Remote Sensing of Dissolved Oxygen and Nitrogen in Water Using Raman Spectroscopy

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Abstract

The health of an estuarine ecosystem is largely driven by the abundance of dissolved oxygen and nitrogen available for maintenance of plant and animal life. An investigation was conducted to quantify the concentration of dissolved molecular oxygen and nitrogen in water by means of Raman spectroscopy. This technique is proposed for the remote sensing of dissolved oxygen in the Chesapeake Bay, which will be utilized by aircraft in order to survey large areas in real-time. A proof of principle system has been developed and the specifications are being optimized to maximize efficiency for the final application. The theoretical criteria of the research, components of the experimental system, and key findings are presented in this report.

I. Introduction

Dissolved oxygen (DO), i.e. molecular oxygen (O$_2$), in ocean waters is critical for stability and survival of marine ecosystems and organisms. Declining DO concentrations will elicit dire consequences for global biogeochemical cycles, marine habitats, and the native organisms. Diminished concentrations of DO can be fatal, and for most aquatic species this critical point is $\sim$4 mg/L DO in water [1]. Areas of water with oxygen concentrations under 2 mg/L are hypoxic and considered anoxic once concentrations reach 0 mg/L. Anoxic areas are referred to as dead zones, which are primarily located in coastal waters due to shallow water depth, abundance of biological activity, and tangency to land [2]. Currently, less than 25% of dead zones have DO measurements, so there is a need for more efficient methods of mapping concentrations in large-scale coastal areas [3].

A substantial portion of the Chesapeake Bay, the largest estuary in the United States, is considered critically hypoxic or anoxic. The use of fertilizer for crop production, resulting in a large input of reactive nitrogen compounds and phosphorous through direct deposition by wastewater run-off and atmospheric deposition, is the primary contributor to coastal hypoxia in the Chesapeake Bay [4]. The increased discharges add a surplus of nutrients, a process known as eutrophication. Hypoxia due to eutrophication occurs when an overabundance of nutrients in the water enable rapid increase of algae populations, known as algal blooms. The algae in these blooms are short lived, and microbes readily decompose the remaining organic material. This process of microbial degradation generates an aberrant increase in aerobic respiration activity, causing the microbes to rapidly consume oxygen; thus, depleting the DO content of the water [5]. A recent scientific overview states that coastal eutrophication has become an increasingly urgent global concern that is responsible for the steady growth in the magnitude and persistence of hypoxic coastal waters [6].

The current measurement technique for dissolved oxygen is Optode technology, which requires direct in-situ measurements. An optode is an optical sensor device that uses a chemical transducer to measure a specific substance [7]. Optodes are spatially limited, as they require direct contact with the water. The extended time it requires a vessel to travel the entirety of the measurement region allows variation in water conditions to occur and produces readings that are not temporally aligned [8]. A national interagency scientific assessment committee agree on the insufficiency of current ship-based surveys due to the temporal dynamics of hypoxia; nonetheless, advocate that this can be resolved through “new technologies for measuring dissolved oxygen, that can be deployed in the field to provide continuous measurements” [9].
Water in coastal regions continuously comes in contact with air due to low depth and active currents; therefore, the predominant gases dissolved in ocean water are molecular nitrogen (N\textsubscript{2}) and oxygen (O\textsubscript{2}). Studies have shown that sea water is virtually saturated with dissolved nitrogen and therefore the concentration remains constant regardless of biological activity [10]. Despite oxygen being more water soluble than nitrogen, its concentration is lower due to overall higher abundance of atmospheric nitrogen. The relative volume percent concentration of N\textsubscript{2} in sea water is 63.3\% compared to 35.6\% for O\textsubscript{2}, assuming 100\% saturation of both gases at 1 atm (up to depth of approx. 10m) [11]. A discrepancy in the N\textsubscript{2} to O\textsubscript{2} ratio (1.78) would indicate the extent of DO depletion; thus, it is necessary to measure both O\textsubscript{2} and N\textsubscript{2} to fully evaluate the concentration of dissolved gases.

