MULTI-PIXEL HIGH-RESOLUTION THREE-DIMENSIONAL IMAGING RADAR

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ABSTRACT

A three-dimensional imaging radar operating at high frequency e.g., 670 GHz radar using low phase-noise synthesizers and a fast chirper to generate a frequency-modulated continuous-wave (FMCW) waveform, is disclosed that operates with a multiplexed beam to obtain range information simultaneously on multiple pixels of a target. A source transmit beam may be divided by a hybrid coupler into multiple transmit beams multiplexed together and directed to be reflected off a target and return as a single receive beam which is demultiplexed and processed to reveal range information of separate pixels of the target associated with each transmit beam simultaneously. The multiple transmit beams may be developed with appropriate optics to be temporally and spatially differentiated before being directed to the target. Temporal differentiation corresponds to a different intermediate frequencies separating the range information of the multiple pixels. Collinear transmit beams having differentiated polarizations may also be implemented.

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FIG. 1B

- Main Reflector
- Secondary Mirror
- Transceiver
- Polarization Grid
- Quasi-optical Waveguide

Pixel 1
Pixel 2
Target

Range (IF Freq)

L_{delay}

IF Power
FIG. 3
FIG. 6

Relative range: 6 - 4 - 2 - 0 cm

Sound level: 50 dB

Shift: 5.0 cm

Wood only

Beam shift: 1.0 cm, 2.0 cm, 0.5 cm
Divide a source transmit beam into a first transmit beam and a second transmit beam and multiplexing them with a quasioptical device.

Direct both the first transmit beam and the second transmit beam to be reflected off a target such that the second transmit beam is time-delayed from the first transmit beam to correspond to a distinct IF frequency for demultiplexing and processing and received as a single multiplexed receive signal with the quasioptical device.

Mix signals and perform fast Fourier transform (FFT) processing for demultiplexing and processing the single receive signal to determine range information of the target for both a first pixel from the first transmit beam and a second pixel from the second transmit beam with a signal system and a digital signal processor.

FIG. 7
MULTI PIXEL HIGH-RESOLUTION THREE-DIMENSIONAL IMAGING RADAR

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims the benefit under 35 U.S.C. §119(e) of the following U.S. provisional patent application, which is incorporated by reference herein:


This application is related to the following co-pending and co-owned application, which is incorporated by reference herein:


STATEMENT OF GOVERNMENT RIGHTS

The invention described herein was made in the performance of work under a NASA contract, and is subject to the provisions of Public Law 96-517 (35 U.S.C. 202) in which the Contractor has elected to retain title.

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention relates to imaging radar systems. Particularly, this invention relates to high frequency real aperture three-dimensional radar imaging systems.

2. Description of the Related Art

Numerous commercial technologies can detect weapons or contraband concealed in clothing from trace chemical sniffers to X-ray imagers—but in almost all cases these approaches require the sensor and the target to be in close proximity. For situations that call for remote detection, such as when hidden explosives may be detonated or where clandestine surveillance is warranted, concealed weapons detection is at best extremely difficult to accomplish.

Conventional radars are being widely investigated for this purpose, but stringent spatial resolution requirements make these systems impractical because of the large bandwidths and aperture sizes needed. Traditional radar systems are also poorly suited for spectroscopic identification of materials such as explosives. Some progress in through-clothing imaging has been reported using passive thermal detectors in the submillimeter spectrum, but these approaches are lacking in sensitivity and spectral selectivity.

Among the conventional detection systems employing radar techniques for human targets, many operate only by detecting power of a beam reflected off a target. Such radar detection systems infer a characteristic of the object reflecting power from a location compared against reflected power from other locations in a two-dimensional scan. Radar detection systems operating in this manner typically do not derive or utilize range information across the target object (the person). Thus, such radar systems operating based on reflected power alone are not three-dimensional imaging systems. In contrast, radar imaging systems employ derived range information to a target, typically ignoring reflected power. However, effective three-dimensional radar imaging systems can be difficult to produce. Imaging technology in the THz range has primarily focused on acquiring two-dimensional camera-like representa-
hidden contraband can be detected based on the downconverted signal. Mueller also speculates that high-resolution radar techniques would assist in detecting hidden objects, and a frequency-modulated continuous-wave (FMCW) radar technique is proposed to accomplish that. However, no algorithmic description explaining how radar data is to be used for object detection is given, and no methods of FM-chirp non-linearity compensation are described.

In real scenarios a coherent radar image will typically exhibit very poor contrast between a concealed object and the surrounding clothing and skin—even for hidden metallic objects such as guns. The challenge of actively illuminated submillimeter wave detection of concealed objects involves extracting signals from scene clutter rather than from noise. For example, while active THz imaging systems using high power coherent illumination and ultra-low-noise heterodyne detection show great promise, they often face operational drawbacks such as requiring cryogenic detectors or bulky laser sources. A more fundamental difficulty with coherent active imaging is that by relying on a single frequency, target recognition is reliant on an object’s contrast and brightness which, in turn, are highly sensitive to incidence angle of radiation, clutter signal from the foreground or background, and interference and speckle effects.

