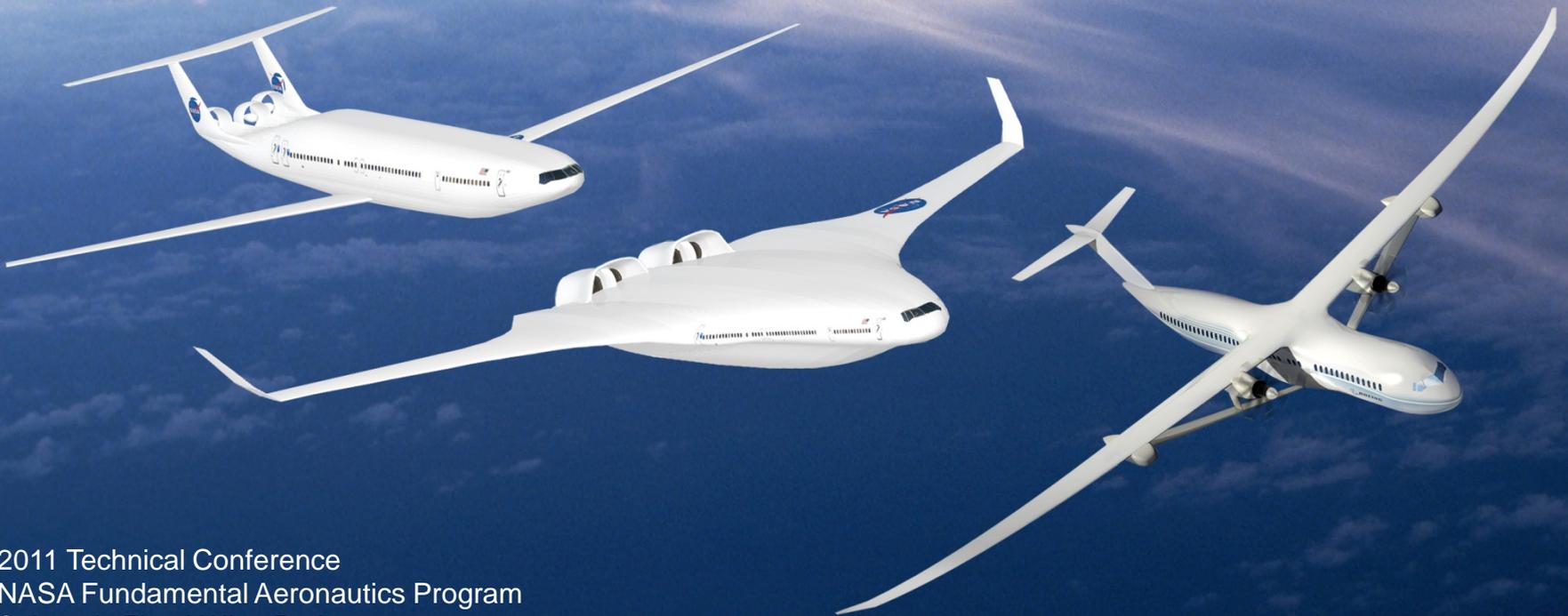




Integrated Control with Structural Feedback to Enable Lightweight Aircraft

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NASA Fundamental Aeronautics Program
Subsonic Fixed Wing Project
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- System Level Metrics
- Benefits of Active Structural Control
- Active Structural Control Research Areas
- Integrated Control for the Prevention of Critical Loads
 - Problem Statement
 - Control System Architecture
 - Simulation Studies
 - Approach
 - Results and Discussion
- Future Research

NASA Subsonic Transport System Level Metrics

... technology for dramatically improving noise, emissions, & performance



CORNERS OF THE TRADE SPACE	N+1 (2015) ^{***} Technology Benefits Relative to a Single Aisle Reference Configuration	N+2 (2020) ^{***} Technology Benefits Relative to a Large Twin Aisle Reference Configuration	N+3 (2025) ^{***} Technology Benefits
Noise (cum below Stage 4)	- 32 dB	- 42 dB	- 71 dB
LTO NOx Emissions (below CAEP 6)	-60%	-75%	better than -75%
Performance Aircraft Fuel Burn	-33%**	-50%**	better than -70%
Performance Field Length	-33%	-50%	exploit metroplex* concepts

^{***} Technology Readiness Level for key technologies = 4-6

^{**} Additional gains may be possible through operational improvements

^{*} Concepts that enable optimal use of runways at multiple airports within the metropolitan areas

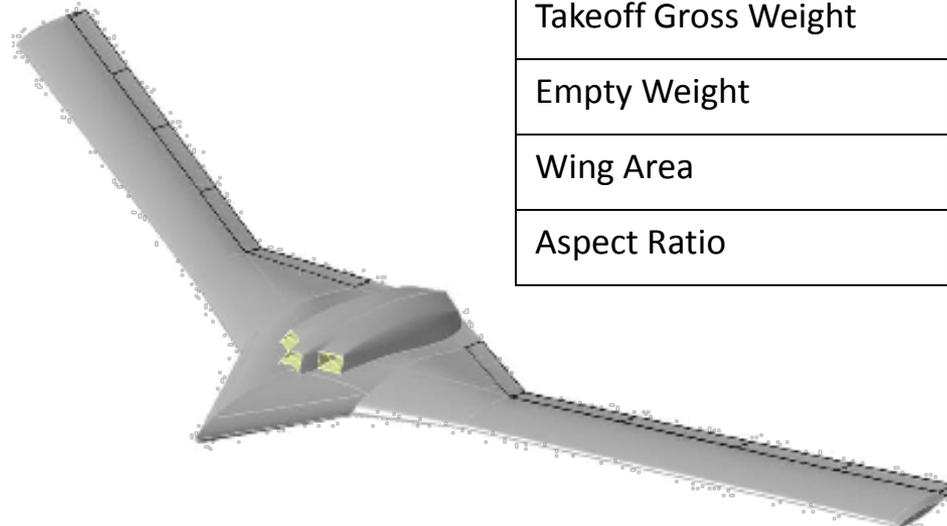
SFW Approach

- Conduct Discipline-based Foundational Research
- Investigate Advanced Multi-Discipline Based Concepts and Technologies
- Reduce Uncertainty in Multi-Disciplinary Design and Analysis Tools and Processes
- Enable Major Changes in Engine Cycle/Airframe Configurations