This paper will describe a new Raman remote sensing technique that could measure the concentration of DO and N\textsubscript{2} from aircraft throughout the Chesapeake Bay or other water body. This remote sensing technique will allow high resolution, real-time measurement of critically important dissolved gases; furthermore, these measurements could substantially improve our understanding of the temporal and spatial dynamics of dissolved gas distributions in maritime coastal ecosystems. The goal of this research effort is to provide evidence that remote sensing of water using Raman spectroscopy is a viable approach to measure both O\textsubscript{2} and N\textsubscript{2} in coastal waters; and subsequently, provide groundwork to design an aircraft based lidar system for spatial and temporal mapping of O\textsubscript{2} and N\textsubscript{2} in coastal regions such as the Chesapeake Bay.

II. Experimental Setup

In the remote DO Raman sensing technique, a pulsed UV laser is directed into a water specimen. The UV laser emission induces an electric dipole moment, thus changing the molecular polarizability and bringing the O\textsubscript{2} and N\textsubscript{2} molecules to a virtual excited state. The difference in energy between the ground and virtual states create a wavelength shift, radiating longer wavelength Raman emission at a wavelength specific to the polarization potential characteristic of the molecule [12]. This shifted emission wavelength is backscattered to the lidar receiver where it is detected. The detected signal is directly proportional to the water concentration of O\textsubscript{2} and N\textsubscript{2} [13]. The Raman differential scattering cross-section (cm\textsuperscript{2}/sr), which is needed to quantify the probability of photon-molecule interaction, varies inversely with the fourth power of the excitation laser wavelength [12]. The Raman shifts for 355nm laser excitation, corresponding wavelengths, and cross sections of molecular species pertinent to this work are shown in Table 1.

<table>
<thead>
<tr>
<th>Molecular Species</th>
<th>Raman shift (cm\textsuperscript{-1})</th>
<th>λ (nm)</th>
<th>σ, 10\textsuperscript{-30} cm\textsuperscript{2}/sr \textsuperscript{[14,15]}</th>
</tr>
</thead>
<tbody>
<tr>
<td>O\textsubscript{2}</td>
<td>1556</td>
<td>376.2</td>
<td>1.1</td>
</tr>
<tr>
<td>H-O-H (bending mode, ν\textsubscript{2})</td>
<td>1640</td>
<td>377.4</td>
<td>0.54</td>
</tr>
<tr>
<td>N\textsubscript{2}</td>
<td>2331</td>
<td>387.5</td>
<td>2.1</td>
</tr>
<tr>
<td>O-H (symmetric stretch, ν\textsubscript{1})</td>
<td>3450</td>
<td>405.1</td>
<td>56.3</td>
</tr>
</tbody>
</table>

A schematic of the experimental setup appears in Figure 1. A flashlamp pumped Nd-YAG Laser (Continuum PL9050), is Q-switch operated at a repetition rate of 30Hz, with a power of
1.8 W at 355nm. The YAG fundamental pulse output is frequency tripled using a KTP nonlinear crystal and generates a pulse at the third harmonic; these parameters are outlined in Table 2.

**Table 2. Third Harmonic Generation Performance Parameters**

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Energy</td>
<td>60 mJ</td>
</tr>
<tr>
<td>Stability</td>
<td>±4%</td>
</tr>
<tr>
<td>Pulsewidth</td>
<td>7ns</td>
</tr>
<tr>
<td>Polarization</td>
<td>&gt;95% horizontal</td>
</tr>
<tr>
<td>Linewidth</td>
<td>1.5 cm⁻¹</td>
</tr>
<tr>
<td>Repetition Rate</td>
<td>30 Hz</td>
</tr>
</tbody>
</table>

The third harmonic provides the excitation wavelength of 355nm. Near UV excitation wavelengths are optimal for Raman scattering from O₂ and N₂, which provide relatively weak signals particularly in liquid medium. The intensity of Raman scattering decreases as the fourth power of the wavelength, so using shorter laser excitation wavelengths are preferred [12].