In view of the foregoing, there is a need in the art for apparatuses and methods for high frequency radar providing three-dimensional imaging with high range resolution. There is also a need for such apparatuses and methods employing long standoff range, speed and penetrability. There is a need for such apparatuses and methods to operate with reduced sensitivity to incidence angle of radiation, clutter signal from the foreground or background, and interference and speckle effects, indicative of other imagers. There is further a need for such apparatuses and methods to operate allow conceal target identification at reasonable cost. There is particularly a need for such apparatuses and methods in security applications to detect concealed weapons and explosives on individuals. In addition, there is a need for such apparatuses and methods to operate at improved imaging rates, ideally facilitating full motion radar imaging. Particularly, there is a need for systems and methods that can yield multi-pixel radar imaging in order to achieve higher imaging rates. These and other needs are met by the present invention as detailed hereafter.

**SUMMARY OF THE INVENTION**

A three-dimensional imaging radar operating at high frequency e.g., 670 GHz radar using low phase-noise synthesizers and a first chirper to generate a frequency-modulated continuous-wave (FMCW) waveform, is disclosed that operates with a multiplexed beam to obtain range information simultaneously on multiple pixels of a target. A source transmit beam may be divided by a hybrid coupler into multiple transmit beams multiplexed together and directed to be reflected off a target and return as a single receive beam which is demultiplexed and processed to reveal range information of separate pixels of the target associated with each transmit beam simultaneously. The multiple transmit beams may be developed with appropriate optics to be temporally and spatially differentiated before being directed to the target. Temporal differentiation corresponds to a different intermediate frequencies separating the range information of the multiple pixels. Collinear transmit beams having differentiated polarizations may also be implemented.

A typical embodiment of the invention comprises a radar imaging system, including a quasi-optical device for dividing a source transmit beam into a first transmit beam and a second transmit beam and multiplexing them, where both the first transmit beam and the second transmit beam are directed to be reflected off a target such that the second transmit beam is time-delayed from the first transmit beam to correspond to a distinct IF frequency for demultiplexing and processing and received as a single multiplexed receive signal with the quasi-optical device, and a system for signal mixing and a digital signal processor for performing fast Fourier transform (FFT) processing for demultiplexing and processing the single multiplexed receive signal to determine range information of the target for both a first pixel from the first transmit beam and a second pixel from the second transmit beam.

In some embodiments, the system for mixing may comprise a first wave synthesizer for generating the source transmit beam, the source transmit beam comprising a frequency modulated continuous wave (FMCW) chirp signal from a source signal, a second wave synthesizer for generating a FMCW local oscillator chirp signal from a source local oscillator signal, a first mixer for combining the reflected FMCW chirp signal and the FMCW local oscillator chirp signal to generate a first intermediate frequency (IF) signal for each of the first transmit beam and the second transmit beam, a second mixer for combining the source signal and the local oscillator signal to generate a second IF signal, and a third mixer for combining the first IF signal and the second IF signal to generate a final IF signal for each of the first transmit beam and the second transmit beam. The digital signal processor may perform fast Fourier transform (FFT) processing of the final IF signal for each of the first transmit beam and the second transmit beam to determine range information for the target of both a first pixel from the first transmit beam and a second pixel from the second transmit beam. A waveform generator generating a common chirp signal in 1 millisecond or less may be employed, wherein the first wave synthesizer generates the frequency modulated continuous wave (FMCW) chirp signal from the source signal mixed with the common chirp signal and the second wave synthesizer generates the FMCW local oscillator chirp signal from the source local oscillator signal mixed with the common chirp signal.

In some embodiments, the quasi-optical device spatially offsets the second transmit beam along a substantially parallel path from the first transmit beam to a distinct point on the target. The quasi-optical device may also be designed to direct the first transmit beam and the second transmit beam along substantially collinear paths and polarize the second transmit beam to that of the first transmit beam to correspond to a distinct polarization for demultiplexing and processing.

In further embodiments of the invention, the quasi-optical device may comprise a coupler for dividing the source transmit beam into the first transmit beam and the second transmit beam, a polarization twist waveguide for rotating polarization of the second transmit beam relative to that of the first transmit beam, and quasi-optical components for imparting a path length differential to induce a time delay between the second transmit beam and the first transmit beam and for directing the first transmit beam and the second transmit beam to the target along a substantially parallel path with a spatial offset.

In some embodiments, a three dimensional map of the target may be derived from the range information determined for each of multiple pixels scanned over the target, where the range information for the multiple pixels are determined in simultaneously processed pairs associated with the first transmit beam and the second transmit beam. A peak-finding algorithm may be applied to the determined range information to differentiate material layers of the target. In addition, a scanning stage may employ in conjunction with the two transmit beams. For example, the quasi-optical device may comprise a
reflector coupled to a two-axis rotation stage and the range information is determined by positioning the two-axis rotation stage for each of the pairs of the multiple pixels scanned over the target with the reflector directing the FMCW chirp signal from the reflector to be reflected off the target and received from the target.