Benefits of Active Structural Control



- Reduction in aircraft fuel burn due to reduced structural weight
 - Reduced structural margins
 - Gust loads
 - Aeroelastic instabilities
- Gust loads and aeroelastic instabilities inherent in high lift-to-drag, high aspect ratio, low sweep wings (N+3 aircraft)
- One study has shown a 25% reduction in airframe weight through the use of active flutter suppression
 - “System Benefits of Active Flutter Suppression for a SensorCraft-Type Vehicle”, Nicolai, Hunten, Zink, and Flick



Takeoff Gross Weight	96,000 lb
Empty Weight	36,332 lb
Wing Area	2445 ft ²
Aspect Ratio	14

Materials and Actuation

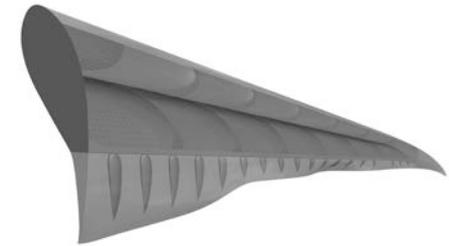
- Conformable mold-line
- Effector development

Sensors

- Fiber optics
- Stagnation point sensors

Actively Controlled, Lightweight Structure

Improved fuel burn, noise, and performance



Control Laws

- Unstable rigid body dynamics
- Unsteady aeroelastic effects (limit cycle oscillation, flutter, dynamic gust load response)
- Reduction of peak loads
- Wing shape optimization

Test, Evaluation, and System Analysis

- Flight validated models and simulations
- Multi-disciplinary design guidelines
- Uncertainty analysis and propagation

Fiber Optic Sensor Development



- Objective: enable a high density of real-time measurements of deflection, rotation, bending moment, torsion, and mode shape
 - Validate method and equations
 - Determine accuracy of measurements
 - Determine optimal fiber placement
- Approach: capture data from ground and flight tests on aircraft and simple test articles to investigate fundamental principles and draw comparisons to other sensor technologies



Ground Test of Global Observer wing

Fiber Optic Sensor Development



- Results: data captured in flight and ground tests
 - Good results for bending deflection of simple test articles and a full scale UAV
- Remaining Work: progression to more complicated structures, validate loads measurements, increased sample rate, increased resolution, and multi-core fiber
- Significance: enable structural weight reduction
 - Structural feedback to control system (shape and loads)
 - Maneuver and gust load alleviation
 - Active control of aeroelastic instabilities
 - Structural health monitoring



Swept Plate Undergoing Test

Aerodynamic Force Sensor Development



- Objective: enable real-time measurement of external forces acting on the aircraft in the presence of flow separation through direct measurement of stagnation point
 - Model generation
 - Parameter identification
 - Stagnation point control
 - Loads, aeroelastic instabilities
- Approach: progression from open-loop observability and validation to closed loop control of stagnation point location

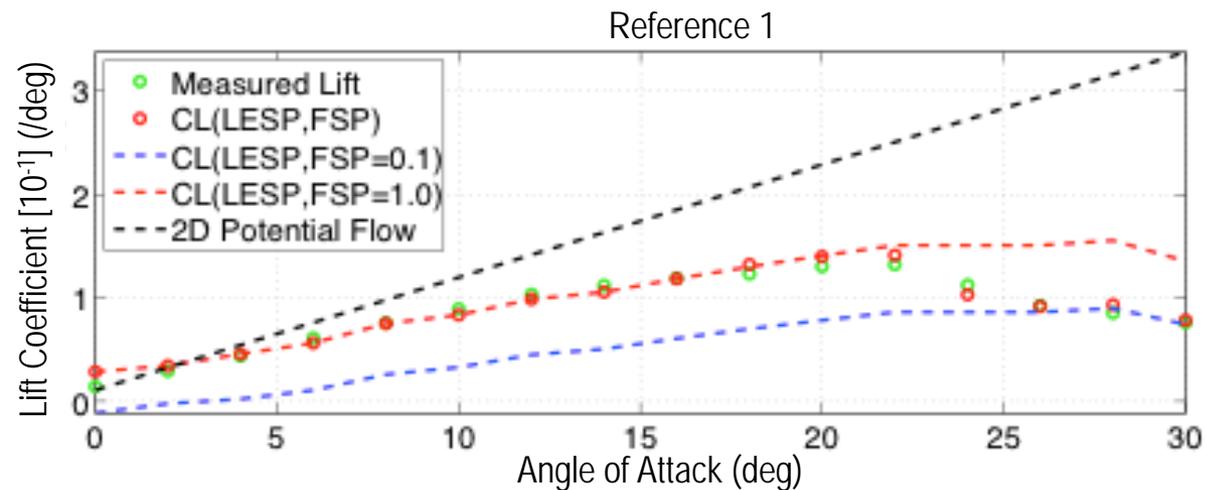


Aerostructures Test Wing

Aerodynamic Force Sensor Development



- Results: validation of stagnation point to sectional forces through wind tunnel tests and open-loop flight test (observability)
- Remaining Work: close the loop around stagnation point sensors to check controllability
- Significance: enables structural weight reduction, optimization of sectional forces to reduce drag, and precise lift control during takeoff and landing
 - Direct measurement of external forces without the associated structural lag
 - Indirect measurement of drag
 - Provides an observable for the state of separated flow around stall conditions
 - Detection and diagnosis of shock/boundary-layer interaction and separation-induced load fluctuations

