

NASA/TM—2011-217012



# Density Weighted FDF Equations for Simulations of Turbulent Reacting Flows

*Tsan-Hsing Shih*  
*Ohio Aerospace Institute, Brook Park, Ohio*

*Nan-Suey Liu*  
*Glenn Research Center, Cleveland, Ohio*

## NASA STI Program . . . in Profile

Since its founding, NASA has been dedicated to the advancement of aeronautics and space science. The NASA Scientific and Technical Information (STI) program plays a key part in helping NASA maintain this important role.

The NASA STI Program operates under the auspices of the Agency Chief Information Officer. It collects, organizes, provides for archiving, and disseminates NASA's STI. The NASA STI program provides access to the NASA Aeronautics and Space Database and its public interface, the NASA Technical Reports Server, thus providing one of the largest collections of aeronautical and space science STI in the world. Results are published in both non-NASA channels and by NASA in the NASA STI Report Series, which includes the following report types:

- **TECHNICAL PUBLICATION.** Reports of completed research or a major significant phase of research that present the results of NASA programs and include extensive data or theoretical analysis. Includes compilations of significant scientific and technical data and information deemed to be of continuing reference value. NASA counterpart of peer-reviewed formal professional papers but has less stringent limitations on manuscript length and extent of graphic presentations.
- **TECHNICAL MEMORANDUM.** Scientific and technical findings that are preliminary or of specialized interest, e.g., quick release reports, working papers, and bibliographies that contain minimal annotation. Does not contain extensive analysis.
- **CONTRACTOR REPORT.** Scientific and technical findings by NASA-sponsored contractors and grantees.

- **CONFERENCE PUBLICATION.** Collected papers from scientific and technical conferences, symposia, seminars, or other meetings sponsored or cosponsored by NASA.
- **SPECIAL PUBLICATION.** Scientific, technical, or historical information from NASA programs, projects, and missions, often concerned with subjects having substantial public interest.
- **TECHNICAL TRANSLATION.** English-language translations of foreign scientific and technical material pertinent to NASA's mission.

Specialized services also include creating custom thesauri, building customized databases, organizing and publishing research results.

For more information about the NASA STI program, see the following:

- Access the NASA STI program home page at <http://www.sti.nasa.gov>
- E-mail your question via the Internet to [help@sti.nasa.gov](mailto:help@sti.nasa.gov)
- Fax your question to the NASA STI Help Desk at 443-757-5803
- Telephone the NASA STI Help Desk at 443-757-5802
- Write to:  
NASA Center for AeroSpace Information (CASI)  
7115 Standard Drive  
Hanover, MD 21076-1320

NASA/TM—2011-217012



# Density Weighted FDF Equations for Simulations of Turbulent Reacting Flows

*Tsan-Hsing Shih*  
*Ohio Aerospace Institute, Brook Park, Ohio*

*Nan-Suey Liu*  
*Glenn Research Center, Cleveland, Ohio*

National Aeronautics and  
Space Administration

Glenn Research Center  
Cleveland, Ohio 44135

---

May 2011

## Acknowledgments

This work is supported by the Subsonic Fixed Wing Project and the Supersonics Project of the NASA Fundamental Aeronautics Program. The authors highly appreciate the fruitful discussions with Dr. P. Tsao.

This report is a formal draft or working paper, intended to solicit comments and ideas from a technical peer group.

This report contains preliminary findings, subject to revision as analysis proceeds.

Trade names and trademarks are used in this report for identification only. Their usage does not constitute an official endorsement, either expressed or implied, by the National Aeronautics and Space Administration.

This work was sponsored by the Fundamental Aeronautics Program at the NASA Glenn Research Center.

*Level of Review:* This material has been technically reviewed by technical management.

Available from

NASA Center for Aerospace Information  
7115 Standard Drive  
Hanover, MD 21076-1320

National Technical Information Service  
5301 Shawnee Road  
Alexandria, VA 22312

Available electronically at <http://www.sti.nasa.gov>

# Contents

Abstract.....	1
1.0 Introduction.....	1
2.0 Density Weighted Filtered Density Function (DW-FDF) and Filtered Turbulent Variables.....	2
2.1 Fine Grained Probability Density Function (FG-PDF) $f'_U(\mathbf{V}; \mathbf{x}, t), f'_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$ .....	2
2.2 Filtered Turbulent Variables and DW-FDF $F_U(\mathbf{V}; \mathbf{x}, t), f_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$ .....	4
2.2.1 Filtered Turbulent Variables.....	4
2.2.2 Definition of DW-FDF.....	5
2.2.3 DW-FDF Mean $\langle \rangle_L$ .....	7
3.0 Traditional DW-FDF Equations for $F_U(\mathbf{V}; \mathbf{x}, t), F_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$ .....	8
3.1 Traditional DW-FDF Equation for $F_U(\mathbf{V}; \mathbf{x}, t)$ .....	8
3.2 Traditional DW-FDF Equation for $F_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$ .....	8
4.0 DW-FDF Equations Derived From Filtered Navier-Stokes Equations.....	9
4.1 Filtered Compressible Navier-Stokes Equations.....	9
4.2 DW-FDF Equation for $F_U(\mathbf{V}; \mathbf{x}, t)$ .....	11
4.3 DW-FDF Equation for $F_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$ .....	13
4.4 Modeling of Unclosed Terms.....	14
4.5 Summary.....	15
5.0 Concluding Remarks.....	16
References.....	16



# Density Weighted FDF Equations for Simulations of Turbulent Reacting Flows

Tsan-Hsing Shih  
Ohio Aerospace Institute  
Brook Park, Ohio 44142

Nan-Suey Liu  
National Aeronautics and Space Administration  
Glenn Research Center  
Cleveland, Ohio 44135

## Abstract

In this report, we briefly revisit the formulation of density weighted filtered density function (DW-FDF) for large eddy simulation (LES) of turbulent reacting flows, which was proposed by Jaber et al. (Ref. 1). At first, we proceed the traditional derivation of the DW-FDF equations by using the fine grained probability density function (FG-PDF), then we explore another way of constructing the DW-FDF equations by starting directly from the compressible Navier-Stokes equations. We observe that the terms which are unclosed in the traditional DW-FDF equations are now closed in the newly constructed DW-FDF equations. This significant difference and its practical impact on the computational simulations may deserve further studies.

## 1.0 Introduction

The concept of filtered density function (FDF) method (Ref. 2) was extended to the compressible turbulent reacting flow by introducing a filtered mass density function (FMDF) (Ref. 1), which is a density weighted FDF and is referred as DW-FDF in this report. The work was considered as the extension of the probability density function (PDF) method (Pope (Ref. 3)) to the LES simulation with the advantage of its direct simulation of turbulence-chemistry interaction without modeling.

This report follows our previous work on the conservational PDF equations (Shih and Liu (Ref. 4)) to explore different ways of constructing the DW-FDF equations for simulations of filtered turbulent reacting flows. It will be shown that there are significant differences between the FMDF equations and the newly proposed DW-FDF equations, with the latter requiring much less empirical modeling.

In Section 2.0, we review the definition of DW-FDF starting from a delta function of a turbulent random variable, which is called in the literature as the fine grained probability density function (FG-PDF)  $f'$ . The definition of a filtered turbulent variable used in LES is also briefly reviewed. Then we explore the relationship between the DW-FDF and the filtered turbulent variable. This relationship suggests the concept of “DW-FDF mean”,  $\langle \rangle_L$  which is the analogy to the statistical mean,  $\langle \rangle$  in the PDF theory. A few properties of the DW-FDF mean are explored, and they are found to be useful in constructing the transport equations for the DW-FDF.

In Section 3.0, we first formulate a compressible transport equation for FG-PDF, and then apply a stationary or homogeneous filtering on it to construct the equations that we refer as the traditional DW-FDF equations, which are consistent with the FMDF equations introduced by Jaber et al. (Ref. 1).

In Section 4.0, we adopt a similar methodology described in Reference 4 to construct the DW-FDF equations by directly starting from the filtered compressible Navier-Stokes equations. The resulted equations are significantly different from the traditional FMDF equations. For example, the unclosed terms appearing on the right hand side of FMDF equations are now closed in the newly constructed DW-FDF equations.

It is noted here that the quantity DW-FDF (or FMDF) is fundamentally different from the quantity PDF, namely, DW-FDF is a random quantity; but PDF is a deterministic quantity. The “DW-FDF mean” defines a density-weighted filtered turbulent random variable; but the “PDF mean” defines a turbulent mean variable. The DW-FDF, unlike PDF, does not represent a probability density of a random variable; it is only a density-weighted filtered FG-PDF and is still a random variable. These fundamental differences between DW-FDF and PDF may require a further investigation on their respective solution procedures based on the stochastic differential equation methods.

## 2.0 Density Weighted Filtered Density Function (DW-FDF) and Filtered Turbulent Variables

In this section, we will first review the basic properties of FG-PDF and its density-weighted filtered quantity, DW-FDF, then explore the relationship between DW-FDF and filtered turbulent variable. This provides the basis for further establishing the transport equations of DW-FDF.