**Figure 1.** Raman scattering dissolved oxygen/nitrogen experimental setup.

The 355nm pulses pass through a hole in a 10cm diameter flat aluminum coated deflection mirror and into a 1.88m x 10cm diameter glass water cell. As the beam passes through the water...
cell, the UV photons excite molecules in the beam path, producing inelastic Raman scattering. The backscattered photons pass back through the water cell and are deflected off the aluminum flat mirror to the focusing lens, which directs the light into a monochromator (Optometrics Corp., model SDMC1-01). The monochromator transmits only the manually selected wavelength of UV light, and is fitted with 355nm blocking filters (Semrock # LPO2-355RU-25) to attenuate the noise signal received from the 355nm laser. A photomultiplier tube (PMT) (Electron Tubes, Inc., 9125QSA) on the monochromator converts the photons into an electrical signal that can be detected by an oscilloscope. In conjunction with the oscilloscope, a gated integrator and boxcar averager module (Stanford Research Systems SR250) acquires and analyzes the PMT signals, increasing the signal to noise ratio by averaging.

The water cell has an attached vertical column to house a Troll 9500 dissolved oxygen in situ monitor (In-Situ Inc Troll 9500). The Troll measures an array of water parameters, such as: temperature, barometric pressure, conductivity, pH, and dissolved oxygen. Troll measurements are used for calibration of DO concentration measurements in the experimental setup. The specifications of these sensors are provided in Table 3. To attain maximum solubility of the dissolved gases in the glass cell during tests, an air bubbler is utilized to saturate the water. Bubbler tubes run up through the water cell’s vertical portion and are fitted along the bottom of the horizontal tube. A thermocouple temperature measurement records water temperature and two thermocouple wires are fitted to the bubbler tubes that run the length of the water cell. The outer perimeter of the glass cell is wrapped with heating tapes to facilitate increasing the water temperature.

### Table 3. Troll 9500 Sensor Specifications

<table>
<thead>
<tr>
<th>Conductivity</th>
<th>Temperature</th>
</tr>
</thead>
<tbody>
<tr>
<td>Type: 4-cell conductivity, AC drive</td>
<td>Type: Platinum resistance thermometer</td>
</tr>
<tr>
<td>Operating range:</td>
<td>Range: -5°C to 50°C</td>
</tr>
<tr>
<td>Low: 5µS/cm, 20,000µS/cm</td>
<td>Accuracy: ±0.1°C</td>
</tr>
<tr>
<td>High: 150µS/cm to 112,000µS/cm</td>
<td>Resolution: 0.01°C</td>
</tr>
<tr>
<td>Accuracy:</td>
<td>Barometric pressure</td>
</tr>
<tr>
<td>Low: ±0.5% or 2µS/cm</td>
<td>Type: Piezoresistive Si pressure sensor</td>
</tr>
<tr>
<td>High: ±0.5% +2µS/cm</td>
<td>Range: 0-16.5 psia (854mm Hg, 33.6in Hg)</td>
</tr>
<tr>
<td>Resolution: Range-dependent</td>
<td>Accuracy: ±0.3% FS (2.54mm Hg, 0.1in Hg)</td>
</tr>
<tr>
<td>Pressure rating: 350 psi (246m, 807ft)</td>
<td>Resolution: 0.1mm Hg, 0.01in Hg</td>
</tr>
<tr>
<td>Operating temperature: 5°C to 50°C</td>
<td>pH</td>
</tr>
<tr>
<td>Dissolved oxygen</td>
<td>Type: Glass sensing bulb, single junction electrode, replaceable ceramic junction, refillable reference electrolyte</td>
</tr>
<tr>
<td>Type: Optical, fluorescence quenching</td>
<td>Range: 0 to 12 pH units</td>
</tr>
<tr>
<td>Range: 0 to 20 mg/L, 0 to 450% saturation</td>
<td>Pressure rating: 350 psi (246m, 807ft)</td>
</tr>
<tr>
<td>Pressure rating: 300 psi</td>
<td>Operating temperature: 0°C to 50°C</td>
</tr>
<tr>
<td>Operating temperature: 0°C to 40°C</td>
<td>Accuracy: ±0.1 pH unit</td>
</tr>
<tr>
<td>Accuracy: ±0.1 mg/L @ 0-8 mg/L</td>
<td>Resolution: 0.01 pH unit</td>
</tr>
<tr>
<td>±0.2 mg/L @ 8-20 mg/L</td>
<td>Resolution: 0.01 mg/L</td>
</tr>
</tbody>
</table>
For calibration of the Troll measurement, distilled water was air bubbled and DO content was measured as a function of time to determine the rate of water saturation. After approximately 20 minutes of bubbling, the water reaches full DO saturation, as shown in Figure 2. Upon full saturation, the DO content was measured as a function of gradually increasing water temperature in order to confirm an accurate solubility measurement of DO. The solubility attained by the Troll measurement is congruent with the literature value [16], as shown in Figure 3.