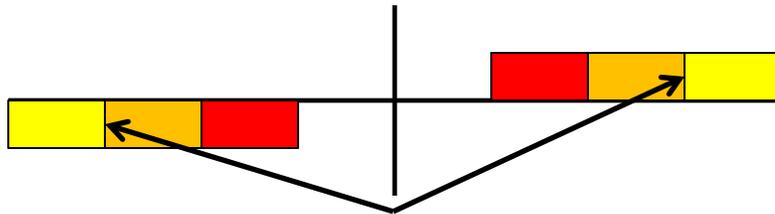




Integrated Control for the Prevention of Critical Loads

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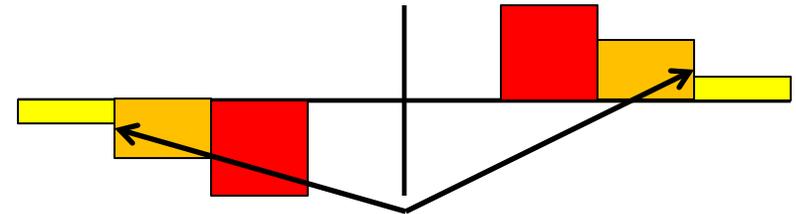
Problem Statement



Roll Moment Achieved

Structural Limit Exceeded

Aileron
Position



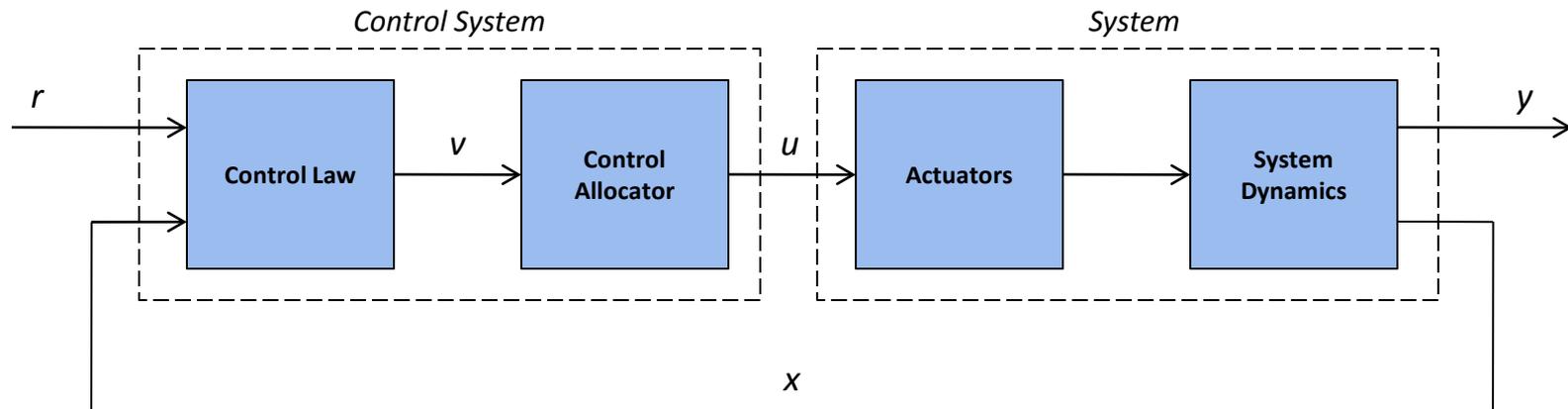
Roll Moment Achieved

Structural Loads *Within Limits*

- Use active structural feedback to determine the optimal control surface positions to:
 - Meet commanded rigid body moments
 - Minimize structural loads
 - Ensure that structural loads do not exceed limits
- Optimal control allocation with structural feedback is a potential solution

Optimal Control Allocation

- Separate the regulation task from the control allocation task
- Mixed optimization to solve multiple objectives simultaneously



Conventional Control Law with Optimal Control Allocation (ref. 2)

Control Allocation Objectives



- Meet commanded rigid body moments (v)
 - Solve for surface positions (u) such that $v = Bu$
- Need both structural feedback and predictive portion similar to the rigid body moments and the control effectiveness (B) matrix
 - Measured load (M) and incremental load due to incremental control surface deflection (T)

$$L = M + Tu$$

- Minimize structural loads
- Ensure that structural loads do not exceed limits
 - Treated like control surface saturation

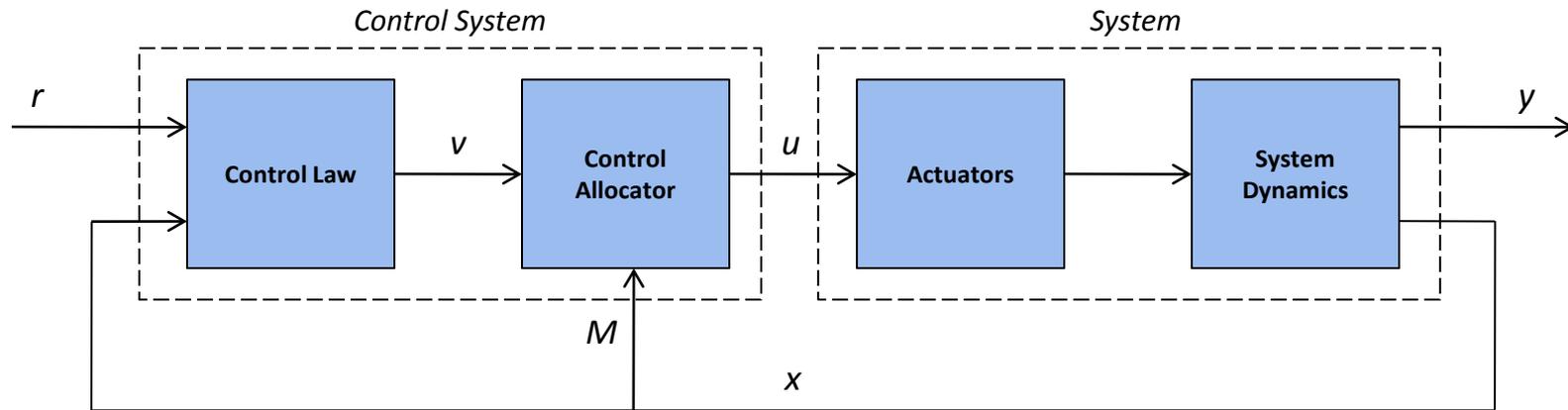
- Cost function:

$$J = \|Bu - v\| + \gamma \|M + Tu\|$$

Subject to:

$$u_{\min} \leq u \leq u_{\max} \quad (M + Tu) \leq L_{\max}$$

Control Allocation Diagram



Structural Feedback Control Law with Optimal Control Allocation

- Feedback of measured load to control allocator
- Inclusion of the T matrix
 - Computed from FEM code
 - Lookup table
 - Parameter estimation

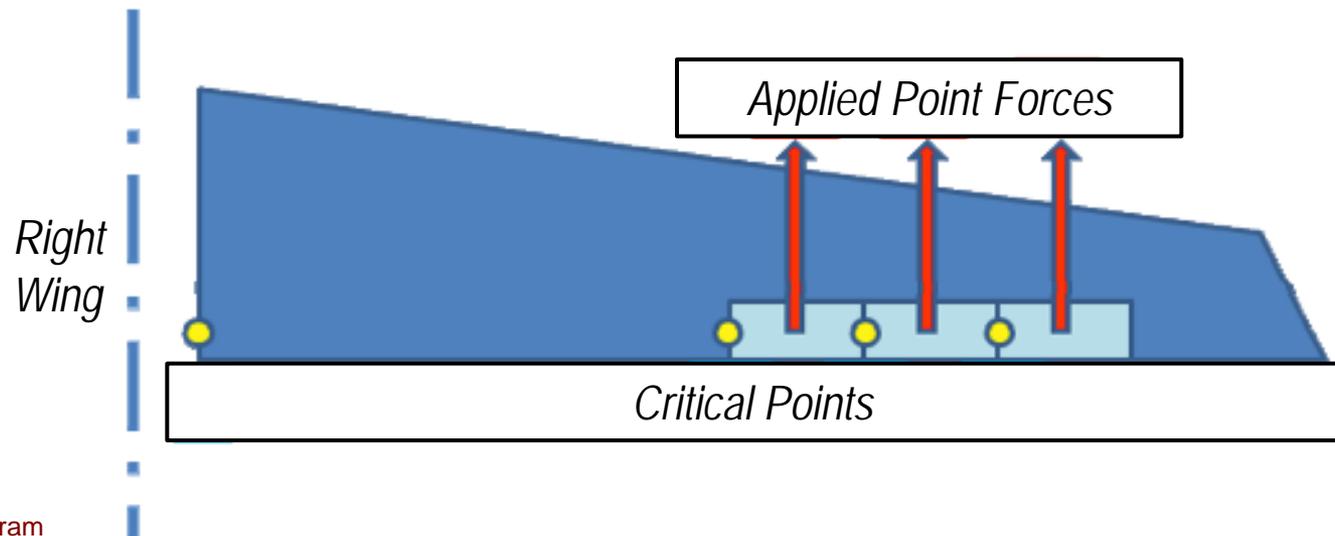
$$T = \frac{\text{Incremental Load}}{\text{Incremental Deflection}}$$

$$B = \frac{\text{Incremental Moment}}{\text{Incremental Deflection}}$$

Simulation Study Approach



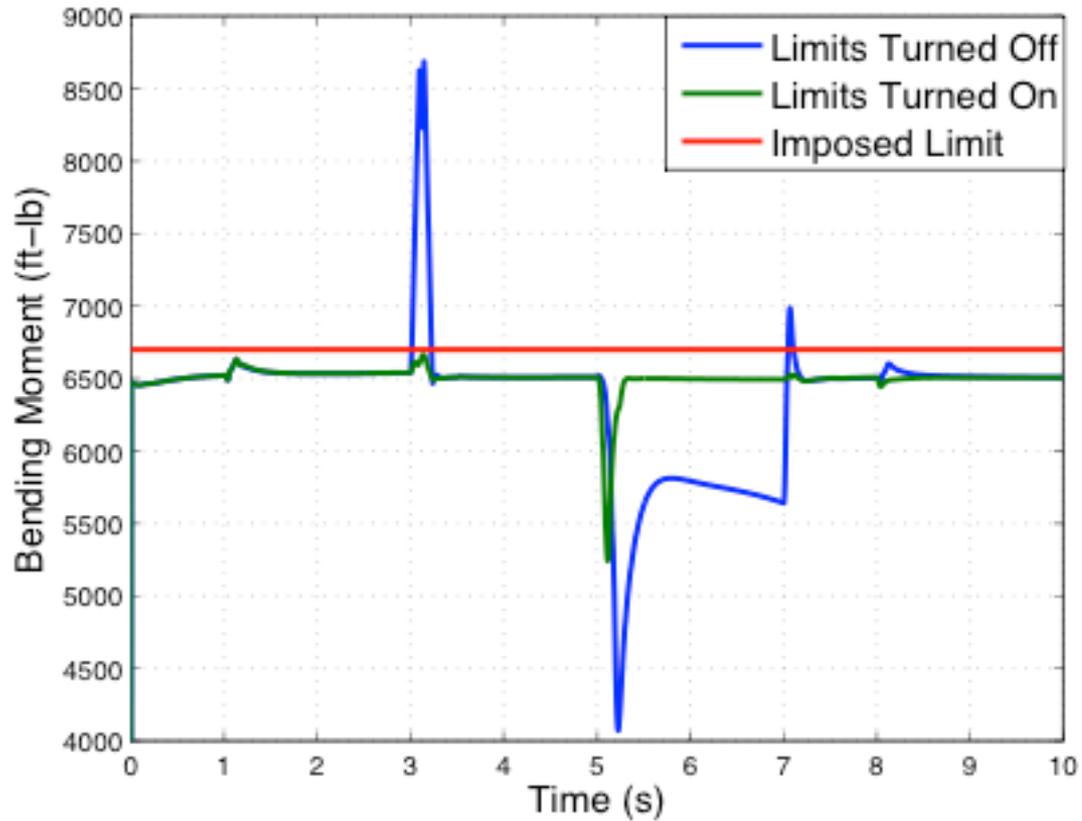
- Modified Generic Transport Model (GTM) simulation
 - 6 ailerons, 4 elevators, 2 rudders
 - FEM of wing, horizontal tail, and vertical tail
 - “Critical points” at inboard edge of control surfaces and roots
 - Distributed lift force over entire wing/tail and point forces due to control surfaces
- Roll maneuver
 - Load control on and off with load limits set low enough to require change in allocation
 - Same rigid body motion with reduction in load at critical point