### 2.1 Fine Grained Probability Density Function (FG-PDF) $f'_U(\mathbf{V}; \mathbf{x}, t)$ , $f'_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$

The FG-PDF for turbulent velocity and scalars (e.g., species mass fraction, internal energy) are defined as follows (Pope (Ref. 3)),

$$f'_U(\mathbf{V}; \mathbf{x}, t) \equiv \delta(\mathbf{U}(\mathbf{x}, t) - \mathbf{V}) \equiv \prod_{i=1}^3 \delta(U_i(\mathbf{x}, t) - V_i) \quad (1)$$

$$f'_\Phi(\boldsymbol{\psi}; \mathbf{x}, t) \equiv \delta(\boldsymbol{\Phi}(\mathbf{x}, t) - \boldsymbol{\psi}) \equiv \prod_{i=1}^{N+1} \delta(\Phi_i(\mathbf{x}, t) - \psi_i) \quad (2)$$

where  $\delta$  denotes the delta function,  $\mathbf{U}(\mathbf{x}, t)$  is the turbulent velocity vector ( $U_1, U_2, U_3$ ),  $\boldsymbol{\Phi}(\mathbf{x}, t)$  is the turbulent scalar array ( $\Phi_1, \Phi_2, \dots, \Phi_N, \Phi_{N+1}$ ), for example,  $N$  species mass fractions and one internal energy  $\Phi_{N+1} = e$ , the  $\mathbf{x}, t$  denote the physical space variable ( $x_1, x_2, x_3$ ) and the time  $t$ ,  $\mathbf{V} \equiv (V_1, V_2, V_3)$  and  $\boldsymbol{\psi} \equiv (\psi_1, \psi_2, \dots, \psi_N, \psi_{N+1})$  are the sample space variables for  $\mathbf{U}(\mathbf{x}, t)$  and  $\boldsymbol{\Phi}(\mathbf{x}, t)$ , respectively. The FG-PDF has the following properties that will be used in this study:

#### i. The Unity Integral of FG-PDF

$$\int_{-\infty}^{+\infty} f'_U(\mathbf{V}; \mathbf{x}, t) d\mathbf{V} = 1, \quad \int_{-\infty}^{+\infty} f'_\Phi(\boldsymbol{\psi}; \mathbf{x}, t) d\boldsymbol{\psi} = 1 \quad (3)$$

Note that  $(-\infty, +\infty)$  represents the whole domain of sample space, for the species mass fractions it really means  $(0, 1)$ .

#### ii. The Differential Chain

$$\frac{\partial f'_U}{\partial t} = \frac{\partial f'_U}{\partial U_i} \frac{\partial U_i}{\partial t} = -\frac{\partial f'_U}{\partial V_i} \frac{\partial U_i}{\partial t} = -\frac{\partial}{\partial V_i} \left( f'_U \frac{\partial U_i}{\partial t} \right) \quad (4)$$

$$\frac{\partial f'_U}{\partial x_j} = \frac{\partial f'_U}{\partial U_i} \frac{\partial U_i}{\partial x_j} = -\frac{\partial f'_U}{\partial V_i} \frac{\partial U_i}{\partial x_j} = -\frac{\partial}{\partial V_i} \left( f'_U \frac{\partial U_i}{\partial x_j} \right) \quad (5)$$

Note that the summation convention on the same index, e.g., “ $i$ ” is implied. Therefore, we have

$$\frac{\partial f'_U}{\partial t} + U_j \frac{\partial f'_U}{\partial x_j} = - \frac{\partial}{\partial V_i} \left[ f'_U \left( \frac{\partial U_i}{\partial t} + U_j \frac{\partial U_i}{\partial x_j} \right) \right], \quad (\text{for incompressible flow}) \quad i, j = 1, 2, 3 \quad (6)$$

and

$$\frac{\partial \rho f'_U}{\partial t} + \frac{\partial \rho U_j f'_U}{\partial x_j} = - \frac{\partial}{\partial V_i} \left[ f'_U \left( \frac{\partial \rho U_i}{\partial t} + \frac{\partial \rho U_i U_j}{\partial x_j} \right) \right], \quad (\text{for compressible flow}) \quad i, j = 1, 2, 3 \quad (7)$$

Note that the continuity equation of compressible flow has been applied here. Similarly,

$$\frac{\partial f'_\Phi}{\partial t} = \frac{\partial f'_\Phi}{\partial \Phi_i} \frac{\partial \Phi_i}{\partial t} = - \frac{\partial f'_\Phi}{\partial \Psi_i} \frac{\partial \Phi_i}{\partial t} = - \frac{\partial}{\partial \Psi_i} \left( f'_\Phi \frac{\partial \Phi_i}{\partial t} \right) \quad (8)$$

$$\frac{\partial f'_\Phi}{\partial x_j} = \frac{\partial f'_\Phi}{\partial \Phi_i} \frac{\partial \Phi_i}{\partial x_j} = - \frac{\partial f'_\Phi}{\partial \Psi_i} \frac{\partial \Phi_i}{\partial x_j} = - \frac{\partial}{\partial \Psi_i} \left( f'_\Phi \frac{\partial \Phi_i}{\partial x_j} \right) \quad (9)$$

and

$$\frac{\partial f'_\Phi}{\partial t} + U_j \frac{\partial f'_\Phi}{\partial x_j} = - \frac{\partial}{\partial \Psi_i} \left[ f'_\Phi \left( \frac{\partial \Phi_i}{\partial t} + U_j \frac{\partial \Phi_i}{\partial x_j} \right) \right], \quad (\text{for incompressible flow}) \quad \begin{cases} i = 1, 2, \dots, N+1 \\ j = 1, 2, 3 \end{cases} \quad (10)$$

$$\frac{\partial \rho f'_\Phi}{\partial t} + \frac{\partial \rho U_j f'_\Phi}{\partial x_j} = - \frac{\partial}{\partial \Psi_i} \left[ f'_\Phi \left( \frac{\partial \rho \Phi_i}{\partial t} + \frac{\partial \rho \Phi_i U_j}{\partial x_j} \right) \right], \quad (\text{for compressible flow}) \quad \begin{cases} i = 1, 2, \dots, N+1 \\ j = 1, 2, 3 \end{cases} \quad (11)$$

### iii. The Sifting Property

$$U(\mathbf{x}, t) f'_U(\mathbf{V}; \mathbf{x}, t) \equiv U(\mathbf{x}, t) \delta(U(\mathbf{x}, t) - V) = V \delta(U(\mathbf{x}, t) - V) = V f'_U(\mathbf{V}; \mathbf{x}, t) \quad (12)$$

$$\Phi(\mathbf{x}, t) f'_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t) = \boldsymbol{\Psi} f'_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t) \quad (13)$$

More generally,

$$\begin{aligned} Q(U(\mathbf{x}, t)) f'_U(\mathbf{V}; \mathbf{x}, t) &= Q(V) f'_U(\mathbf{V}; \mathbf{x}, t) \\ Q(\Phi(\mathbf{x}, t)) f'_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t) &= Q(\boldsymbol{\Psi}) f'_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t) \end{aligned} \quad (14)$$

where  $Q(\cdot)$  denotes a general (but not the time or space differential) function form.

### iv. The Statistical Mean of FG-PDF

Equations (1) and (2) indicate that FG-PDF is a random quantity, because it is the delta function of the random variable  $U(\mathbf{x}, t)$  or  $\Phi(\mathbf{x}, t)$ . The basic probability theory says that a random variable and its (non-differential) function share the same probability density. Therefore, the probability density function PDF of the random variable FG-PDF is  $f_U(\mathbf{V}; \mathbf{x}, t)$  or  $f_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t)$ , which is the PDF of turbulent velocity

$U(\mathbf{x},t)$  or scalars  $\Phi(\mathbf{x},t)$ , respectively. It is easy to verify that the statistical mean of FG-PDF is the corresponding PDF (Pope (Ref. 3)):

$$\langle f'_U(\mathbf{V}; \mathbf{x}, t) \rangle = \langle \delta(U(\mathbf{x}, t) - \mathbf{V}) \rangle \equiv \int_{-\infty}^{+\infty} \delta(\mathbf{V}' - \mathbf{V}) f_U(\mathbf{V}'; \mathbf{x}, t) d\mathbf{V}' = f_U(\mathbf{V}; \mathbf{x}, t) \quad (15)$$

Similarly,

$$\langle f'_\Phi(\Psi; \mathbf{x}, t) \rangle = f_\Phi(\Psi; \mathbf{x}, t) \quad (16)$$

The FG-PDF is a useful quantity for mathematical derivations. It is interesting to examine the following expressions:

$$\int \mathbf{V} f'_U(\mathbf{V}; \mathbf{x}, t) d\mathbf{V} \equiv \langle U(\mathbf{x}, t) \rangle_{FG} = U(\mathbf{x}, t) \quad (17)$$

$$\int \Psi f'_\Phi(\Psi; \mathbf{x}, t) d\Psi \equiv \langle \Phi(\mathbf{x}, t) \rangle_{FG} = \Phi(\mathbf{x}, t) \quad (18)$$

which indicate that the ‘‘FG-PDF mean’’ defines the original random variable itself. More generally,

$$\int Q(\mathbf{V}) f'_U(\mathbf{V}; \mathbf{x}, t) d\mathbf{V} \equiv \langle Q(U(\mathbf{x}, t)) \rangle_{FG} = Q(U(\mathbf{x}, t)) \quad (19)$$

$$\int Q(\Psi) f'_\Phi(\Psi; \mathbf{x}, t) d\Psi \equiv \langle Q(\Phi(\mathbf{x}, t)) \rangle_{FG} = Q(\Phi(\mathbf{x}, t))$$

## 2.2 Filtered Turbulent Variables and DW-FDF $f_U(\mathbf{V}; \mathbf{x}, t)$ , $f_\Phi(\Psi; \mathbf{x}, t)$

First we review the definition of filtered turbulent variables conventionally used in the turbulent simulation and the definition of DW-FDF, and then we explore the relationship between the DW-FDF and the filtered turbulent variables.