Water temperature recordings are an average of measurements from three locations along the water cell, and are maintained within 0.5°C. The Troll 9500 measurement utilizes automatic internal salinity correction factors, which adjust the recorded conductivity (µS/cm or PSU) of the water. Theoretical DO content (mg/L) at 100% saturation must be manually corrected by salinity factors, which are given by the conductivity at various water temperatures [16].

The sample of water used for testing was retrieved from the Back Bay, VA, a tributary of the Chesapeake Bay near NASA Langley Research Center, Hampton, VA.

Due to the experimental configuration, a gap between the deflection mirror and water cell creates an air interface. The possibility that this interface is the source of the detected oxygen and nitrogen signals was eliminated when the water cell window was blocked, and all signal intensity immediately dropped to noise; thus, the detected bands are a product of inelastic Raman backscattering within the water cell.

**Figure 2.** Saturation time of DO (mg/L) in water at 22°C, 1 atm.
Figure 3. Experimentally acquired by the Troll solubility of DO (mg/L) in distilled water with increasing water temperature compared with theoretical prediction given by tabulated values [16].

III. Dynamics of Dissolved Gases in Water

A study by Emerson et al [17] quantitatively measured the total gas pressure in water to exist as it does in the atmosphere, thus as the sum of its partial pressures of constituent gases. To obtain the total gas pressure in water \( w \) in terms of \( N_2 \) and \( O_2 \) in water, it must be assumed that \( Ar, H_2O, \) and \( CO_2 \) are at equilibrium with the atmosphere \( a \), hence,

\[
p_{Ar}^w + p_{H_2O}^w + p_{CO_2}^w = p_{Ar}^a + p_{H_2O}^a + p_{CO_2}^a \tag{1}
\]

These species often have large variabilities in sea water, but are present at such miniscule concentrations that this assumption does not affect measurement accuracy by more than 0.2%. The partial pressure of the dissolved gas is related to its concentration in seawater, as a function of temperature and salinity. This function creates the solubility coefficient, the reciprocal of which is equivalent to the Bunsen coefficient [17].
The Bunsen coefficient \( B_G \) is used to describe gas solubilities in liquids, and is defined as the volume of a gas absorbed per unit volume liquid at a specific temperature of measurement, when the partial pressure of that gas is 1 atm [19]. Any unit of volume can be used to describe the gas and liquid volumes, as long as both are the same [20]. The Bunsen coefficient is dependent on salinity as well as temperature, as shown in Figures 4a & b. This coefficient describes the solubility of a dissolved gas as a unitless value [21].