Simulation Study Results



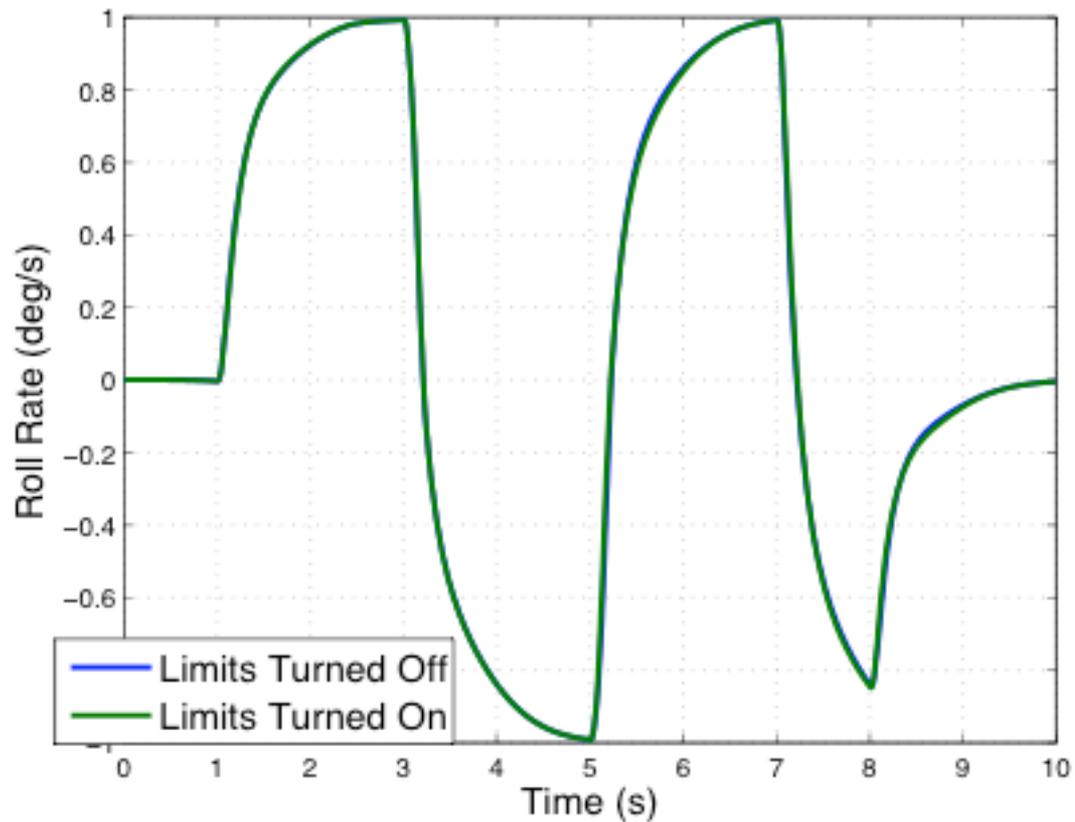
Outboard Aileron Bending Moment



Simulation Study Results



Roll Performance



Simulation Study Discussion



- Roll moment generation moved from outboard aileron surfaces to inboard surfaces
 - L1 norm optimal control allocation used for study
 - L2 norm would more evenly distribute demand
 - All control surfaces that generate roll moment available (split elevator and rudder)
- Roll performance maintained without violating load limits
- Can be used to:
 - Enable optimal control allocation on existing aircraft
 - Control surface commands constrained not to exceed existing load limits
 - Enable lighter weight structure on future aircraft
 - Reduce future load limits while still meeting performance demands
 - Extension to algorithm for gust load alleviation

Next Steps



- Study T matrix assumptions and accuracy necessary for flight
- Extension of algorithm for gust load alleviation
 - Gust load alleviation literature survey
 - Incremental load per incremental gust
 - “ G ” matrix
 - Need measurement of gust
 - Addition of gust loads into optimal allocator objectives
- Improved sensor fidelity
 - Delays inherent in each sensor
- Hardware test of algorithm and feedback