### 2.2.1 Filtered Turbulent Variables

In the conventional simulation of compressible reacting flows, we often deal with two types of filtered turbulent variables: one with the density weighting, the other without the density weighting. The filtered turbulent variable without the density weighting is denoted by  $\bar{\phi}(\mathbf{x}, t)$  and is defined as

$$\bar{\phi}(\mathbf{x}, t) = \int_{-\infty}^{+\infty} \phi(\mathbf{x}, t') G(t - t') dt' \quad (20)$$

where  $\phi$  is the unfiltered turbulent variable, e.g., velocity components  $U_i$ , density  $\rho$ , pressure  $P$ , species mass fraction  $\Phi_i$  and internal energy  $e = \sum_{m=1}^N \Phi_m e_m$ . The integration is over the entire time domain

$-\infty < t' < +\infty$ .  $G(t - t')$  is the time filter with a constant filter width  $\Delta_T$  and satisfies the following condition and asymptotic property:

$$\int_{-\infty}^{+\infty} G(t - t') dt' = 1 \quad (21)$$

$$\int_{-\infty}^{+\infty} \phi(\mathbf{x}, t') G(t-t') dt' = \phi(\mathbf{x}, t), \quad \text{as } \Delta_T \rightarrow 0 \quad (22)$$

The density-weighted filtered turbulent variable is denoted by  $\tilde{\phi}(\mathbf{x}, t)$  and defined as

$$\tilde{\phi}(\mathbf{x}, t) = \frac{\overline{\rho\phi}}{\bar{\rho}} \quad (23)$$

It is noted here that these filtered variables  $\bar{\phi}(\mathbf{x}, t)$ ,  $\tilde{\phi}(\mathbf{x}, t)$  represent the large scale turbulent variables (Shih and Liu (Refs. 5 and 6)), and they are still random but contain relatively low frequency part of the turbulent motion when comparing with the unfiltered turbulent variable  $\phi(\mathbf{x}, t)$ .

### 2.2.2 Definition of DW-FDF

Jaberi et al. (Ref. 1) introduced the density-weighted space filter operation  $\rho(\mathbf{x}', t)G(\mathbf{x} - \mathbf{x}')$  on the FG-PDF  $f'_U(\mathbf{V}; \mathbf{x}, t)$ ,  $f'_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t)$  and referred to them as the filtered mass density function FMDF. However, we prefer a more intuitive name related to the existing FDF methodology (Colluci et al. (Ref. 2)), and refer them as the density weighted FDF (DW-FDF). With the density-weighted time filter  $\rho(\mathbf{x}, t')G(t-t')$  we define the following marginal DW-FDF as

$$\begin{aligned} F_U(\mathbf{V}; \mathbf{x}, t) &\equiv \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') f'_U(\mathbf{V}; \mathbf{x}, t') G(t-t') dt' \\ &= \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \delta(\mathbf{U}(\mathbf{x}, t') - \mathbf{V}) G(t-t') dt' \\ F_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t) &\equiv \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') f'_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t') G(t-t') dt' \\ &= \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \delta(\boldsymbol{\Phi}(\mathbf{x}, t') - \boldsymbol{\Psi}) G(t-t') dt' \end{aligned} \quad (24)$$

Obviously, DW-FDF, i.e.,  $F_U(\mathbf{V}; \mathbf{x}, t)$  or  $F_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t)$ , is still a random quantity. It satisfies the following ‘‘normalization’’ property:

$$\begin{aligned} \int_{-\infty}^{\infty} F_U(\mathbf{V}; \mathbf{x}, t) d\mathbf{V} &= \int_{-\infty}^{\infty} \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') f'_U(\mathbf{V}; \mathbf{x}, t') G(t-t') dt' d\mathbf{V} = \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') G(t-t') dt' = \bar{\rho} \\ \int_{-\infty}^{\infty} F_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t) d\boldsymbol{\Psi} &= \int_{-\infty}^{\infty} \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') f'_\Phi(\boldsymbol{\Psi}; \mathbf{x}, t') G(t-t') dt' d\boldsymbol{\Psi} = \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') G(t-t') dt' = \bar{\rho} \end{aligned} \quad (25)$$

With the definition of DW-FDF described in Equation (24), we can exactly deduce the filtered turbulent variables that are conventionally defined by Equations (20) and (23). For example,

$$\begin{aligned} \int_{-\infty}^{+\infty} \mathbf{V} F_U(\mathbf{V}; \mathbf{x}, t) d\mathbf{V} &= \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \mathbf{V} \rho(\mathbf{x}, t') \delta(\mathbf{U}(\mathbf{x}, t') - \mathbf{V}) G(t-t') dt' d\mathbf{V} \\ &= \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \mathbf{U}(\mathbf{x}, t') \rho(\mathbf{x}, t') \delta(\mathbf{U}(\mathbf{x}, t') - \mathbf{V}) G(t-t') dt' d\mathbf{V} \\ &= \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \mathbf{U}(\mathbf{x}, t') G(t-t') dt' = \overline{\rho\mathbf{U}} = \bar{\rho}(\mathbf{x}, t) \tilde{\mathbf{U}}(\mathbf{x}, t) \end{aligned} \quad (26)$$

where the sifting property of FG-PDF has been used in the second line of (26). Similarly,

$$\int_{-\infty}^{+\infty} \Psi F_{\Phi}(\Psi; \mathbf{x}, t) d\Psi = \overline{\rho \Phi} = \bar{\rho}(\mathbf{x}, t) \tilde{\Phi}(\mathbf{x}, t) \quad (27)$$

If we denote the left hand side of Equations (26) and (27) as the operation  $\langle U \rangle_L$  and  $\langle \Phi \rangle_L$ , we may write Equations (26) and (27) as

$$\langle U \rangle_L \equiv \int_{-\infty}^{+\infty} V F_U(V; \mathbf{x}, t) dV = \bar{\rho}(\mathbf{x}, t) \tilde{U}(\mathbf{x}, t) \quad (28)$$

$$\langle \Phi \rangle_L \equiv \int_{-\infty}^{+\infty} \Psi F_{\Phi}(\Psi; \mathbf{x}, t) d\Psi = \bar{\rho}(\mathbf{x}, t) \tilde{\Phi}(\mathbf{x}, t) \quad (29)$$

and for the function  $Q(U(\mathbf{x}, t))$  or  $W(\Phi(\mathbf{x}, t))$ ,

$$\langle Q(U) \rangle_L = \int_{-\infty}^{+\infty} Q(V) F_U(V; \mathbf{x}, t) dV = \bar{\rho}(\mathbf{x}, t) \tilde{Q}(U(\mathbf{x}, t)) \quad (30)$$

$$\langle W(\Phi) \rangle_L = \int_{-\infty}^{+\infty} W(\Psi) F_{\Phi}(\Psi; \mathbf{x}, t) d\Psi = \bar{\rho}(\mathbf{x}, t) \tilde{W}(\Phi(\mathbf{x}, t))$$

Furthermore, we may consider the derivatives  $\nabla P$ ,  $\nabla U$ ,  $\nabla \Phi$  as the new random quantities and legitimately write

$$\langle \nabla P \rangle_L = \bar{\rho} \widetilde{\nabla P \nabla P}, \quad \langle \nabla U \rangle_L = \bar{\rho} \widetilde{\nabla U}, \quad \langle \nabla \Phi \rangle_L = \bar{\rho} \widetilde{\nabla \Phi} \quad (31)$$

However, the operation  $\langle \rangle_L$  does not have the differential commute property, i.e.

$$\langle \nabla P \rangle_L \neq \nabla \langle P \rangle_L, \quad \langle \nabla U \rangle_L \neq \nabla \langle U \rangle_L, \quad \langle \nabla \Phi \rangle_L \neq \nabla \langle \Phi \rangle_L \quad (32)$$

because  $\bar{\rho} \widetilde{\nabla P} \neq \nabla(\bar{\rho} \tilde{P})$ ,  $\bar{\rho} \widetilde{\nabla U} \neq \nabla(\bar{\rho} \tilde{U})$ ,  $\bar{\rho} \widetilde{\nabla \Phi} \neq \nabla(\bar{\rho} \tilde{\Phi})$ .

