Composite/Cu-clad-Mo Joint**

- Braze penetration to several hundred micrometers in 5 min.
- No effect of fiber ply orientation on infiltration.
- Improved wetting by Ti in braze facilitated infiltration.
- Extensive infiltration of C-C consistent with sessile-drop tests (complete disappearance of drops in porous carbon!).

**3-D C-C composite/Cusil ABA/Cu-clad-Mo joint**

- High concentrations of Ti at interface.
- Two-phase eutectic structure in braze (Ag-rich light-grey and Cu-rich dark grey).
- No melting of clad layer (M.P. of Cu: 1086°C)
- Possible formation of titanium carbide (Ti+C → TiC, ΔG = -171.18 kJ at 850°C).
- Sub-stoichiometric carbides (TiC0.95, TiC0.91, TiC0.80, TiC0.70, TiC0.60 and TiC0.48) may also form.

<table>
<thead>
<tr>
<th>Location</th>
<th>C</th>
<th>Ti</th>
<th>Cu</th>
<th>Mo</th>
<th>Ag</th>
</tr>
</thead>
<tbody>
<tr>
<td>Point 1</td>
<td>96.468</td>
<td>0.893</td>
<td>0.000</td>
<td>0.723</td>
<td>2.116</td>
</tr>
<tr>
<td>Point 2</td>
<td>35.131</td>
<td>49.912</td>
<td>5.203</td>
<td>0.941</td>
<td>8.613</td>
</tr>
<tr>
<td>Point 3</td>
<td>0.675</td>
<td>0.238</td>
<td>3.881</td>
<td>0.281</td>
<td>94.835</td>
</tr>
<tr>
<td>Point 4</td>
<td>0.000</td>
<td>2.437</td>
<td>88.489</td>
<td>0.000</td>
<td>0.004</td>
</tr>
</tbody>
</table>
3-D C-C composite/Ticusil/Cu-clad-Mo joint

- Some dissolution of carbon in braze (possibly due to higher temperature of Ticusil).
- Carbon also detected within the Cu-clad-Mo region.

C-C composite/Ticusil/Cu-clad-Mo joint
(resin-derived composite)

- Cracks in composite (low interlaminar shear strength).
- Braze displays eutectic structure with Ag- and Cu-rich phases.
- Precipitation of Ag-rich phase on C-C and Cu-clad-Mo surfaces.
- A small amount of Cu detected within the C-C composite.

<table>
<thead>
<tr>
<th>Location</th>
<th>C</th>
<th>Ti</th>
<th>Cu</th>
<th>Mo</th>
<th>Ag</th>
</tr>
</thead>
<tbody>
<tr>
<td>Point 1</td>
<td>5.345</td>
<td>8.090</td>
<td>81.097</td>
<td>0.314</td>
<td>5.154</td>
</tr>
<tr>
<td>Point 2</td>
<td>2.097</td>
<td>0.228</td>
<td>4.540</td>
<td>0.508</td>
<td>92.627</td>
</tr>
<tr>
<td>Point 3</td>
<td>0.000</td>
<td>0.368</td>
<td>75.623</td>
<td>0.236</td>
<td>14.057</td>
</tr>
<tr>
<td>Point 4</td>
<td>1.852</td>
<td>10.084</td>
<td>2.776</td>
<td>0.382</td>
<td>88.623</td>
</tr>
<tr>
<td>Point 5</td>
<td>98.060</td>
<td>0.264</td>
<td>1.183</td>
<td>0.231</td>
<td>0.262</td>
</tr>
<tr>
<td>Point 6</td>
<td>18.237</td>
<td>54.484</td>
<td>16.697</td>
<td>0.553</td>
<td>2.050</td>
</tr>
</tbody>
</table>
Knoop Hardness across Brazed Joints

- No effect of fiber ply orientation and composite type (CVI vs resin-derived) on HK within the braze region.
- HK of Mo substrate is ~200-330; HK depends on braze type: Ticusil (4.5%Ti) has higher HK (~85-200) than Cusil-ABA (1.75%Ti) (~50-150).
- Some effect of larger residual stresses in Ticusil because of its higher joining temperature.

Strain Energy in Brazed Joints

- Less strain energy develops in Cusil-ABA joints than in Ticusil joints.
- Strain energy C-C/Ticusil/Cu-clad-Mo joints is 37.5 mJ.
- Ductile braze and Cu cladding prevented failure.
- Lower strain energy in comparable joints of Cu-clad-Mo with SiC-SiC.
Estimation of Thermal Resistance in Brazed Joints

Effective thermal resistance (1-D steady-state conduction)

\[ R_{\text{eff}} = \sum (\Delta x_i / K_i) \]

(\( \Delta x_i \): thickness, \( K_i \): thermal conductivity)

- C-C/Cu-clad-Mo joints have 22% lower thermal resistance than C-C.
- There is some weight penalty in joining C-C to Cu-clad-Mo (39% increase in density).
- Potential benefit to join C-C to Cu-clad-Mo in thermal management systems.

Concluding Remarks

- C-C composites with CVI and resin-derived matrices were brazed to Cu-clad-Mo using active braze alloys.
- SEM and EDS revealed sound bonding and Ti segregation at interface and no evidence of extensive chemical attack of C-C. There was limited redistribution of alloying elements.
- De-lamination in resin-derived C-C was observed due to its low inter-laminar shear strength (ILSS). Extensive braze infiltration of inter-fiber channels occurred in 3D composites.
- Sharp hardness gradients occurred at Cu-clad-Mo/braze interface. Ticusil exhibited greater hardness (~85-250 HK) than Cusil-ABA (~50-150 HK). This may be due to higher Ti content of Ticusil (4.5% Ti) than Cusil-ABA (1.75% Ti).
- C-C/Cu-clad-Mo joints may have ~22% lower thermal resistance compared to C-C composites.
Acknowledgement

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