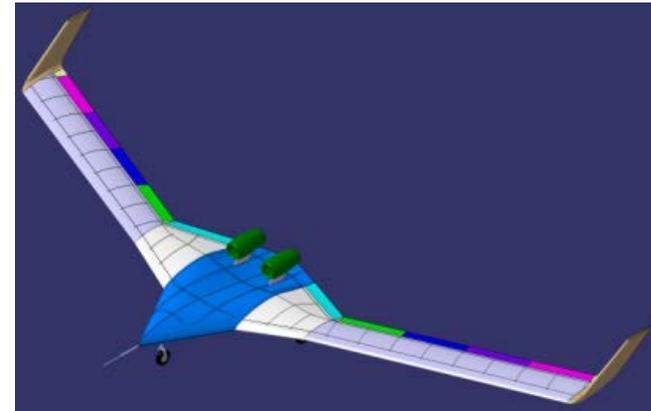
Future Research



- Characterize input and response of structure in flight
 - Stagnation point sensors, fiber optics, strain gages, accelerometers, photogrammetry
- Create and release validated models and simulations
- Active load control, gust load alleviation, and flutter suppression
 - Dedicated surfaces
 - Demands spread across all surfaces
- Passive aeroelastic tailoring
- Develop analysis techniques
- Validate design and optimization tools using flight data



NASA F-18 FAST



Multi-Utility Technology Testbed



Nomenclature



Symbol	Definition
r	Commanded rates
v	Commanded moments
u	Commanded surface positions
y	Aircraft response
x	Observed aircraft states
M	Measured load
L	Predicted future load
T	Incremental load per incremental surface deflection
B	Incremental moment per incremental surface deflection
G	Incremental load per incremental gust
γ	Weighting matrix
u_{\max}	Maximum surface position
u_{\min}	Minimum surface position
L_{limit}	Load limit
J	Cost function



References

1. A. Mangalam et al, "Aerodynamic and Structural Measurement of the Aerostructures Test Wing for Flutter Testing," Presentation at NASA Dryden Flight Research Center, Edwards, CA. October 2010.
2. O. Harkegard, "Backstepping and Control Allocation with Applications to Flight Control," Linkoping Studies in Science and Technology. Dissertations No. 820. 2003.

Integrated Control for the Prevention of Critical Loads Publications

1. S. Frost et al, "A Framework for Optimal Control Allocation with Structural Load Constraints," AIAA Atmospheric Flight Mechanics Conference, Toronto, Canada. August 2010

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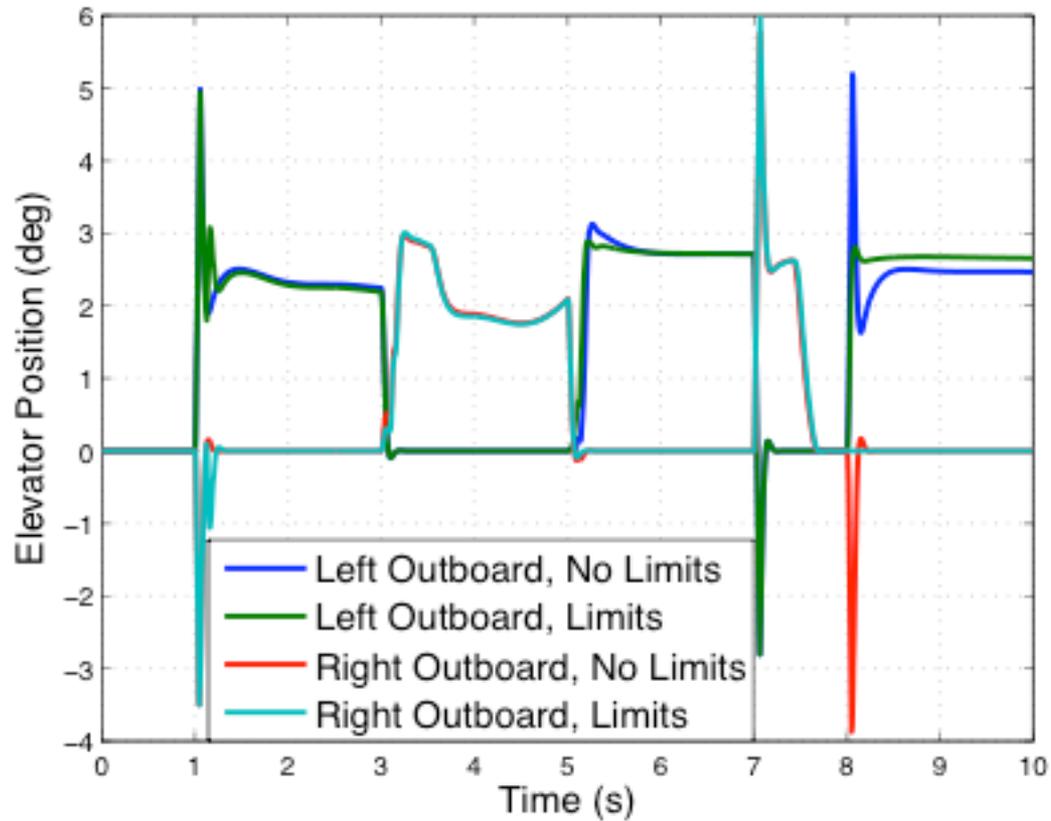
Susan Frost (ARC)

Arun Mangalam (Tao Systems)