It can be verified that

$$\langle U_i U_j \rangle_L = \int_{-\infty}^{+\infty} V_i V_j F_U(V; \mathbf{x}, t) dV = \bar{\rho}(\mathbf{x}, t) \widetilde{U_i U_j}(\mathbf{x}, t) \quad (33)$$

We can also write  $\langle U_j \Phi_i \rangle_L$  for the joint variables as

$$\langle U_j \Phi_i \rangle_L = \int_{-\infty}^{+\infty} V_j \Psi_i F_{U, \Phi}(V, \Psi; \mathbf{x}, t) dV d\Psi = \bar{\rho}(\mathbf{x}, t) \widetilde{U_j \Phi_i}(\mathbf{x}, t) \quad (34)$$

where,  $F_{U, \Phi}(V, \Psi; \mathbf{x}, t)$  is the joint DW-FDF defined as

$$F_{U, \Phi}(V, \Psi; \mathbf{x}, t) = \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \delta(U(\mathbf{x}, t') - V) \delta(\Phi(\mathbf{x}, t') - \Psi) G(t - t') dt' \quad (35)$$

which also satisfies the normalization property:

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} F_{U, \Phi}(V, \Psi; \mathbf{x}, t) dV d\Psi = \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') G(t - t') dt' = \bar{\rho} \quad (36)$$

### 2.2.3 DW-FDF Mean $\langle \rangle_L$

Analogous to  $\int V f_U(V; \mathbf{x}, t) dV = \langle \mathbf{U}(\mathbf{x}, t) \rangle$ , which defines the statistical mean of the random velocity by its PDF  $f_U$ , we may refer the operation  $\langle \rangle_L$  as the ‘‘DW-FDF-mean’’, which defines the density weighted filtered turbulent variable, e.g.,  $\langle \mathbf{U} \rangle_L = \overline{\rho \mathbf{U}}$ ,  $\langle U_j \Phi_i \rangle_L = \overline{\rho U_j \Phi_i}$  (see Eqs. (28) to (34)). From Equation (35), we may follow Pope (Ref. 3) to define a ‘‘conditional’’ DW-FDF on the condition  $\Phi = \psi$  as

$$F_{U|\Phi}(V|\psi; \mathbf{x}, t) \equiv \frac{F_{U,\Phi}(V, \psi; \mathbf{x}, t)}{F_\Phi(\psi; \mathbf{x}, t)} \quad (37)$$

and the ‘‘conditional DW-FDF-mean’’ as

$$\begin{aligned} \langle \mathbf{U}(\mathbf{x}, t) | \psi \rangle_L &\equiv \int_{-\infty}^{+\infty} V F_{U|\Phi}(V|\psi; \mathbf{x}, t) dV = \frac{1}{F_\Phi(\psi; \mathbf{x}, t)} \int_{-\infty}^{+\infty} V F_{U,\Phi}(V, \psi; \mathbf{x}, t) dV \\ &= \frac{1}{F_\Phi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} V \rho(\mathbf{x}, t') \delta(\mathbf{U}(\mathbf{x}, t') - V) \delta(\Phi(\mathbf{x}, t') - \psi) G(t-t') dt' dV \\ &= \frac{1}{F_\Phi} \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \mathbf{U}(\mathbf{x}, t') \delta(\Phi(\mathbf{x}, t') - \psi) G(t-t') dt' \end{aligned} \quad (38)$$

Then we have

$$\int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \mathbf{U}(\mathbf{x}, t') f'_\Phi(\psi; \mathbf{x}, t') G(t-t') dt' = \int_{-\infty}^{+\infty} V F_{U,\Phi}(V, \psi; \mathbf{x}, t) dV = F_\Phi \cdot \langle \mathbf{U}(\mathbf{x}, t) | \psi \rangle_L \quad (39)$$

and

$$\begin{aligned} \int_{-\infty}^{+\infty} (F_\Phi \cdot \langle \mathbf{U}(\mathbf{x}, t) | \psi \rangle_L) d\psi &= \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} V F_{U,\Phi}(V, \psi; \mathbf{x}, t) dV d\psi \\ &= \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \mathbf{U}(\mathbf{x}, t') G(t-t') dt' \\ &= \bar{\rho}(\mathbf{x}, t) \tilde{U}(\mathbf{x}, t) \end{aligned} \quad (40)$$

Equation (39) can be extended to any other turbulent quantities, for example,  $\nabla P$ ,  $\nabla U$ ,  $\nabla \Phi$ ,  $S_i(\Phi)$ :

$$\begin{aligned} \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \nabla P(\mathbf{x}, t') f'_U(V; \mathbf{x}, t') G(t-t') dt' &= F_U \cdot \langle \nabla P | V \rangle_L \\ \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \nabla U(\mathbf{x}, t') f'_U(V; \mathbf{x}, t') G(t-t') dt' &= F_U \cdot \langle \nabla U | V \rangle_L \\ \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') \nabla \Phi(\mathbf{x}, t') f'_\Phi(\psi; \mathbf{x}, t') G(t-t') dt' &= F_\Phi \cdot \langle \nabla \Phi | \psi \rangle_L \\ \int_{-\infty}^{+\infty} \rho(\mathbf{x}, t') S_i(\Phi(\mathbf{x}, t')) f'_\Phi(\psi; \mathbf{x}, t') G(t-t') dt' &= F_\Phi \cdot \langle S_i(\Phi) | \psi \rangle_L = F_\Phi \cdot S_i(\psi) \end{aligned} \quad (41)$$

where  $\nabla P$ ,  $\nabla U$ ,  $\nabla \Phi$ , are viewed as the random variables in addition to  $P$ ,  $U$ ,  $\Phi$ .

### 3.0 Traditional DW-FDF Equations for $F_U(\mathbf{V}; \mathbf{x}, t), F_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$

In this section, we briefly review the traditional way of deriving DW-FDF equations starting from the equation of FG-PDF. The “exact” but not closed DW-FDF equations are derived, which are consistent with the traditional FPDF equations introduced by Jaber et al. (Ref. 1).

#### 3.1 Traditional DW-FDF Equation for $F_U(\mathbf{V}; \mathbf{x}, t)$

The transport equation for the fine grained PDF with the variable density  $\rho(\mathbf{x}, t)$  can be written as (see Equation (7)):

$$\frac{\partial \rho f'_U}{\partial t} + \frac{\partial \rho U_j f'_U}{\partial x_j} = -\frac{\partial}{\partial V_i} \left\{ f'_U \left( -\frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \left( 2\mu S_{ij} - \frac{2}{3} \mu \delta_{ij} S_{kk} \right) \right) \right\} \quad (42)$$

Where the right hand side of (42) is from the Navier-Stoke equation (47).

Applying the time filtering operation  $G(t-t')$  with a constant filter width on Equation (42) and using the sifting property of FG-PDF, we may obtain (noting that the differential commutation property of the time filtering operation is valid with a constant time filter width)

$$\frac{\partial F_U}{\partial t} + V_j \frac{\partial F_U}{\partial x_j} = -\frac{\partial}{\partial V_i} \left\{ -\int_{-\infty}^{\infty} \rho f'_U \left( \frac{1}{\rho} \frac{\partial P}{\partial x_i} \right) G(t-t') dt' + \int_{-\infty}^{\infty} \rho f'_U \left( \frac{1}{\rho} \frac{\partial}{\partial x_j} \left( 2\mu S_{ij} - \frac{2}{3} \mu \delta_{ij} S_{kk} \right) \right) G(t-t') dt' \right\}$$

According to Equation (41), the DW-FDF equation for the velocity can be written as

$$\frac{\partial F_U}{\partial t} + V_j \frac{\partial F_U}{\partial x_j} = -\frac{\partial}{\partial V_i} \left\{ -F_U \cdot \left\langle \frac{1}{\rho} \frac{\partial P}{\partial x_i} \middle| \mathbf{V} \right\rangle_L + F_U \cdot \left\langle \frac{1}{\rho} \frac{\partial}{\partial x_j} \left( 2\mu S_{ij} - \frac{2}{3} \mu \delta_{ij} S_{kk} \right) \middle| \mathbf{V} \right\rangle_L \right\} \quad (43)$$

At this point, the velocity DW-FDF equation is general but unclosed because of the unknown terms of the conditional DW-FDF means. The last term in Equation (43) is referred as the molecular mixing term and was modeled in various empirical ways by different researchers. Later, we will see that, when using a different way to derive the DW-FDF equation, the molecular mixing term is automatically closed with no need of modeling. The same happens to the pressure gradient term.

#### 3.2 Traditional DW-FDF Equation for $F_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$

Applying the time filtering  $G(t-t')$  on the following FG-PDF equation for scalars,

$$\frac{\partial \rho f'_\Phi}{\partial t} + \frac{\partial \rho U_j f'_\Phi}{\partial x_j} = -\frac{\partial}{\partial \psi_i} \left\{ f'_\Phi \left( \frac{\partial}{\partial x_j} \left( \rho \Gamma_{(i)} \frac{\partial \Phi_i}{\partial x_j} \right) + \rho S_i(\Phi(\mathbf{x}, t)) \right) \right\} \quad (44)$$

we obtain the DW-FDF equation for the turbulent species:

$$\frac{\partial F_\Phi}{\partial t} + \frac{\partial \left( F_\Phi \langle U_j | \boldsymbol{\psi} \rangle_L \right)}{\partial x_j} = -\frac{\partial}{\partial \psi_i} \left\{ F_\Phi \cdot \left\langle \frac{1}{\rho} \frac{\partial}{\partial x_j} \rho \Gamma_{(i)} \frac{\partial \Phi_i}{\partial x_j} \middle| \boldsymbol{\psi} \right\rangle_L + F_\Phi \cdot S_i(\boldsymbol{\psi}) \right\} \quad (45)$$

where  $S_{N+1}(\boldsymbol{\psi}) = 0$ . Equation (45) is also unclosed, because the conditional DW-FDF means need to be modeled. Later, we will also see that using a different derivation of DW-FDF equation, the molecular mixing term is closed.