The gas partial pressure in water is the gas pressure that would be in equilibrium with the seawater concentration at the measured temperature and salinity. At saturation equilibrium, the partial pressure of gases in surface water are equal to the values in a water vapor saturated atmosphere [17]. As water depth increases, the absolute pressure increases and thus the partial pressures of the dissolved species increase as well, as shown in Figure 5.
Figure 5. The partial pressures of N\textsubscript{2} and O\textsubscript{2} as functions of water depth and absolute pressure, calculated using the species mole fractions listed in Table 4. At zero water depth the partial pressures are equivalent to the atmospheric partial pressures.

Figure 6. The theoretical concentration of N\textsubscript{2} vs partial pressure per unit air pressure of N\textsubscript{2} as function of water temperature, calculated using equation 2 and the Bunsen coefficients from Figure 4.
Using the Bunsen coefficient to account for the solubility specific to each gas, in conjunction with partial pressure derived by depth, the theoretical concentration of the gas at 100% saturation can be determined, as shown in Figure 6 [19]. This relationship is described by equation 2 as

\[ C_{N_2} = P_{N_2} \cdot B_{N_2} \]  

(2)

where \( C \) is the concentration, \( P \) is the partial pressure, and \( B \) is the Bunsen coefficient; each specific to \( N_2 \), but can similarly be applied to \( O_2 \). Water temperature, salinity, and depth are all measurable by remote sensing techniques, and an algorithm can be written to account for these variables in real time.

IV. Methodology for Raman Spectroscopic Analysis

For data analysis, all Raman signals are normalized to 1W, 355nm laser power. Wavelength calibration was performed using a Hg vapor lamp. Known Hg wavelengths at 365.19, 366.59 and 404.60 nm were used to calibrate the monochromator [23]. A secondary calibration was performed using the relative position of the 377.4nm Raman water bending mode peak, shown in Figure 7.

![Figure 7](image)

**Figure 7.** Experimentally acquired monochromator calibration using peak of water bending mode (literature value: 377.40nm) [24].
In order to determine the 355nm laser attenuation through the water medium, the transmittance ($T$) of 355nm light was measured. Theoretical and experimental absorption of distilled water was calculated using equations 3 and 4 respectively. The optical absorption coefficient at 355nm is 0.01517m$^{-1}$ for distilled water [25]. Experimental transmission values are taken as a mean of multiple measurements. Total cell window loss was measured and found to be 0.155 absorption.

\[
I = I_o e^{-[0.01517m^{-1} \cdot 1.88m]} = 0.972 \text{ transmittance theoretical (3)}
\]
\[
1-0.972 = 0.028 \text{ absorption theoretical}
\]
\[
T = \frac{I}{I_o} = 0.78 \text{ transmittance + 0.155 cell window absorption = 0.935 (4)}
\]
\[
1-0.930 = 0.065 \text{ absorption measured}
\]

The measured absorption of distilled water was calculated to be 0.065, which is comparable to the theoretical absorption of 0.028. The discrepancy seen here is likely due to particle accumulation in the water cell over time, increasing sources of scattering. Theoretical and measured absorption of Back Bay water was then calculated using equations 5 and 6 respectively. The optical absorption coefficient at 355nm wavelength is 0.58m$^{-1}$ for Back Bay water [26].

\[
I = I_o e^{-[0.58m^{-1} \cdot 1.88m]} = 0.336 \text{ transmittance theoretical (5)}
\]
\[
1-0.336 = 0.66 \text{ absorption theoretical}
\]
\[
T = \frac{I}{I_o} = 0.0048 \text{ transmittance + 0.155 cell window absorption = 0.1598 (6)}
\]
\[
1-0.1598 = 0.84 \text{ absorption measured}
\]

The measured absorption of Back Bay water was calculated to be 0.84, which is comparable to the theoretical absorption of 0.66. Back Bay water contains an abundance of ionic compounds and organic particulates not found in distilled water, which provide greater scattering of incident light, thus increasing absorption.