In a similar manner, a typical method of radar imaging, comprises dividing a source transmit beam into a first transmit beam and a second transmit beam and multiplexing them with a quasioptical device, directing both the first transmit beam and the second transmit beam to be reflected off a target such that the second transmit beam is time-delayed from the first transmit beam to correspond to a distinct IF frequency for demultiplexing and processing and received as a single multiplexed receive signal with the quasioptical device, and signal mixing and performing fast Fourier transform (FFT) processing for demultiplexing and processing the single multiplexed receive signal to determine range information of the target for both a first pixel from the first transmit beam and a second pixel from the second transmit beam with a signal system and a digital signal processor. Method embodiments of the invention may be further modified consistent with the apparatuses and systems described herein.

Embodiments of the invention may also encompass an apparatus for multiplexing in a radar imaging system, comprising a coupler for dividing the source transmit beam into a first transmit beam and a second transmit beam and multiplexing them, a polarization twist waveguide for rotating polarization of the second transmit beam relative to that of the first transmit beam, and quasioptical components for imparting a path length differential to induce a time delay between the second transmit beam and the first transmit beam and for directing the first transmit beam and the second transmit beam to the target along a substantially parallel path with a spatial offset. Both the first transmit beam and the second transmit beam are directed to be reflected off a target and received as a single multiplexed receive signal by the quasioptical device and the single multiplexed receive signal is demultiplexed and processed to determine range information of the target for both a first pixel from the first transmit beam and a second pixel from the second transmit beam. Typically, the source transmit beam comprises a frequency modulated continuous wave (FMCW) chirp signal. The apparatus for multiplexing in a radar imaging system may be further modified consistent with the other apparatuses and methods described herein.

BRIEF DESCRIPTION OF THE DRAWINGS

Referring now to the drawings in which like reference numbers represent corresponding parts throughout:

FIG. 1A is a block diagram of an exemplary apparatus for multiplexing a transmit beam in a radar imaging system embodiment of the invention;

FIG. 1B is a diagram of another exemplary apparatus for multiplexing a transmit beam in a radar imaging system embodiment of the invention;

FIG. 1C is a block diagram of an exemplary three-dimensional imaging radar system embodiment of the invention which may be employed with multiplexing transmit beam;

FIG. 2 is a block diagram of an exemplary chirp source for an embodiment of the invention;

FIG. 3 is a block diagram of an exemplary base signal source for a two-pixel imaging embodiment of the invention;

FIG. 4 illustrates a scanning process that may be applied by the example system to derive three-dimensional images of a target with multiplexed transmit beams to yield multiple simultaneous pixels;

FIGS. 5A and 5B illustrate beam diagrams of a beamsplitter and lens quasioptical device and a two-axis rotation stage quasioptical device for an exemplary three-dimensional imaging radar system;

FIG. 6 illustrates results of an imaging scan of a target configuration relevant to a concealed weapon scenario where reflection off the shirt and that off the masked wood surface can be distinguished from each other for separations of 1 cm or more; and

FIG. 7 is a flowchart of an exemplary method of radar imaging.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

1. Overview

Previously an imaging radar was described that operates at submillimeter wavelengths for applications ranging from concealed weapons detection to planetary trace-chemical identification in U.S. patent application Ser. No. 12/135,040, filed Jun. 6, 2008, and entitled “HIGH-RESOLUTION THREE-DIMENSIONAL IMAGING RADAR”, by Cooper et al., which is incorporated by reference herein. Unlike conventional radars, which typically operate below 100 GHz (i.e., wavelengths greater than approximately 3 mm), such a system operating well above this, e.g., 670 GHz, is capable of very high imaging resolution in three dimensions because since its high modulation bandwidth gives higher range resolution and its shorter wavelength gives higher lateral image resolution for any fixed antenna aperture size. Using a novel signal generation architecture, the submillimeter radar is capable of quickly, quietly, and linearly frequency-sweep over a bandwidth of 18 GHz, thus permitting an ultra-high range resolution of less than 1 cm. With an aperture size of 50 cm, the radar is also able to resolve targets within 2 cm at stand-off distances of 25 m. In addition, the submillimeter radar is novel because it has the potential to acquire spectroscopic information from targets for distinguishing their materials characteristics or chemical composition. Finally, owing to its all solid-state implementation, this technology is scalable to a fast, compact multipixel imaging system capable of three-dimensional imaging.

However, the previously disclosed three-dimensional radar imaging system is described using only a scanning stage to repoint the radar in order to obtain range information of the different pixels across the target. The imaging speed of such a system may be improved adapting it to simultaneous multipixel imaging. However, there is no demonstrated previously technique for forming large multi-pixel heterodyne imagers at any wavelength above 100 GHz due to the complexity of having to deal with three different signals for each detector, the local oscillator (LO), radio frequency (RF), and intermediate frequency (IF). In order to increase the number of pixels that are imaged simultaneously using the existing scanning approach, the transmit (Tx) and receive (Rx) modules would need to be increased respectively with the attendant technological difficulty of dealing with the three different signals.

To avoid these difficulties, embodiments of the present invention are directed to a technique of dividing a single transmit beam into two beams multiplexed into a single multiplexed receive signal. This approach allows the transmit and receive chains to remain unaltered and thus greatly simplifies the front- and back-end electronics. A functioning system...
requires only new quasioptical components to double the number of pixels as described hereafter. It should be noted that although embodiments of the invention are taught using two simultaneous transmit beams to range two image pixels simultaneously, those skilled in the art will appreciate that the principle may be expanded to any reasonable number of simultaneous transmit beams with each beam having a different time delay so that they may be safely multiplexed into a single receive signal.