## 4.0 DW-FDF Equations Derived From Filtered Navier-Stokes Equations

### 4.1 Filtered Compressible Navier-Stokes Equations

The Navier-Stokes equations for a compressible reacting flow can be written as

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho U_j}{\partial x_j} = 0 \quad (46)$$

$$\frac{\partial \rho U_i}{\partial t} + \frac{\partial \rho U_i U_j}{\partial x_j} = -\frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \left( 2\rho \nu (S_{ij} - \frac{1}{3} \delta_{ij} S_{kk}) \right) \quad (47)$$

$$\frac{\partial \rho e}{\partial t} + \frac{\partial \rho U_i e}{\partial x_i} = -\frac{\partial q_i}{\partial x_i} + P S_{kk} + 2\rho \nu \left( S_{ij} S_{ij} - \frac{1}{3} S_{ii} S_{kk} \right) + Q \quad (48)$$

$$\frac{\partial \rho \Phi_m}{\partial t} + \frac{\partial \rho U_i \Phi_m}{\partial x_i} = \frac{\partial}{\partial x_i} \left( \rho \Gamma^{(m)} \frac{\partial \Phi_m}{\partial x_i} \right) + W_m \quad m = 1, 2, \dots, N \quad (49)$$

$$P = \rho R \sum_{n=1}^N \frac{\Phi_n T}{w_n} \quad (50)$$

$$q_i = -\rho \kappa c_v \frac{\partial T}{\partial x_i} - \sum_{m=1}^N \rho \Gamma^{(m)} h_m \frac{\partial \Phi_m}{\partial x_i} \quad (51)$$

Applying the time filtering operation with a constant filter width on the above equations, we obtain the following filtered Navier-Stokes equations:

$$\frac{\partial \bar{\rho}}{\partial t} + \frac{\partial \bar{\rho} \tilde{U}_j}{\partial x_j} = 0 \quad (52)$$

$$\frac{\partial \bar{\rho} \tilde{U}_i}{\partial t} + \frac{\partial \bar{\rho} \tilde{U}_i \tilde{U}_j}{\partial x_j} = -\frac{\partial \bar{P}}{\partial x_i} + \frac{\partial}{\partial x_j} \left( \overline{2\rho \nu (S_{ij} - \frac{1}{3} \delta_{ij} S_{kk})} \right) \quad (53)$$

$$\frac{\partial \bar{\rho} \tilde{e}}{\partial t} + \frac{\partial \bar{\rho} \tilde{U}_i \tilde{e}}{\partial x_i} = -\frac{\partial \bar{q}_i}{\partial x_i} + \overline{P S_{kk}} + \overline{2\rho \nu \left( S_{ij} S_{ij} - \frac{1}{3} S_{ii} S_{kk} \right)} + \bar{Q} \quad (54)$$

$$\frac{\partial \bar{\rho} \tilde{\Phi}_m}{\partial t} + \frac{\partial \bar{\rho} \tilde{U}_i \tilde{\Phi}_m}{\partial x_i} = \frac{\partial}{\partial x_i} \left( \overline{\rho \Gamma^{(m)} \frac{\partial \Phi_m}{\partial x_i}} \right) + \bar{W}_m \quad m = 1, 2, \dots, N \quad (55)$$

where

$$\bar{P} = \bar{\rho} R \sum_{n=1}^N \frac{\widetilde{\Phi_n T}}{w_n} = \frac{\bar{\rho} R}{c_v} \sum_{n=1}^N \frac{\widetilde{\Phi_n e}}{w_n}$$

or

$$\bar{P} = \frac{\bar{\rho} R}{c_v} \sum_{n=1}^N \frac{\widetilde{\Phi_n \Phi_{N+1}}}{w_n}$$

$$\bar{q}_i = -\rho \kappa c_v \frac{\partial T}{\partial x_i} - \sum_{m=1}^N \overline{\rho \Gamma^{(m)} h_m \frac{\partial \Phi_m}{\partial x_i}} \quad (57)$$

In the above equations,  $\kappa$ ,  $\nu$  and  $\Gamma^{(m)}$  are the molecular heat conductivity, kinematic viscosity and the  $m$ -th species diffusivity, they have the same dimension (i.e., velocity  $\cdot$  length). The  $h_m$ ,  $T$  are the enthalpy of species and temperature,  $Q$  is the radiation rate,  $W_m = \rho S_m$  is the chemical generation rate of the  $m$ -th species,  $\Phi_{N+1}$  represents the internal energy  $e$ ,  $R$  is the universal gas constant. These equations are general; however, unlike the constant density flows, further approximations for the terms on their right hand side are required in order to complete the filtering process. One of such approximations leads to

$$2\rho\nu \left( S_{ij} - \frac{1}{3} \delta_{ij} S_{kk} \right) \approx \mu \left( \frac{\partial \tilde{U}_i}{\partial x_j} + \frac{\partial \tilde{U}_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial \tilde{U}_k}{\partial x_k} \right) \quad (58)$$

In which, we have basically neglected the variations of  $\mu$  and  $\rho$  during the filtering process, the value of  $\mu$  will be considered as the function of  $\bar{P}$ ,  $\tilde{T}$ ,  $\dots$ . Another type of approximation writes

$$2\rho\nu \left( S_{ij} - \frac{1}{3} \delta_{ij} S_{kk} \right) \approx \nu \left( \frac{\partial \bar{\rho} \tilde{U}_i}{\partial x_j} + \frac{\partial \bar{\rho} \tilde{U}_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial \bar{\rho} \tilde{U}_k}{\partial x_k} \right) \quad (59)$$

Similarly,

$$\bar{q}_i = -\rho \kappa c_v \frac{\partial T}{\partial x_i} - \sum_{m=1}^N \overline{\rho \Gamma^{(m)} h_m \frac{\partial \Phi_m}{\partial x_i}} \approx -\kappa c_v \frac{\partial \bar{\rho} \tilde{T}}{\partial x_i} - \sum_{m=1}^N \Gamma^{(m)} \frac{\partial \bar{\rho} \widetilde{h_m \Phi_m}}{\partial x_i} \quad (60)$$

$$\overline{\rho \Gamma^{(m)} \frac{\partial \Phi_m}{\partial x_i}} \approx \Gamma^{(m)} \frac{\partial \bar{\rho} \tilde{\Phi}_m}{\partial x_i} \quad (61)$$

Furthermore, invoking the turbulent kinetic energy dissipation rate:

$$2\rho\nu \left( S_{ij} S_{ij} - \frac{1}{3} S_{ii} S_{kk} \right) \equiv \bar{\rho} \tilde{\varepsilon} \quad (62)$$

Where  $\nu$ ,  $\kappa$ ,  $c_v$  and  $\Gamma^{(m)}$  are considered as the function of  $\bar{P}$ ,  $\tilde{T}$ ,  $\dots$ .

Therefore, the filtered Navier-Stokes equations can approximately be written as

$$\frac{\partial \bar{\rho}}{\partial t} + \frac{\partial \bar{\rho} \tilde{U}_j}{\partial x_j} = 0 \quad (63)$$

$$\frac{\partial \bar{\rho} \tilde{U}_i}{\partial t} + \frac{\partial \bar{\rho} \widetilde{U_i U_j}}{\partial x_j} = -\frac{\partial \bar{P}}{\partial x_i} + \frac{\partial}{\partial x_j} \left[ v \left( \frac{\partial \bar{\rho} \tilde{U}_i}{\partial x_j} + \frac{\partial \bar{\rho} \tilde{U}_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial \bar{\rho} \tilde{U}_k}{\partial x_k} \right) \right] \quad (64)$$

$$\frac{\partial \bar{\rho} \tilde{e}}{\partial t} + \frac{\partial \bar{\rho} \widetilde{U_i e}}{\partial x_i} = -\frac{\partial \bar{q}_i}{\partial x_i} + \overline{PS_{kk}} + \bar{\rho} \tilde{\epsilon} + \bar{Q} \quad (65)$$

$$\frac{\partial \bar{\rho} \tilde{\Phi}_m}{\partial t} + \frac{\partial \bar{\rho} \widetilde{U_i \Phi_m}}{\partial x_i} = \frac{\partial}{\partial x_i} \left( \Gamma^{(m)} \frac{\partial \bar{\rho} \tilde{\Phi}_m}{\partial x_i} \right) + \bar{\rho} \tilde{S}_m \quad m = 1, 2, \dots, N \quad (66)$$

$$\bar{P} = \bar{\rho} R \sum_{n=1}^N \frac{\widetilde{\Phi_n T}}{w_n} = \frac{\bar{\rho} R}{c_v} \sum_{n=1}^N \frac{\widetilde{\Phi_n e}}{w_n} \quad (67)$$

or

$$\bar{P} = \frac{\bar{\rho} R}{c_v} \sum_{n=1}^N \frac{\widetilde{\Phi_n \Phi_{N+1}}}{w_n}$$

$$\bar{q}_i = -\kappa c_v \frac{\partial \bar{\rho} \tilde{T}}{\partial x_i} - \sum_{m=1}^N \Gamma^{(m)} \frac{\partial \bar{\rho} \widetilde{h_m \Phi_m}}{\partial x_i} \quad (68)$$

These equations are still considered as quite general, because i) they are exact if the flow becomes incompressible, ii) all the approximations made in Equations (64), (65) and (66) are related only to the molecular diffusion terms that are less important and even negligible comparing with the convection terms on the left hand side for turbulent flows at high Reynolds number (see Tennekes and Lumley (Ref. 7) and Pope (Ref. 3)). For the LES simulation, Equation (63) to (66) are often used together with the further approximations for (67) and (68):

$$\bar{P} = \overline{\rho R \sum_{n=1}^N \frac{\Phi_n T}{w_n}} = \overline{\left( \frac{\rho R T}{M} \right)} \approx \frac{\bar{\rho} R \tilde{T}}{\bar{M}}, \quad \bar{M} = \sum_{n=1}^N \frac{\tilde{\Phi}_n}{w_n} \quad (69)$$

$$\bar{q}_i = -\kappa c_v \frac{\partial \bar{\rho} \tilde{T}}{\partial x_i} \quad (70)$$

The momentum flux  $\bar{\rho} \widetilde{U_i U_j}$ , the energy flux  $\bar{\rho} \widetilde{U_i e}$  and the species flux  $\bar{\rho} \widetilde{U_i \Phi_m}$  are considered to be critically important in LES simulations and should be carefully modeled. Many models in the literature, from the simplest Smagorinsky (Ref. 8) model to the complex two-equation models (Refs. 9 and 6) including the dynamic procedure (Ref. 10) have been suggested. In the next Section 4.2 and 4.3, we will derive the DW-FDF equations directly from Equations (63) to (68).