Number densities ($n$) of target species, e.g. DO, provide the number of molecules per volume and is used in conjunction with the Raman scattering cross section to determine concentrations of O$_2$ and N$_2$ molecules in water. The number density is proportional to the Raman scattering. Number densities were calculated based on the molecular species mass density ($\rho$) at 100% saturation, 20°C and 1 atm pressure, as shown in equation 7. Avogadro’s constant ($N_{Av}$) refers to the number of molecules in 1 mole of a particular substance, with a value of 6.02214x10$^{23}$ mol$^{-1}$. The molar mass (M) of that particular substance is determined by the species molecular mass and amount present, expressed in g/mol [27].

\[
n = \frac{N_{Av}}{M} \rho \quad (7)
\]

The saturation number density calculation for O$_2$ in seawater accounts for salinity at 35ppt, which lowers maximum saturation; therefore, causing a decrease in mass density from 9.08x10$^{-9}$ kg/cm$^3$ to 7.2x10$^{-9}$ kg/cm$^3$. Number density values are provided in Table 4.
The primary mechanism for quantitative analysis of Raman spectroscopy is the proportional relationship between gas concentration and Raman backscatter intensity [13]. The molecular species concentration can be derived from the Raman scattering intensity and other parameters, as shown by,

\[ C = \frac{I_r}{(I_L \sigma \eta)} P \]  

(8)

where \( C \) is the species number density, \( I_r \) is the measured Raman backscatter intensity integrated over the band width, \( I_L \) is the laser intensity, \( \sigma \) is the species Raman cross-section, \( \eta \) includes instrument parameters (e.g. optical transmission), and \( P \) is the sample path length [28]. Variable path length modulates Raman intensity; therefore, peak heights and areas are not necessarily the same for different measurement water depth. In a typical aircraft lidar scenario the water path length would vary widely and this variance must be accounted for in calculations. Additionally, relative concentrations are independent of path length, and can be determined using the peak ratio method described by Wopenka and Pasteris [29], and specifically employing the two-component system described by Sum et al. [30],

\[ \frac{C_{H_2O}}{C_{O_2}} = \frac{A_{H_2O}}{A_{O_2}} \frac{\sigma_{O_2}}{\sigma_{H_2O}} \frac{\eta_{O_2}}{\eta_{H_2O}} \]  

(9)

where \( C \) is the concentration of molecular species in a sample; \( A \) is the measured Raman band area, \( \eta \) is the instrument efficiency correction factors and \( \sigma \) is the absolute Raman scattering cross section values. These factors provide a relative, empirically derived, and instrument specific calibration; therefore, must be calculated for each experimental setup [29]. This concentration ratio technique provides an expression comparable to the Beer-Lambert Law and can be applied similarly, also by creation of a calibration curve. Through Raman measurement, it has been shown that simple gas mixtures yield a linear calibration curve [31].

V. Results and Discussion

Oxygen and nitrogen Raman peaks were initially optimzed in air to confirm wavelengths of the molecular species at 376.2 and 387.55nm, respectively [12]. Raman signals obtained using
the experimental setup were recorded every 0.2 nm and scanned between 364.4 nm-390.4 nm, as shown in Figure 8.

**Figure 8.** Experimentally measured Raman backscattered spectra of air and water.

A comparison of the N\textsubscript{2} and O\textsubscript{2} number densities noted in Table 4 show that the ratio N\textsubscript{2}/N\textsubscript{2\textsuperscript{w}} is 66, and O\textsubscript{2}/O\textsubscript{2\textsuperscript{w}} is 32, thus the Raman scattering intensities are 66 and 32 times below that of the air measurement shown in Figure 8. This significant difference in magnitude is the reason N\textsubscript{2} and O\textsubscript{2} are not visible in the experimentally acquired Raman water spectrum shown in Figure 8.

Due to the inherently lower concentrations of gases in water than that in air, optimizing the O\textsubscript{2} and N\textsubscript{2} backscattered signals require scanning much shorter wavelength increments, 0.02 nm, and as an average of 1k samples, increasing signal to noise ratio and thus providing more precise band measurement.