Thus, embodiments of the invention are directed to a multi-pixel three-dimensional imaging radar operating at high frequency, e.g., 670 GHz, employing multiplexed radar signals in a multi-pixel heterodyne system using compact quasioptical components. At such high frequencies, centimeter-scale spatial resolution in three dimensions is possible without excessively large fractional bandwidths or aperture sizes. The active target illumination inherent in radar ensures high signal power and provides for spectroscopic flexibility. A submillimeter imaging radar may use low phase-noise synthesizers and a fast microwave chirp-generator to produce a frequency-modulated continuous-wave (FMCW) waveform. Three-dimensional images are generated through range information derived for each pixel scanned over a target and employing a peak finding algorithm in processing for each pixel to differentiate material layers of the target. In addition, improved focusing may be achieved through a compensation signal sampled from a point source calibration target and applied to received signals from targets prior to FFT-based range compression to extract and display high-resolution target images. Such an imaging radar has particular application in detecting concealed weapons or contraband.

FIG. 1A is a block diagram of an exemplary quasioptical device 100 for multiplexing a transmit beam in a radar imaging system 150 embodiment of the invention. The quasioptical device 100 comprises a coupler 158 for dividing the source transmit beam 156 into the first transmit beam 152A and the second transmit beam 152B. The second transmit beam 152B passes through a polarization twist waveguide 160 for rotating polarization of the second transmit beam 152B relative to that of the first transmit beam 152A. Additional quasioptical components are employed on the second transmit beam 152B to impact a path length differential in order to induce a time delay between the second transmit beam 152B and the first transmit beam 152A and for directing the first transmit beam and the second transmit beam to the target along a substantially parallel path with a spatial offset 162 between the two beams 152A, 152B. In this example, the path differential is developed with a pair of parabolic reflectors 164A, 164B (shown schematically) arranged to reflect and focus the second transmit beam 152B from the polarization twist waveguide 160 to bring it back to a polarizing wire grid 114. The first transmit beam 152A passes through the polarizing wire grid 114 from the coupler 158 and the second transmit beams 152B is reflected off the polarizing wire grid 114 to both be directed to the target 116 with a spatial offset 162 between the to co-aligned beams 152A, 152B. The beams 152A, 152B are reflected off the target 116 and return along their respective paths and through the coupler 158 to form a multiplexed received beam 154 in a single channel.

2. Multiplexed Transmit Beams for Multiple Simultaneous Pixels

In an exemplary radar imaging system, the transmit and receive signals are divided/combined by a hybrid coupler into two horns. The signal from one of the horns is focused by a reflector toward the target in order to deliver a first pixel (range information), while the second one is spatially delayed by a quasioptical waveguide and then focused with the same reflector in order to deliver a second pixel. The two pixels will have both a cross range and a temporal displacement. In the receive mode, this time delay will be translated into different IF frequencies, separating the information from the two pixels. The beam profiles of the two pixels can be tuned with the quasioptical system. For example, the two pixels can be designed to have a crossover of approximately −3 dB or instead be separated a certain number of beamwidths. It is also possible to direct both transmit at the same point on the target but with orthogonal polarizations in order to study polarization properties. Embodiments of the invention may also employ a combination of polarization and time delays to obtain a single multiplexed receive signal that can be processed to obtain the separate pixels information. The design of such quasioptical multiplexing can be performed in a single plane, and therefore may be used with a linear array.

Although embodiments of the invention may be applied to other radar imagers as will be understood by those skilled in the art, the active target illumination inherent in the example radar imager solves the problem of low signal power and narrow-band detection by using submillimeter heterodyne mixer receivers. A submillimeter imaging radar may use low phase-noise synthesizers and a fast chirp-generator to generate a frequency-modulated continuous-wave (FMCW) waveform. Three-dimensional images are generated through range information derived for each pixel scanned over a target. A peak finding algorithm may be used in processing for each pixel to differentiate material layers of the target. Improved focusing is achieved through a compensation signal sampled from a point source calibration target and applied to received signals from active targets prior to FFT-based range compression to extract and display high-resolution target images. Such an imaging radar has particular application in detecting concealed weapons or contraband.
The issue of ohmic loss in the system may be addressed by designing more compact waveguide components, possibly using silicon micro-machining. The isolation of the coupler, however, may be difficult to improve using any kind of waveguide design. Therefore, the SNR degradation due to phase noise may need to be addressed using a better IF circuit design, or just accepted as a moderate performance penalty. However, it is important to note that the same multiplexing technique described here could be implemented using all quasioptical components (e.g. beam splitter and polarization rotator), which would be practically immune to both the loss and leakage effects encountered in the all-waveguide multiplexing approach. The waveguide approach has potential applicability to an eventual integrated array technology.