## 4.2 DW-FDF Equation for $F_U(\mathbf{V}; x, t)$

Using Equations (28) and (33), the left hand side of Equation (64) can be written as

$$\frac{\partial \bar{\rho} \tilde{U}_i}{\partial t} + \frac{\partial \bar{\rho} \widetilde{U_i U_j}}{\partial x_j} = \frac{\partial}{\partial t} \int_{-\infty}^{\infty} V_i F_U d\mathbf{V} + \frac{\partial}{\partial x_j} \int_{-\infty}^{\infty} V_i V_j F_U d\mathbf{V} = \int_{-\infty}^{\infty} V_i \left( \frac{\partial F_U}{\partial t} + V_j \frac{\partial F_U}{\partial x_j} \right) d\mathbf{V} \quad (71)$$

The pressure gradient term can be written as using (67)

$$-\frac{\partial \bar{P}}{\partial x_i} = -\frac{\partial}{\partial x_i} \left( \frac{\bar{\rho} R}{c_v} \sum_{n=1}^N \frac{\overline{\Phi_n \Phi_{N+1}}}{w_n} \right) = \begin{cases} \int_{-\infty}^{\infty} V_i \frac{\partial^2}{\partial V_k \partial x_k} \left[ \sum_{n=1}^N \frac{R}{c_v w_n} \left( \int_{-\infty}^{\infty} \Psi_n \Psi_{N+1} F_{U,\Phi}(\Psi, \mathbf{V}; \mathbf{x}, t) d\Psi \right) \right] d\mathbf{V} \\ \text{or} \\ \int_{-\infty}^{\infty} V_i \frac{\partial^2}{\partial V_k \partial x_k} \left[ \sum_{n=1}^N \frac{R}{c_v w_n} \langle \Phi_n \Phi_{N+1} | \mathbf{V} \rangle_L F_U \right] d\mathbf{V} \end{cases} \quad (72)$$

During the above arrangement, no approximations have been made other than the integration by parts and a zero integration property like Eq.(74).

Note that the pressure gradient term can be closed only when the joint DW-FDF,  $F_{U,\Phi}$ , is considered, otherwise, the ‘‘conditional DW-FDF mean’’ will be unavoidable. Now the molecular mixing term in Equation (64) can be written as

$$\begin{aligned} & \frac{\partial}{\partial x_j} \mathbf{v} \left( \frac{\partial \bar{\rho} \tilde{U}_i}{\partial x_j} + \frac{\partial \bar{\rho} \tilde{U}_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial \bar{\rho} \tilde{U}_m}{\partial x_m} \right) \\ &= \frac{\partial}{\partial x_j} \mathbf{v} \left( \frac{\partial}{\partial x_j} \int_{-\infty}^{\infty} V_i F_U d\mathbf{V} + \frac{\partial}{\partial x_i} \int_{-\infty}^{\infty} V_j F_U d\mathbf{V} - \frac{2}{3} \delta_{ij} \frac{\partial}{\partial x_m} \int_{-\infty}^{\infty} V_m F_U d\mathbf{V} \right) \\ &= \begin{cases} \int_{-\infty}^{\infty} V_i \left( \frac{\partial}{\partial x_j} \mathbf{v} \frac{\partial F_U}{\partial x_j} \right) d\mathbf{V} - \frac{\partial}{\partial x_j} \mathbf{v} \left( \frac{\partial}{\partial x_k} \int_{-\infty}^{\infty} V_i \frac{\partial}{\partial V_k} (V_j F_U) d\mathbf{V} - \frac{2}{3} \delta_{kj} \frac{\partial}{\partial x_m} \int_{-\infty}^{\infty} V_i \frac{\partial}{\partial V_k} (V_m F_U) d\mathbf{V} \right) \\ \text{or} \\ -\frac{\partial}{\partial x_j} \mathbf{v} \left( \frac{\partial}{\partial x_j} \int_{-\infty}^{\infty} V_i \frac{\partial}{\partial V_k} (V_k F_U) d\mathbf{V} + \frac{\partial}{\partial x_k} \int_{-\infty}^{\infty} V_i \frac{\partial}{\partial V_k} (V_j F_U) d\mathbf{V} - \frac{2}{3} \delta_{kj} \frac{\partial}{\partial x_m} \int_{-\infty}^{\infty} V_i \frac{\partial}{\partial V_k} (V_m F_U) d\mathbf{V} \right) \\ \int_{-\infty}^{\infty} V_i \left( \frac{\partial}{\partial x_j} \mathbf{v} \frac{\partial F_U}{\partial x_j} \right) d\mathbf{V} - \int_{-\infty}^{\infty} V_i \frac{\partial}{\partial x_j} \left( \mathbf{v} \frac{\partial^2 V_j F_U}{\partial V_k \partial x_k} \right) d\mathbf{V} + \int_{-\infty}^{\infty} V_i \frac{2}{3} \delta_{kj} \frac{\partial}{\partial x_j} \left( \mathbf{v} \frac{\partial^2 V_m F_U}{\partial V_k \partial x_m} \right) d\mathbf{V} \\ \text{or} \\ -\int_{-\infty}^{\infty} V_i \frac{\partial}{\partial x_j} \left( \mathbf{v} \frac{\partial^2 V_k F_U}{\partial V_k \partial x_j} \right) d\mathbf{V} - \int_{-\infty}^{\infty} V_i \frac{\partial}{\partial x_j} \left( \mathbf{v} \frac{\partial^2 V_j F_U}{\partial V_k \partial x_k} \right) d\mathbf{V} + \int_{-\infty}^{\infty} V_i \frac{2}{3} \delta_{kj} \frac{\partial}{\partial x_j} \left( \mathbf{v} \frac{\partial^2 V_m F_U}{\partial V_k \partial x_m} \right) d\mathbf{V} \end{cases} \quad (73) \end{aligned}$$

Note, on the third line of (73), we have applied the integration by parts and the following type of zero integration similar to the one used in PDF formulations (Ref. 3):

$$\int_{-\infty}^{\infty} \frac{\partial}{\partial V_k} (V_i V_k F_U) d\mathbf{V} = 0 \quad (74)$$

Finally, collecting the terms that are in the integrands and factored by  $V_i$ , we obtain the transport equation for  $F_U(\mathbf{V}; \mathbf{x}, t)$  as

$$\begin{aligned} \frac{\partial F_U}{\partial t} + V_j \frac{\partial F_U}{\partial x_j} &= \frac{\partial^2}{\partial V_k \partial x_k} \left[ \sum_{n=1}^N \frac{R}{c_v w_n} \langle \Phi_n \Phi_{N+1} | \mathbf{V} \rangle_L F_U \right] + \frac{\partial}{\partial x_j} \left( v \frac{\partial F_U}{\partial x_j} \right) \\ &\quad - \frac{\partial}{\partial V_k} \left( V_j \frac{\partial}{\partial x_j} v \frac{\partial F_U}{\partial x_k} \right) + \frac{\partial}{\partial V_k} \left( \frac{2}{3} \delta_{kj} V_m \frac{\partial}{\partial x_j} v \frac{\partial F_U}{\partial x_m} \right) \end{aligned} \quad (75)$$

or

$$\begin{aligned} \frac{\partial F_U}{\partial t} + V_j \frac{\partial F_U}{\partial x_j} &= \frac{\partial^2}{\partial V_k \partial x_k} \left[ \sum_{n=1}^N \frac{R}{c_v w_n} \langle \Phi_n \Phi_{N+1} | \mathbf{V} \rangle_L F_U \right] - \frac{\partial}{\partial V_k} \left( V_k \frac{\partial}{\partial x_j} v \frac{\partial F_U}{\partial x_j} \right) \\ &\quad - \frac{\partial}{\partial V_k} \left( V_j \frac{\partial}{\partial x_j} v \frac{\partial F_U}{\partial x_k} \right) + \frac{\partial}{\partial V_k} \left( \frac{2}{3} \delta_{kj} V_m \frac{\partial}{\partial x_j} v \frac{\partial F_U}{\partial x_m} \right) \end{aligned}$$

In Equation (75), all the terms are closed, except for the one involving the conditional DW-FDF mean originating from the pressure gradient. It should be noticed that one of the most important terms in the momentum equation, i.e.,  $\bar{\rho} \widetilde{U_i U_j}$ , now is closed in the corresponding DW-FDF equation. And the less important molecular diffusion terms remain in the closed form.