Backup Slides



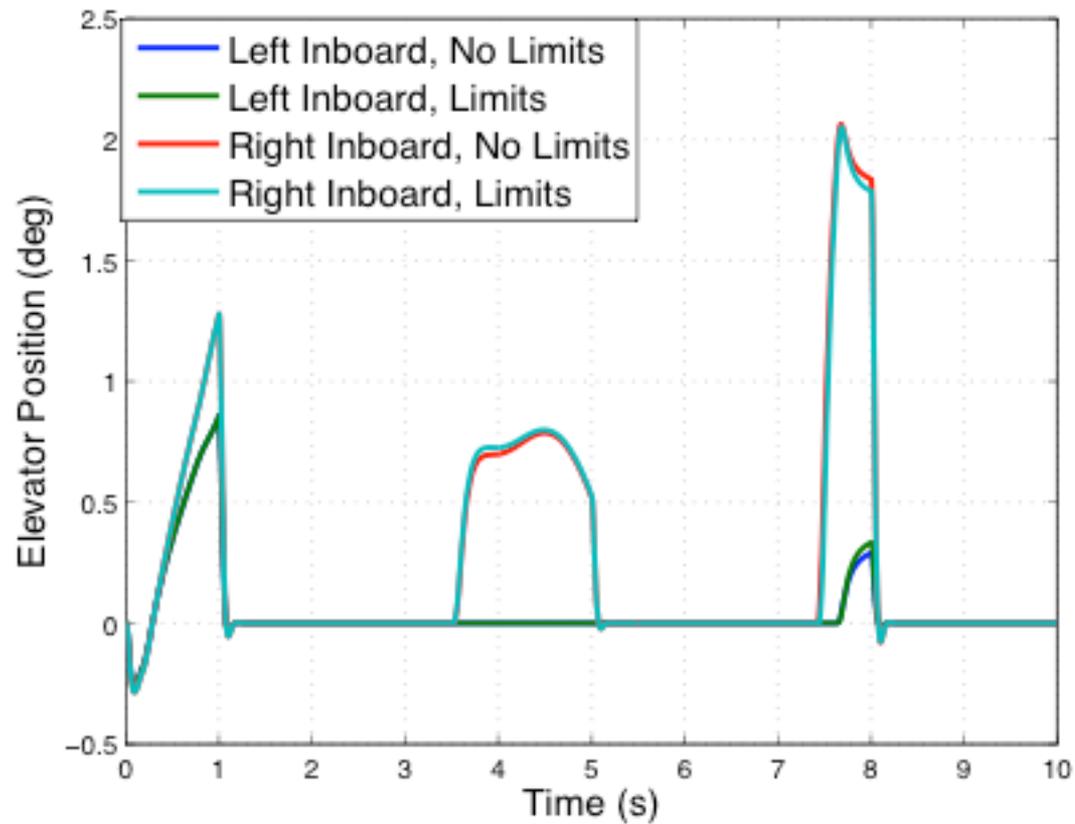
- Elevator outboard



Backup Slides



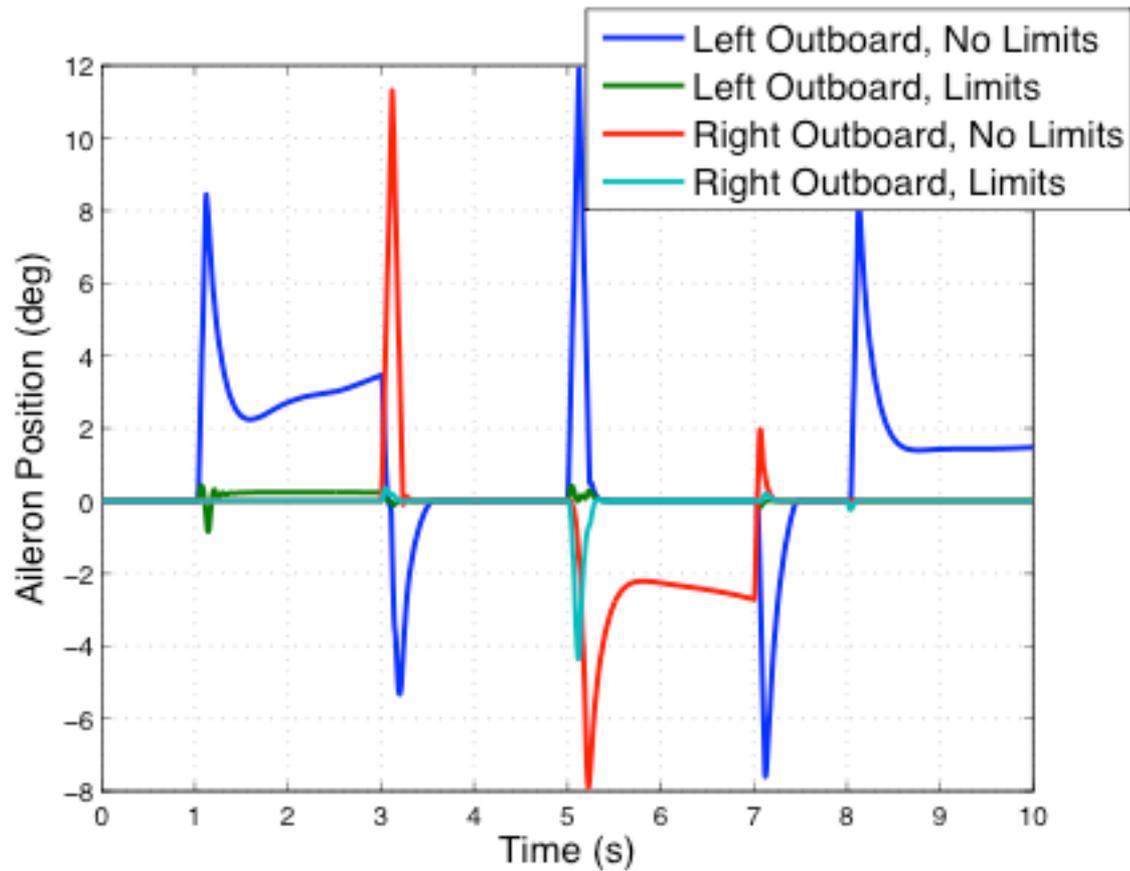
- Elevator inboard



Backup Slides



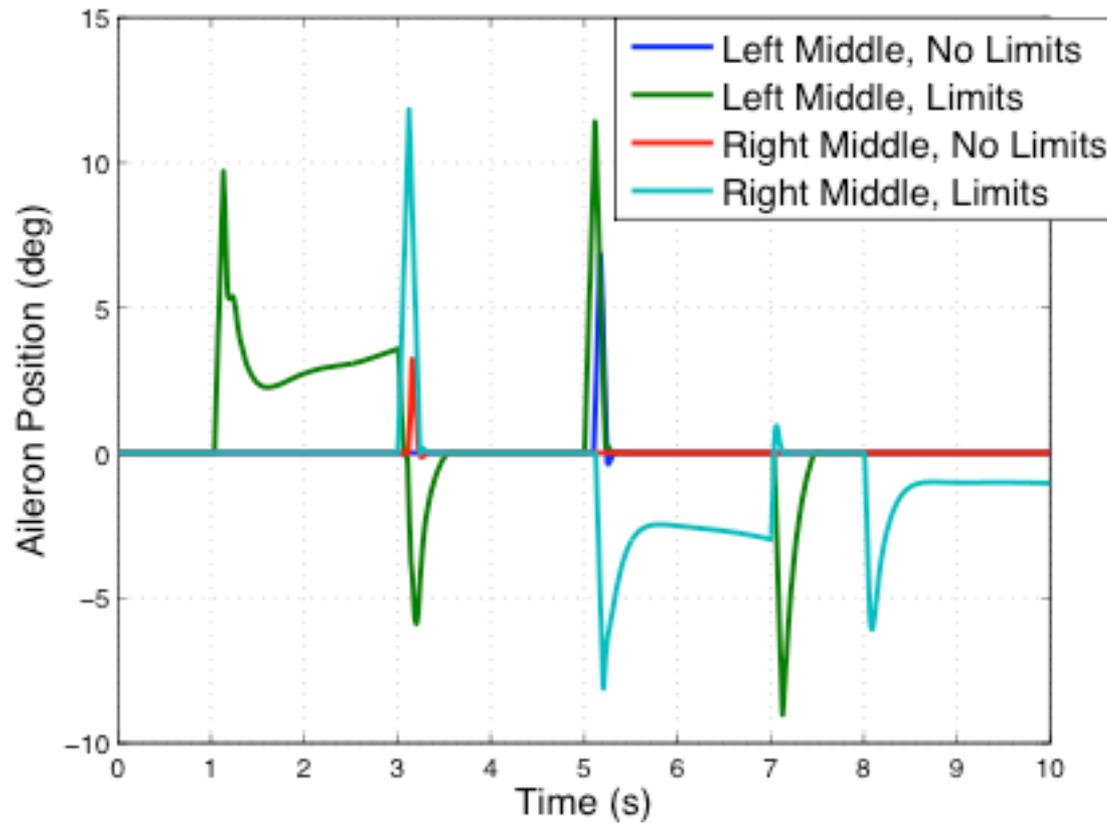