FIG. 1B is a diagram of another exemplary apparatus for multiplexing a transmit beam in a radar imaging system embodiment of the invention. The optical path of the first transmit beam, may follow from one of the coupler's horns through the wire grid that is oriented to be transparent to this first transmit beam, then to a secondary flat mirror, and finally to the main 40 cm ellipsoidal antenna which focuses the beam to a spot size of less than 1 cm at a target 4 m away. A second beam, on the other hand, is shown as a dashed line in FIG. 1B. After emerging from the second horn of the coupler/twist pair, it is first captured and delayed by a quasi-optical waveguide of length L_{delay}=90 cm. The second beam encounters the wire grid, but because of its orthogonal polarization with respect to the first beam, it is reflected by the grid. This is then followed by reflection from the common flat secondary mirror and ellipsoidal main mirror for focusing at 4 m range.

The exemplary beam multiplexing system is designed so that the first horn is offset in the focal plane by about 0.9 cm from the main antenna focal point, while the effective focal point of the quasi-optical waveguide matches that of the main antenna. The result is that the two beams are projected toward the target at a slightly offset angle of 0.61° in elevation, corresponding to a 4.25 cm displacement at the target range of 4 m. Thus, while the two beams share a common source and detector, they are separated both in the two-dimensional cross-range space of the target focal plane and in the third range dimension by virtue of the time delay of the second beam. This means that even though both beams may be reflected by separate regions of a target at the roughly same range from the main reflector, the detected signals of the two beams will be separated by a distance L_{delay} in the final IF power spectrum. In other words, the power spectrum of the detected IF signal will generally exhibit two regions of high intensity, corresponding to the two beams, separated by a range corresponding to the time delay introduced in the second beam, as indicated inset of FIG. 1B. The peaks in the power spectrum can then be assigned with high reliability to the appropriate beam for image reconstruction. Thus three-dimensional target information can be acquired from two beams simultaneously, all without any additional THz sources, receivers, or analog-to-digital sampling channels.

FIG. 1C is a block diagram of an exemplary three-dimensional imaging radar system 150 that may employ an embodiment of the invention. This simplified diagram eliminates necessary frequency multipliers and amplifiers to better illustrate general function of the radar. Location and type of filters, frequency multipliers and amplifiers are variable and depend upon a particular system design as will be understood by those skilled in the art. Detailed examples of three-dimensional imaging radar that are operable with embodiments of the invention are described in U.S. patent application Ser. No. 12/135,040 previously mentioned. In general, an applicable imaging system 150 employs a transmit wave synthesizer 102 for generating a frequency modulated continuous wave (FMCW) chirp signal as the source transmit beam 156 based on a source signal. The final FMCW chirp signal is smoothly chirped in frequency over a wide bandwidth and output at high frequency, e.g. 560 GHz. A receive wave synthesizer 104 generates a FMCW local oscillator chirp signal from a source local oscillator (LO) signal. Note that the transmit wave synthesizer 102 and the receive wave synthesizer 104 may be combined in a single device. The source signal and the source LO signal may be generated through different techniques, e.g. from separate waveform generators 106, 108 or a common waveform generator unit 112, as will be described hereafter.

The output FMCW chirp signal source transmit beam 156 is divided into two transmit beams 152A, 152B directed to the target 116 by the appropriate quasioptical device 100. The FMCW chirp signal transmit beams 152A, 152B are reflected off the target 116 and return to a first mixer 118 as a multiplexed receive signal 154 in a single channel to be combined with a FMCW local oscillator chirp signal from the receive wave synthesizer 104 and yield a first intermediate frequency (IF) signal for each transmit beam 152A, 152B. The induced time delay from the path differential of the second transmit beam 152B imparts distinct IF frequency which differentiates the two power peaks in the single receive channel for each pixel as illustrated in the inset graph of FIG. 1A. Both the source signal 106 and the source LO signal 108 are tapped (at signal taps 110A, 110B, respectively) and mixed in a second mixer 120 to yield a second IF signal. A third mixer 122 is then used to combine the first IF signal and the second IF signal to generate a final IF signal for each of the first transmit beam 152A and the second transmit beam 152B.

Processing may be performed by a digital signal processor system 124 which digitizes 126 the final IF signal and performs fast Fourier transform (FFT) processing 128 on the digitized final IF signal to determine range information 132 for the target 116 for each of the simultaneous transmit beams 152A, 152B. The present invention may also employ a compensation signal 130 derived from a pointed source test target response which is applied to the final IF signal prior to FFT processing 128 for each beam 152A, 152B to focus the determined range in formation 132 for the target 116. Details of the operations and processes of an applicable imaging radar are described in related U.S. patent application Ser. No. 12/135,040 in various example embodiments of the invention.

For scanned three-dimensional imaging applications, it may be very helpful to increase the PRF by building a custom chirped source that is fast, linear, and wideband. These requirements are conflicting because of the tradeoff between speed and phase noise, but such systems have already been developed for some specialized FMCW radars. See e.g., Gogineni et al., “An Ultra-wideband Radar for Measurements of Snow Thickness Over Sea Ice,” Proceedings of the IGARSS '03, IEEE Geoscience and Remote Sensing Symposium, vol. 4, pp. 2802-2804, 21-25 Jul., 2003, which is incorporated by reference herein. Indeed, phase noise and chirp nonlinearities in submillimeter radars may be likely to pose severe constraints as target distances increase and clutter and multipath signals appear. See e.g., Wehner, “High-Resolution Radar,” Artech House, Boston 1995, which is incorporated by reference herein. Nonetheless, based on the results presented herein, the component technology and signal processing algorithms are advanced enough to make submillimeter radar viable.