### 4.3 DW-FDF Equation for $F_\Phi(\boldsymbol{\psi}; \mathbf{x}, t)$

Similarly, we may obtain the DW-FDF equations for the scalars (i.e. species and internal energy) from Equations (65), (66) as follows: first, we write the terms on the left hand side of Equation (66) as

$$\begin{aligned} \frac{\partial \bar{\rho} \widetilde{\Phi}_m}{\partial t} &= \frac{\partial}{\partial t} \int_{-\infty}^{\infty} \psi_m F_\Phi d\boldsymbol{\psi} = \int_{-\infty}^{\infty} \psi_m \frac{\partial F_\Phi}{\partial t} d\boldsymbol{\psi} \quad (76) \\ \frac{\partial \bar{\rho} \widetilde{U_i \Phi}_m}{\partial x_i} &= \frac{\partial}{\partial x_i} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} V_i \psi_m F_{U, \Phi} d\mathbf{V} d\boldsymbol{\psi} = \begin{cases} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \psi_m \left( V_i \frac{\partial}{\partial x_i} F_{U, \Phi} \right) d\mathbf{V} d\boldsymbol{\psi} \\ \text{or} \\ \int_{-\infty}^{\infty} \psi_m \left( \frac{\partial}{\partial x_i} (F_\Phi \langle U_i | \boldsymbol{\psi} \rangle_L) \right) d\boldsymbol{\psi} \end{cases} \quad (77) \end{aligned}$$

Then, the terms on the right hand side of (66) can be written as

$$\frac{\partial}{\partial x_i} \left( \Gamma^{(m)} \frac{\partial \bar{\rho} \widetilde{\Phi}_m}{\partial x_i} \right) = \frac{\partial}{\partial x_i} \left( \Gamma^{(m)} \frac{\partial}{\partial x_i} \int_{-\infty}^{\infty} \psi_m F_\Phi d\boldsymbol{\psi} \right) = \begin{cases} \int_{-\infty}^{\infty} \psi_m \frac{\partial}{\partial x_i} \left( \Gamma^{(m)} \frac{\partial F_\Phi}{\partial x_i} \right) d\boldsymbol{\psi} \\ \text{or} \\ - \int_{-\infty}^{\infty} \psi_m \frac{\partial}{\partial x_i} \left( \Gamma^{(m)} \frac{\partial^2 \psi_k F_\Phi}{\partial \psi_k \partial x_i} \right) d\boldsymbol{\psi} \end{cases} \quad (78)$$

$$\bar{\rho} \tilde{S}_m = \int_{-\infty}^{\infty} S_m(\boldsymbol{\psi}) F_{\Phi} d\boldsymbol{\psi} = - \int_{-\infty}^{\infty} \psi_m \frac{\partial(S_k F_{\Phi})}{\partial \psi_k} d\boldsymbol{\psi} \quad (79)$$

Where in Equations (78) and (79), we have applied the integration by parts and zero integrations similar to (74). Collecting all the integrand terms that factored by  $\psi_m$ , we obtain

$$\frac{\partial F_{\Phi}}{\partial t} + \frac{\partial(F_{\Phi} \langle U_i | \boldsymbol{\Psi} \rangle_L)}{\partial x_i} = \left\{ \frac{\partial}{\partial x_i} \left( \Gamma^{(m)} \frac{\partial F_{\Phi}}{\partial x_i} \right) - \frac{\partial}{\partial \psi_k} [F_{\Phi} \cdot S_k(\boldsymbol{\psi})] \right\}, \quad m = 1, 2, \dots, N+1$$

or

$$\frac{\partial F_{\Phi}}{\partial t} + \frac{\partial(F_{\Phi} \langle U_i | \boldsymbol{\Psi} \rangle_L)}{\partial x_i} = - \frac{\partial}{\partial \psi_k} \left\{ \frac{\partial}{\partial x_i} \left( \Gamma^{(m)} \psi_k \frac{\partial F_{\Phi}}{\partial x_i} \right) + F_{\Phi} \cdot S_k(\boldsymbol{\psi}) \right\}, \quad m = 1, 2, \dots, N+1$$

This equation also represents the equation of internal energy  $m = N + 1$ , where  $S_{N+1}(\boldsymbol{\psi}) = 0$  and other source terms in Equation (65) are neglected as suggested by Jaberi et al. (Ref. 1). Equation (80) is essentially closed if we consider the joint DW-FDF  $F_{U,\Phi}$ . For the marginal  $F_{\Phi}$ , the convection term is not closed because of the conditional DW-FDF mean  $\langle U_i | \boldsymbol{\Psi} \rangle_L$ . Then, this critically important term, corresponding to  $\bar{\rho} \widetilde{U_i \Phi}_m$  in Equation (66), must be carefully modeled while the less important molecular diffusion term remains in the closed form. In addition, we noticed that the equally important chemistry source term  $\bar{\rho} \widetilde{S_m(\Phi)}$  in Equation (66) contains complex processes of turbulence-chemistry interaction, which is considered as very hard to be modeled. However, it is closed in the DW-FDF equation with no need of modeling. This direct calculation of turbulence-chemistry interaction represents one of the unique features of DW-FDF methodology.

#### 4.4 Modeling of Unclosed Terms

Consider the approximation described by Equation (69), i.e.  $\bar{P} \approx \bar{\rho} R \tilde{T} / \bar{M}$ , we may write from Equation (72)

$$\begin{aligned} -\frac{\partial \bar{P}}{\partial x_i} &= -\frac{\partial}{\partial x_i} \left( \frac{\bar{\rho} R}{c_v} \sum_{n=1}^N \frac{\widetilde{\Phi_n \Phi_{N+1}}}{w_n} \right) \approx -\frac{\partial}{\partial x_i} \left( \frac{\bar{\rho} R \tilde{\Phi}_{N+1}}{c_v \bar{M}} \right) \\ &= -\frac{\partial}{\partial x_i} \frac{R}{c_v \bar{M}} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \psi_{N+1} F_{U,\Phi} d\boldsymbol{\psi} d\mathbf{V} \\ &= -\frac{\partial}{\partial x_i} \frac{R}{c_v \bar{M}} \int_{-\infty}^{\infty} \langle \Phi_{N+1} | \mathbf{V} \rangle_L F_U d\mathbf{V} \\ &= \int_{-\infty}^{\infty} V_i \frac{\partial^2}{\partial V_k \partial x_k} \left[ \frac{R}{c_v \bar{M}} \langle \Phi_{N+1} | \mathbf{V} \rangle_L F_U \right] d\mathbf{V} \\ &\approx \int_{-\infty}^{\infty} V_i \frac{\partial^2}{\partial V_k \partial x_k} \left[ \frac{R \tilde{\epsilon}}{c_v \bar{M}} F_U \right] d\mathbf{V} \end{aligned} \quad (81)$$

The last step in Equation (81) employs a rough approximation:

$$\langle \Phi_{N+1} | \mathbf{V} \rangle_L \approx \tilde{\Phi}_{N+1} = \tilde{\epsilon} \quad (82)$$

As for the convection term in the species Equation (80),  $F_\Phi \langle U_i | \Psi \rangle_L$ , we may start from a more general model for the term  $\overline{\rho U_i \Phi_m}$  (see Ref. 6):

$$\overline{\rho U_i \Phi_m} = \overline{\rho} \tilde{U}_i \tilde{\Phi}_m - \Gamma_T^{(m)} \frac{\partial \overline{\rho} \tilde{\Phi}_m}{\partial x_i} - \Gamma_T^{(m)} \frac{k}{\epsilon} (c_1 \tilde{S}_{ij} + c_2 \tilde{\Omega}_{ij}) \frac{\partial \overline{\rho} \tilde{\Phi}_m}{\partial x_j} \quad (83)$$

Where  $c_1 = c_2 = -0.24$ . This will lead to the following model by directly applying the Equations (27) and (39) described in Sections 2.2.2 and 2.2.3:

$$F_\Phi \langle U_i | \Psi \rangle_L = \tilde{U}_i F_\Phi - \left[ \Gamma_T^{(m)} \frac{\partial F_\Phi}{\partial x_i} \right] + \frac{\partial}{\partial \Psi_k} \left[ \Gamma_T^{(m)} \frac{k}{\epsilon} (c_1 \tilde{S}_{ij} + c_2 \tilde{\Omega}_{ij}) \Psi_k \frac{\partial F_\Phi}{\partial x_j} \right]$$

or

$$F_\Phi \langle U_i | \Psi \rangle_L = \tilde{U}_i F_\Phi + \frac{\partial}{\partial \Psi_k} \left[ \Gamma_T^{(m)} \Psi_k \frac{\partial F_\Phi}{\partial x_i} \right] + \frac{\partial}{\partial \Psi_k} \left[ \Gamma_T^{(m)} \frac{k}{\epsilon} (c_1 \tilde{S}_{ij} + c_2 \tilde{\Omega}_{ij}) \Psi_k \frac{\partial F_\Phi}{\partial x_j} \right] \quad (84)$$