In accordance with solubility laws, the concentration of a gas decreases with increasing water temperature; likewise, in accordance with Raman spectroscopy theory, the concentration of a molecular species is directly proportional to the signal intensity. As the water temperature increases, the signal intensity decreases; thus the N\textsubscript{2} concentration is also decreasing, as shown in the experimental measurements in Figure 9. This data supports that N\textsubscript{2} was in fact observed by
Raman backscattering at 387.55nm. To further justify this outcome, N$_2$ and O$_2$ Raman bands were scanned at various levels of DO saturation, as shown in Figures 10 and 11.

\[
y = -1.5346 + 0.0075508x \quad R= 0.77073
\]

**Figure 9.** Measured relative N$_2$ peak intensity at 387.55nm as a function of increasing water temperature.

The Raman N$_2$ peak band was scanned at two different concentrations of DO; 6.01 and 8.70 mg/L, as shown in Figure 10. The temperature and pressure are the same for both spectra; 24°C and 760 mmHg. Likewise, Figure 11 shows the Raman O$_2$ peak band scanned at three different concentrations of DO; 6.04, 8.80, and 9.11 mg/L. The temperature and pressure are the same for all three spectra; 24°C and 760 mmHg. The change in peak intensities shown in Figure 11 result from the change in dissolved oxygen content in the water. In this setup, the percent saturation of O$_2$ can be used to infer the percent saturation of N$_2$, since there is no biological activity affecting oxygen content, and bubble action produces nearly equal supersaturation for all dissolved gases, as noted in a study by Memery and Merlivat [32]. The concentration of N$_2$ can then be calculated by the degree of saturation. In seawater, O$_2$ is produced biologically, so the percent saturation can not be assumed equivocal with N$_2$, which is an inert gas not affected by biological activity.
Figure 10. Measured relative intensity of N\textsubscript{2} band peak as function of Troll DO content (mg/L) at 24°C and 1 atm.

Figure 11. Measured relative intensity of O\textsubscript{2} band peak as function of Troll DO content (mg/L) at 24°C and 1 atm.
Raman spectra can be analyzed by superposition of overlapping bands of non-equivalent species, such as O\(_2\) and the H\(_2\)O bending mode. Observation of changes in band width or shape result from a change in the non-equivalent species relative concentrations [13]. Previous researchers have employed comparing Raman water bands with gas species in aqueous phase by use of a ratio technique. A study by White [31] describes utilizing the water stretching band to create a calibration curve which serves as a reference for quantitative analysis. Using this approach, dissolved gas species can be identified and quantified at various pressures, temperatures, and salinity due to the relative constant intensity of the H\(_2\)O band. The H\(_2\)O peak area, unlike dissolved gas peak areas, does not change in response to variation of those parameters [31].

\[ y = 3855.9 - 378.83x \quad R = 0.99956 \]

**Figure 12.** Measured dissolved O\(_2\) concentration as given by Troll vs. H\(_2\)O/O\(_2\) peak area ratio in Back Bay water.

Using the Raman experimental setup, a measurement was taken of DO content in Back Bay water, as shown in Figure 12. The area of the O\(_2\) peak at 376.2nm is ratioed to the H\(_2\)O bending peak at 377.4nm. The Raman peak areas were calculated using half widths and peak heights measured from the spectrums shown in Figures 7 and 11. The H\(_2\)O band area remains constant as a function of DO, so changes in the H\(_2\)O/O\(_2\) ratio are attributed to changing O\(_2\) peak area. The Raman peak area of DO is directly proportional to changes in DO concentration. The peak area ratio as a function of DO concentration give a linear calibration curve, which can be used as a quantitative measurement of DO concentration.