FIG. 2 is a block diagram of an exemplary chirp source 200 for an embodiment of the invention. This chirp source 200 may be readily implemented in to the example radar system.
of FIG. 1C as will be understood by those skilled in the art. The chirp speed may limited in part by the signal to noise ratio of the system. If a high multiplication ratio used (x>36), the primary factor limiting the dynamic range is the receiver noise figure or lack of transmitter power, but phase noise in the transmitted and LO signals. In order to reduce this noise, a lower multiplication factor of x18 may be chosen. In order to generate the base chirp signals, a pair of very low noise 35 GHz synthesizers, e.g., Mitelq synthesizers, may be employed. These synthesizers may then be used to upconvert a new chirp source. A lower multiplication factor will raise the required bandwidth of the chirper. For x18 multiplication and 29 GHz chirp bandwidth, a base chirp bandwidth of ~1.6 GHz is required. Additionally, in order to keep the wide band phase noise contribution from the chirp source as low as possible, the lowest possible frequency range that still yielded a 1.6 GHz chirp band may be chosen. A Mini-Circuits ROS- 3200-419+ may be selected as the VCO for the chirper due to its low cost, wide full-octave bandwidth and low operating frequency. Its phase noise at frequency offsets above 1 MHz is 15 to 20 dB lower than higher frequency wideband VCOs.

While reduced phase noise is important to improving the signal to noise ratio, this reduced noise must be maintained while chirping at a fast rate. In order to ultimately achieve near real-time imaging speeds using a reasonably small number of parallel transceiver channels, a single chirped pulse must be acquired in 1 millisecond or less. This represents a factor of 12 decrease in chirp duration over a high multiplication factor chirper, with a chirp rate of roughly double the increase in duration due to the halving of the base source multiplication factor. For example, the chirp source in such a system may run at approximately 0.064 MHz/µsec chirp rate, the chirper 200 of FIG. 2 may operate at approximately 1.6 MHz/µsec. These requirements can be achieved using the example hybrid PLL/DDS design shown in FIG. 2. The 1.6-3.2 GHz chirper may be designed using vendor-assembled evaluation boards for the VCO, DDS, microwave divider and phase detector/PLL. The DDS board reference may be driven from the same ultra low-noise 240 MHz reference oscillator feeding the Mitelq synthesizers in order to obtain the lowest possible phase noise output from the DDS, which was used as the reference input for the PLL section. The phase detector/PLL device chosen, an Analog Devices ADF4002 has a very low normalized phase noise floor (~222 dBc/Hz). Since the example VCO requires a tuning voltage of 0-20 V while the charge pump output from the ADF4002's phase detector only supplies 5 V, an active loop filter can be designed using SimPL. In addition to providing the DC gain required to drive the VCO's tuning input across its entire range, the loop filter may be optimized for low phase noise while maintaining sufficient loop bandwidth to maintain phase lock during chirping. As previously mentioned, it is critical that a chirp source maintain good phase performance while actually chirping.

FIG. 3 is a block diagram of an exemplary base signal source 300 for a two-pixel imaging embodiment of the invention. Additional transceiving elements can decrease the image acquisition time without decreasing individual pixel acquisition time. Although adding a second pixel to the system doubles the amount of submillimeter components required, some savings in microwave hardware can be realized by using a common low noise source. In FIG. 3 the low noise transmit and LO synthesizer signals are divided and sent to both pixels, while each pixel maintains its own chirp source 200. By applying an asynchronous chirp signal generated by independent chirpers to each pixel, cross coupling between the pixels may be completely eliminated. This has the added benefit of eliminating an undesired modulation problem within the base signal generating subsystem: the power dividers fed by each synthesizer have limited isolation, allowing mixing products from one upconverter to leak out of its LO input and back into the LO input of the other pixel’s upconverter. When the chirps for each pixel are temporally correlated, this leakage may cause subphase and amplitude shifts in the base transmit signals at the output of the upconverters, leading to loss of range resolution caused by “smearing” of the demodulated spectrum. By decorrelating the two chirps signals, these products fall outside the final IF range of the receivers. Although additional isolators at the outputs of the power dividers may also remedy this problem, the use of independent asynchronous chirpers for each pixel affords the additional benefit of eliminating any cross coupling between the beam patterns of closely spaced pixels (the two pixels in the example system are separated by about 183 dB beamwidths, corresponding to 10 cm at 4 m standoff distance, so this is not an issue in the example). Since proper detection requires that the LO chirp be phase matched to the transmit signal, each chirper is able to supply signal for both the transmit and LO upconverters for its associated pixel. Low cost 1.5-3.5 GHz isolators on the chirper power divider outputs prevent cross coupling between the IF ports of the transmit and LO upconverters.

FIG. 4 illustrates a scanning process that may be applied by the example system 150 to derive three-dimensional images of a target with multiplexed transmit beams to yield multiple simultaneous pixels. Using any known suitable beam scanning technique, the multiple transmit beams from the radar system 150 are directed to different points on the target 400. Cross sections for a side view 402B, and a top view 402C maximum of the target show the separate transmitted beams 404A, 404B along these planes directed to the target 400 at multiple points. Range information is derived for each of the scanned points (i.e., each intersection of the grid projected over the entire front view 406). The range information for each point corresponds to a pixel of the resulting three-dimensional image 408.