#### 4.5 Summary

With the models given by Equations (81) and (84), the marginal DW-FDF equations for  $F_U(\mathbf{V}; \mathbf{x}, t)$  and  $F_\Phi(\Psi; \mathbf{x}, t)$  can be written as

$$\begin{aligned} \frac{\partial F_U}{\partial t} + V_j \frac{\partial F_U}{\partial x_j} &= \frac{\partial^2}{\partial V_k \partial x_k} \left[ \frac{R \tilde{\Phi}_{N+1}}{c_v \bar{M}} F_U \right] + \frac{\partial}{\partial x_j} \left( \mathbf{v} \frac{\partial F_U}{\partial x_j} \right) \\ &\quad - \frac{\partial}{\partial V_k} \left( V_j \frac{\partial}{\partial x_j} \mathbf{v} \frac{\partial F_U}{\partial x_k} \right) + \frac{\partial}{\partial V_k} \left( \frac{2}{3} \delta_{kj} V_m \frac{\partial}{\partial x_j} \mathbf{v} \frac{\partial F_U}{\partial x_m} \right) \end{aligned}$$

or

$$\begin{aligned} \frac{\partial F_U}{\partial t} + V_j \frac{\partial F_U}{\partial x_j} &= \frac{\partial^2}{\partial V_k \partial x_k} \left[ \frac{R \tilde{\Phi}_{N+1}}{c_v \bar{M}} F_U \right] - \frac{\partial}{\partial V_k} \left( V_k \frac{\partial}{\partial x_j} \mathbf{v} \frac{\partial F_U}{\partial x_j} \right) \\ &\quad - \frac{\partial}{\partial V_k} \left( V_j \frac{\partial}{\partial x_j} \mathbf{v} \frac{\partial F_U}{\partial x_k} \right) + \frac{\partial}{\partial V_k} \left( \frac{2}{3} \delta_{kj} V_m \frac{\partial}{\partial x_j} \mathbf{v} \frac{\partial F_U}{\partial x_m} \right) \end{aligned} \quad (85)$$

$$\frac{\partial F_\Phi}{\partial t} + \frac{\partial(\tilde{U}_i F_\Phi)}{\partial x_i} = \left\{ \frac{\partial}{\partial x_i} \left( \left( \Gamma^{(m)} + \Gamma_T^{(m)} \right) \frac{\partial F_\Phi}{\partial x_i} \right) \right\} - \frac{\partial}{\partial \psi_k} (F_\Phi \cdot S_k(\boldsymbol{\Psi}))$$

$$- \frac{\partial}{\partial \psi_k} \left\{ \psi_k \frac{\partial}{\partial x_i} \left( \Gamma_T^{(m)} \frac{k}{\varepsilon} (c_1 \tilde{S}_{ij} + c_2 \tilde{\Omega}_{ij}) \frac{\partial F_\Phi}{\partial x_j} \right) \right\}, \quad m = 1, 2, \dots, N+1$$

or (86)

$$\frac{\partial F_\Phi}{\partial t} + \frac{\partial(\tilde{U}_i F_\Phi)}{\partial x_i} = - \frac{\partial}{\partial \psi_k} \left\{ \psi_k \frac{\partial}{\partial x_i} \left( \left( \Gamma^{(m)} + \Gamma_T^{(m)} \right) \frac{\partial F_\Phi}{\partial x_i} \right) + F_\Phi \cdot S_k(\boldsymbol{\Psi}) \right\}$$

$$- \frac{\partial}{\partial \psi_k} \left\{ \psi_k \frac{\partial}{\partial x_i} \left( \Gamma_T^{(m)} \frac{k}{\varepsilon} (c_1 \tilde{S}_{ij} + c_2 \tilde{\Omega}_{ij}) \frac{\partial F_\Phi}{\partial x_j} \right) \right\}, \quad m = 1, 2, \dots, N+1$$

It can be verified that the DW-FDF Equations (85) and (86) can exactly deduce the filtered compressible Navier-Stokes equations (64) to (66) with the assumed approximations of (81) and (83). However, by no means, the models described by Equations (81) and (84) are unique. Furthermore, the variables ( $\tilde{\Phi}_{N+1}$ ,  $\tilde{U}_i$ ,  $\tilde{S}_{ij}$  and  $\tilde{\Omega}_{ij}$ ) are considered as available during the solution procedure of the DW-FDF equations.

## 5.0 Concluding Remarks

We have revisited the derivations of the traditional DW-FDF or FMDF equations by starting from the equation of FG-PDF that contains all the terms on the right hand side of the Navier-Stokes equations, see Equations (42) and (44). The resulting FMDF equations contain the “conditional DW-FDF mean” quantities for all the terms on the right hand side (except for the reaction term), see Equations (43), (45), which need empirical models to make the equations closed.

From the relationship between the DW-FDF and the filtered turbulent variables, it is possible to construct the DW-FDF equations directly from the filtered compressible Navier-Stokes equations. Such DW-FDF equations have an outstanding feature that all the terms that were not closed on the right hand side of traditional FMDF equations are now in the closed form, see Equations (75) and (80), except for the pressure gradient term that involves joint DW-FDF.

In the marginal DW-FDF equations, the two unclosed terms, one related to the pressure gradient and the other related to the species convection, are expected to be more important than the molecular “mixing” or “diffusion” terms, especially in the case of high Reynolds number. Their physics-based models, such as Equations (81) and (84), should be further developed and evaluated.

The fundamental differences between the DW-FDF (a random quantity) and the PDF (a deterministic quantity) warrant further investigation on their respective solution procedure using the stochastic differential equation methods.

## References

1. Jaber, F.A., Colucci, P.J., James, S., Givi, P. and Pope, S.B., “Filtered mass density function for Large-eddy simulation of turbulent reacting flows,” *J. Fluid Mech.*, vol. 401, pp. 85–121, 1999.
2. Colluci, P.J., Jaber, F.A., Givi, P. and Pope, S., “Filtered density function for large eddy simulation of turbulent reacting flow,” *Phys. Fluids* 10, 499–515, 1998.
3. Pope, S.B., “*Turbulent Flows*,” Cambridge University Press, 2000.
4. Shih, T.-H. and Liu, N.-S. “Conservational PDF equations of turbulence,” NASA/TM—2010-216368.
5. Liu, N.-S. and Shih, T.-H., “Turbulence Modeling for Very Large-Eddy Simulation,” *AIAA Journal*, Vol. 44, No. 4, April 2006.

6. Shih, T.-H. and Liu, N.-S., "A non-linear Dynamic Subscale Model for Partially Resolved Numerical Simulation (PRNS)/Very Large Eddy Simulation (VLES) of Internal Non-Reacting Flows," NASA/TM—2010-216323, May 2010.
7. Tennekes, H. and Lumley, J.L., A First Course in Turbulence, The MIT Press, 1972.
8. Smagorinsky, J., "General Circulation Experiments with the Primitive Equations," Mon. Wea., 91, 99, 1963.
9. Speziale, C.G., "Turbulence Modeling for Time-Dependent RANS and VLES: A Review," AIAA J., Vol. 36, No. 2, 1998.
10. Germano, M., Piomelli, U., Moin, P., and Cabot, W.H., "A Dynamic Subscale Eddy Viscosity Model," Proc. Summer Workshop, Center for Turbulence Research, Stanford CA, 1990.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188		
<p>The public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.</p> <p>PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.</p>					
<b>1. REPORT DATE (DD-MM-YYYY)</b> 01-05-2011		<b>2. REPORT TYPE</b> Technical Memorandum		<b>3. DATES COVERED (From - To)</b>	
<b>4. TITLE AND SUBTITLE</b> Density Weighted FDF Equations for Simulations of Turbulent Reacting Flows			<b>5a. CONTRACT NUMBER</b>		
			<b>5b. GRANT NUMBER</b>		
			<b>5c. PROGRAM ELEMENT NUMBER</b>		
<b>6. AUTHOR(S)</b> Shih, Tsan-Hsing; Liu, Nan-Suey			<b>5d. PROJECT NUMBER</b>		
			<b>5e. TASK NUMBER</b>		
			<b>5f. WORK UNIT NUMBER</b> WBS 561581.02.08.03.16.02		
<b>7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)</b> National Aeronautics and Space Administration John H. Glenn Research Center at Lewis Field Cleveland, Ohio 44135-3191			<b>8. PERFORMING ORGANIZATION REPORT NUMBER</b> E-17676		
<b>9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)</b> National Aeronautics and Space Administration Washington, DC 20546-0001			<b>10. SPONSORING/MONITOR'S ACRONYM(S)</b> NASA		
			<b>11. SPONSORING/MONITORING REPORT NUMBER</b> NASA/TM-2011-217012		
<b>12. DISTRIBUTION/AVAILABILITY STATEMENT</b> Unclassified-Unlimited Subject Categories: 01 and 64 Available electronically at <a href="http://www.sti.nasa.gov">http://www.sti.nasa.gov</a> This publication is available from the NASA Center for AeroSpace Information, 443-757-5802					
<b>13. SUPPLEMENTARY NOTES</b>					
<b>14. ABSTRACT</b> In this report, we briefly revisit the formulation of density weighted filtered density function (DW-FDF) for large eddy simulation (LES) of turbulent reacting flows, which was proposed by Jaber et al. (Jaber, F.A., Colucci, P.J., James, S., Givi, P. and Pope, S.B., "Filtered mass density function for Large-eddy simulation of turbulent reacting flows," J. Fluid Mech., vol. 401, pp. 85-121, 1999). At first, we proceed the traditional derivation of the DW-FDF equations by using the fine grained probability density function (FG-PDF), then we explore another way of constructing the DW-FDF equations by starting directly from the compressible Navier-Stokes equations. We observe that the terms which are unclosed in the traditional DW-FDF equations are now closed in the newly constructed DW-FDF equations. This significant difference and its practical impact on the computational simulations may deserve further studies.					
<b>15. SUBJECT TERMS</b> Turbulence					
<b>16. SECURITY CLASSIFICATION OF:</b>			<b>17. LIMITATION OF ABSTRACT</b> UU	<b>18. NUMBER OF PAGES</b> 25	<b>19a. NAME OF RESPONSIBLE PERSON</b> STI Help Desk (email:help@sti.nasa.gov)
<b>a. REPORT</b> U	<b>b. ABSTRACT</b> U	<b>c. THIS PAGE</b> U			<b>19b. TELEPHONE NUMBER (include area code)</b> 443-757-5802