- Aileron outboard



Backup Slides



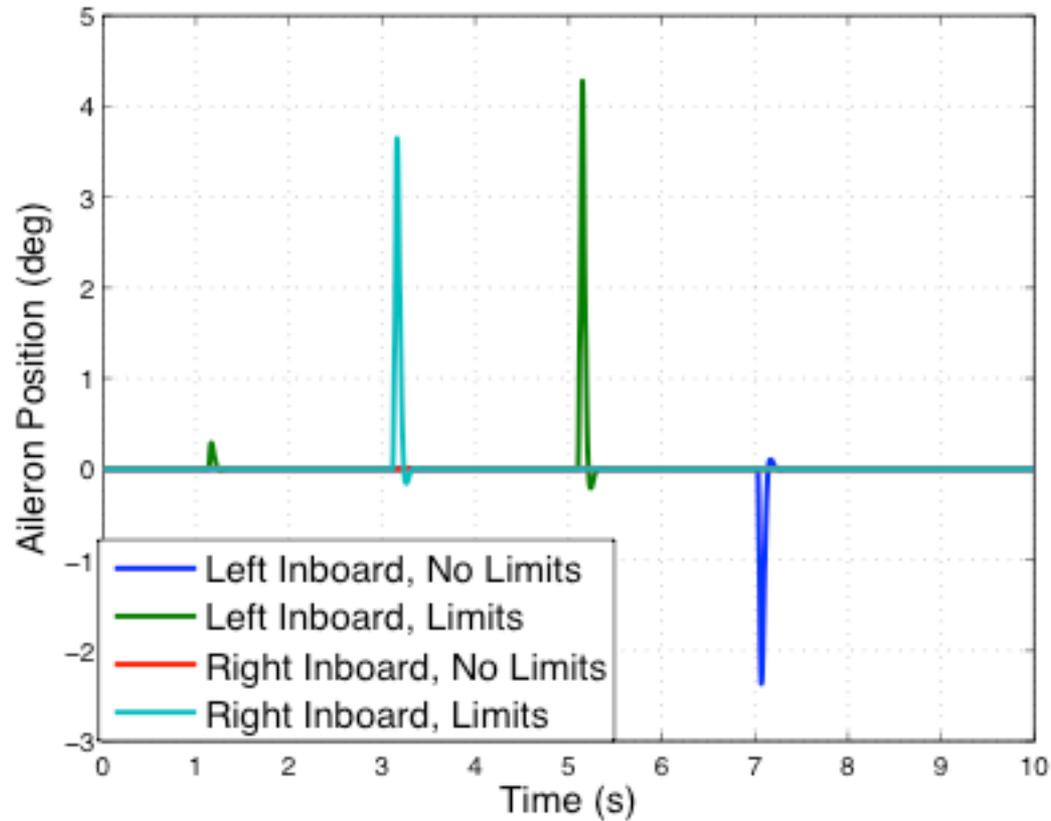
- Aileron middle



Backup Slides



- Aileron inboard



Backup Slides



- Rudder upper and lower