FIGS. 5A and 5B illustrate beam diagrams of some exemplary quasioptical devices 100 that can be used to direct the two transmit beams of the imaging radar system 150 to scan over points of the target 116 as previously described in reference to FIGS. 1A to 1C. FIG. 5A is a beam diagram of a flat mirror quasioptical device 500 where the submillimeter power transmit beams 512A, 512B are co-aligned at a polarizing wire grid 502 and then directed to a plano-convex lens 504 (e.g., comprising Teflon with a diameter of 20 cm). This lens 504 focuses the two THz transmit beams 512A, 512B to two separate spots, e.g., approximately 2 cm at a standoff range of 4 m. To achieve scanned images, a flat mirror 506 on a two-axis rotational stage 508 is manipulated to deflect the transmit beams 512A, 512B together in the desired direction to scan over the target 510 as previously described. FIG. 5B is a beam diagram of an ellipsoid reflector quasioptical device 520 for the exemplary three-dimensional imaging radar system 150. Beam focusing and scanning can alternately be accomplished by an aluminum off-axis ellipsoid reflector 522 mounted on a two-axis rotation stage 524. Using a precision machined reflector 522 (e.g., a 40 cm diameter reflector) instead of a refractive Teflon plano-convex lens 504 can boost the quasioptical efficiency by approximately 8 dB, due to lower absorption loss and the elimination of reflection loss from the approximately 2 cm thick dielectric lens. See Benford et al., “Optical properties of Zixit in the infrared to submillimeter.” Applied Optics, vol. 42, no. 25, pp. 5118-5122, Sep. 2003. In addition, clutter resulting from the lens backscattering may be eliminated. Upon leaving the trans
processor. The method pixel from the first transmit beam and a second pixel from the second transmit beam to correspond to a distinct IF frequency for demultiplexing and processing with respect to the target. What is claimed is:

1. A radar imaging system, comprising:
   a. diode for dividing a source transmit beam into a first transmit beam and a second transmit beam;
   b. a wave synthesizer for generating an FMCW chirp signal from a source local oscillator signal to generate a second IF signal for each of the first transmit beam and the second transmit beam using a first mixer. The source signal and the source local oscillator signal are then combined to generate a second IF signal using a second mixer. The first IF signal and the second IF signal are combined to generate a final IF signal for each of the first transmit beam and the second transmit beam using a third mixer. The digital signal processor performs a fast Fourier transform (FFT) to determine the frequency information for each of the first transmit beam and the second transmit beam.