With sufficient data, this ratio technique could be used to assemble a calibration curve to show the linear relationship between N\(_2\)/O\(_2\) mole fraction ratio and N\(_2\)/O\(_2\) Raman peak area.
The mole fraction ratio of a gas mixture directly correlates to the Raman peak area ratio of that gas mixture at the same total pressure. A proportionality constant between the two ratios would provide a linear correlation to convey the level of saturation of the dissolved gases in the water.

The area of a Raman peak of a particular species is quantified as a function of the absolute concentration of the species, Raman cross section of the species, irradiance, and the solid angle of light collection. The absolute concentration is the number of molecules in the scattering volume. The scattering volume, irradiance and solid angle are presumably equivalent for all species simultaneously analyzed in the water column [13]. Therefore, to accurately determine the N₂/O₂ concentration ratio the two species must be scanned over a continuous spectrum.

VI. Future Work

The block diagram in Figure 13 illustrates one proposed configuration for the remote Raman sensing flight experiment to measure dissolved gases in coastal waters. The deployment configuration employs the technique described in this paper with the modifications necessary for in-flight measurement of dissolved gases in coastal waters.

In order to develop a system capable of acquiring reliable and precise measurements, certain variables must be simultaneously measured, such as water temperature and gas saturation. While DO concentrations (mg/L) can be derived by Raman spectroscopy, the conditions at which those concentrations are measured are also necessary to ensure precision of that measurement. Water temperature can also be measured by Raman spectroscopy, from the change in peak width and intensity of the water bending and stretching modes [33]. Saturation is dependent upon multiple variables itself, such as salinity, and gas exchange across the air-water interface. For calm conditions, the gas exchange constant for oxygen has been shown to increase as the square of the wind velocity, and the exchange flux is proportional to the partial pressure difference between water and air [34,35]. Bubble action, on average, drives ocean water to super-saturation of a few percent for gases such as oxygen. When water is turbulent, this increased bubble exchange can increase the gas exchange constant to a third or fourth power of the wind velocity, as well as alter the proportionality of the exchange flux [34]. The solubility of O₂ and N₂ in water decreases with increased salinity; therefore, salinity adjustments are a necessary component to calculate accurate dissolved gas saturation. Salinity distributions throughout the Chesapeake Bay and its tributaries vary with current, seasonal changes and on a yearly basis [36]. This distribution is commonly mapped by use of airborne microwave radiometry as well as satellite ocean color radiometry [37].
VII. Conclusion

A laser system capable of detecting dissolved O\textsubscript{2} and N\textsubscript{2} in water has been demonstrated and is ready for implementation to a remote sensing lidar application. This initial research has been sufficient to demonstrate the theoretical principle, proving the validity of the DO measurement Raman technique. Raman spectroscopic measurement of O\textsubscript{2} and N\textsubscript{2} in water have been performed and shown to produce quantitative measurements when ratioed to the H\textsubscript{2}O bending peak. This research represents a novel approach to addressing the problems of hypoxia in estuarine systems, and has shown that it is possible to measure concentrations of dissolved oxygen and nitrogen by a remote sensing technique and has the potential capability to parallel the high accuracy of in-situ DO measurements. This new remote sensing technique will allow much higher temporal and spatial DO measurements at comparable accuracies when compared to current in-situ techniques.

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Remote Sensing of Dissolved Oxygen and Nitrogen in Water Using Raman Spectroscopy

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Remote Sensing of Dissolved Oxygen and Nitrogen in Water Using Raman Spectroscopy

Lidar; Oxygen; Raman spectroscopy; Remote sensing

The health of an estuarine ecosystem is largely driven by the abundance of dissolved oxygen and nitrogen available for maintenance of plant and animal life. An investigation was conducted to quantify the concentration of dissolved molecular oxygen and nitrogen in water by means of Raman spectroscopy. This technique is proposed for the remote sensing of dissolved oxygen in the Chesapeake Bay, which will be utilized by aircraft in order to survey large areas in real-time. A proof of principle system has been developed and the specifications are being honed to maximize efficiency for the final application. The theoretical criteria of the research, components of the experimental system, and key findings are presented in this report.