2. The radar imaging system of claim 1, wherein the system for mixing comprises a first wave synthesizer for generating the source transmit beam, the source transmit beam comprising a frequency modulated continuous wave (FMCW) chirp signal from a source signal:
   a. a second wave synthesizer for generating a FMCW local oscillator chirp signal from a source local oscillator signal;
   b. a first mixer for combining the reflected FMCW chirp signal from the FMCW local oscillator chirp signal to generate a first intermediate frequency (IF) signal for each of the first transmit beam and the second transmit beam;
   c. a second mixer for combining the source signal and the second IF signal to generate a final IF signal for each of the first transmit beam and the second transmit beam using a second mixer. The second IF signal is then combined to generate a second IF signal for each of the first transmit beam and the second transmit beam using a third mixer. The digital signal processor performs a fast Fourier transform (FFT) to determine the frequency information for each of the first transmit beam and the second transmit beam.
wherein the digital signal processor performs fast Fourier transform (FFT) processing the final IF signal for each of the first transmit beam and the second transmit beam to determine range information for the target of both a first pixel from the first transmit beam and a second pixel from the second transmit beam;  
3. The radar imaging system of claim 2, further comprising a waveform generator generating a common chirp signal in 1 millisecond or less;  
wherein the first wave synthesizer generates the frequency modulated continuous wave (FMCW) chirp signal from the source signal mixed with the common chirp signal and the second wave synthesizer generates the FMCW local oscillator chirp signal from the source local oscillator signal mixed with the common chirp signal.  
4. The radar imaging system of claim 1, wherein the quasioptical device spatially offsets the second transmit beam along a substantially parallel path from the first transmit beam to a distinct point on the target.  
5. The radar imaging system of claim 1, wherein the quasioptical device directs the first transmit beam and the second transmit beam along substantially collinear paths and polarizes the second transmit beam to that of the first transmit beam to correspond to a distinct polarization for demultiplexing and processing.  
6. The radar imaging system of claim 1, wherein the quasioptical device comprises a coupler for dividing the source transmit beam into the first transmit beam and the second transmit beam;  
a polarization twist waveguide for rotating polarization of the second transmit beam relative to that of the first transmit beam; and  
quasioptical components for imparting a path length differential to induce a time delay between the second transmit beam and the first transmit beam and for directing the first transmit beam and the second transmit beam to the target along a substantially parallel path with a spatial offset.  
7. The radar imaging system of claim 1, wherein a three dimensional map of the target is derived from the range information determined for each of multiple pixels scanned over the target, where the range information for the multiple pixels are determined in simultaneously processed pairs associated with the first transmit beam and the second transmit beam.  
8. The radar imaging system of claim 7, wherein a peak-finding algorithm is applied to the determined range information to differentiate material layers of the target.  
9. The radar imaging system of claim 7, wherein the quasioptical device comprises a reflector coupled to a two-axis rotation stage and the range information is determined by positioning the two-axis rotation stage for each of the pairs of the multiple pixels scanned over the target with the reflector directing the FMCW chirp signal from the reflector to be reflected off the target and received from the target.  
10. A method of radar imaging, comprising:  
dividing a source transmit beam into a first transmit beam and a second transmit beam and multiplexing them with a quasioptical device;  
directing both the first transmit beam and the second transmit beam to be reflected off a target such that the second transmit beam is time-delayed from the first transmit beam to correspond to a distinct IF frequency for demultiplexing and processing and received as a single multiplexed receive signal with the quasioptical device; and  
signal mixing and performing fast Fourier transform (FFT) processing for demultiplexing and processing the single multiplexed receive signal to determine range information of the target for both a first pixel from the first transmit beam and a second pixel from the second transmit beam with a signal system and a digital signal processor.  
11. The method of claim 10, wherein signal mixing and performing FFT processing comprises:  
generating the source transmit beam with a first wave synthesizer, the source transmit beam comprising a frequency modulated continuous wave (FMCW) chirp signal from a source signal;  
generating a FMCW local oscillator chirp signal from a source local oscillator signal using a second wave synthesizer;  
combining the reflected FMCW chirp signal and the FMCW local oscillator chirp signal to generate a first intermediate frequency (IF) signal for each of the first transmit beam and the second transmit beam using a first mixer;  
and  
combing the source signal and the source local oscillator signal to generate a second IF signal using a second mixer; and  
12. The method of claim 11, further comprising generating a common chirp signal in 1 millisecond or less with a waveform generator;  
wherein the first wave synthesizer generates the frequency modulated continuous wave (FMCW) chirp signal from the source signal mixed with the common chirp signal and the second wave synthesizer generates the FMCW local oscillator chirp signal from the source local oscillator signal mixed with the common chirp signal.  
13. The method of claim 10, wherein the quasioptical device spatially offsets the second transmit beam along a substantially parallel path from the first transmit beam to a distinct point on the target.  
14. The method of claim 10, wherein the quasioptical device directs the first transmit beam and the second transmit beam along substantially collinear paths and polarizes the second transmit beam to that of the first transmit beam to correspond to a distinct polarization for demultiplexing and processing.  
15. The method of claim 10, wherein the quasioptical device comprises a coupler for dividing the source transmit beam into the first transmit beam and the second transmit beam;  
a polarization twist waveguide for rotating polarization of the second transmit beam relative to that of the first transmit beam; and  
quasioptical components for imparting a path length differential to induce a time delay between the second transmit beam and the first transmit beam and for directing the first transmit beam and the second transmit beam to the target along a substantially parallel path with a spatial offset.  
16. The method of claim 10, wherein a three dimensional map of the target is derived from the range information determined for each of multiple pixels scanned over the target, where the range information for the multiple pixels are determined in simultaneously processed pairs associated with the first transmit beam and the second transmit beam;  
and  
wherein signal mixing and performing FFT processing comprises:  
generating the source transmit beam with a first wave synthesizer, the source transmit beam comprising a frequency modulated continuous wave (FMCW) chirp signal from a source signal;  
generating a FMCW local oscillator chirp signal from a source local oscillator signal using a second wave synthesizer;  
combining the reflected FMCW chirp signal and the FMCW local oscillator chirp signal to generate a first intermediate frequency (IF) signal for each of the first transmit beam and the second transmit beam using a first mixer;  
and  
combing the source signal and the source local oscillator signal to generate a second IF signal using a second mixer; and.
determined in simultaneously processed pairs associated with the first transmit beam and the second transmit beam.

17. The method of claim 16, wherein a peak-finding algorithm is applied to the determined range information to differentiate material layers of the target.

18. The method of claim 16, wherein the quasioptical device comprises a reflector coupled to a two-axis rotation stage and the range information is determined by positioning the two-axis rotation stage for each of the pairs of the multiple pixels scanned over the target with the reflector directing the FMCW chirp signal from the reflector to be reflected off the target and received from the target.

19. An apparatus for multiplexing in a radar imaging system, comprising:
   - a coupler for dividing the source transmit beam into a first transmit beam and a second transmit beam and multiplexing them;
   - a polarization twist waveguide for rotating polarization of the second transmit beam relative to that of the first transmit beam;
   - quasioptical components for imparting a path length differential to induce a time delay between the second transmit beam and the first transmit beam and for directing the first transmit beam and the second transmit beam to the target along a substantially parallel path with a spatial offset;
   - wherein both the first transmit beam and the second transmit beam are directed to be reflected off a target and received as a single multiplexed receive signal by the quasioptical device and the single multiplexed receive signal is demultiplexed and processed to determine range information of the target for both a first pixel from the first transmit beam and a second pixel from the second transmit beam.

20. The apparatus of claim 19, wherein the source transmit beam comprises a frequency modulated continuous wave (FMCW) chirp signal.