Atmospheric Mining in the Outer Solar System: Aerial Vehicle Mission and Design Issues

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Introduction

• Why atmospheric mining?
• Resource capturing: helium 3, hydrogen, helium.
• Aerospacecraft as uninhabited aerial vehicles (UAVs), cruisers for weather reconnaissance, monitoring, etc.
• Engine issues.
  – Gas core engines, closed cycle.
  – Lifetime(s).
• Orbital transfer vehicle (OTV), lander, factory sizing and optimization(s).
• Observations.
• Concluding remarks.
In Situ Resource Utilization (ISRU)

• In Situ Resource Utilization uses the materials from other places in the solar system to sustain human exploration

• Using those resources reduces the reliance on Earth launched mass, and hopefully reduces mission costs

• There are powerful capabilities to free humans from Earth
Why Atmospheric Mining?

• **Benefits:**
  – Large amount of matter to mine (hydrogen and helium 3)
  – Potentially easier than mining regolith (dust) and rock
  – Larger reservoir of materials not readily available in regolith (and in a gaseous state)

• **Potential drawbacks**
  – Dipping deep into the gravity well of planets is expensive for propulsion systems
  – Lifetime of systems
  – Repetitive maneuvers
  – Cryogenic atmospheric environments
  – Long delivery pipelines
Uranus

JPL
Neptune

JPL
Neptune and Moons

HST ACS/HRC

Proteus

Galatea

Despina

50,000 kilometers
31,000 miles

Larissa
Outer Planet Atmospheres

Tristan Guillot, “Interiors of Giant Planets Inside and Outside the Solar System.”
Outer Planet Atmospheres and Wind Speeds

JPL, Ingersoll
Uranus – Outer Planet Atmospheres and Wind Speeds

Sromovsky, L., 2010, Investigating Atmospheric Change on Uranus and Neptune, Award number NNG05GF00G.
Uranus –
Outer Planet
Atmospheres
and
Wind Speeds

Sromovsky, L., 2010, Investigating Atmospheric Change on Uranus and Neptune, Award number NNG05GF00G.
Uranus – Outer Planet Atmospheres and Wind Speeds
ASC - UAV Selection: Weather (2/2)

Figure B3. Neptune cloud features (Voyager, Hubble, Ref. 27)
# Orbital Velocities: 10 km altitude

<table>
<thead>
<tr>
<th>Planet</th>
<th>Delta-V (km/s)</th>
<th>Comment</th>
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<tbody>
<tr>
<td>Jupiter</td>
<td>41.897</td>
<td>BIG</td>
</tr>
<tr>
<td>Saturn</td>
<td>25.492</td>
<td>BIG</td>
</tr>
<tr>
<td>Uranus</td>
<td>15.053</td>
<td>More acceptable</td>
</tr>
<tr>
<td>Neptune</td>
<td>16.618</td>
<td>More acceptable</td>
</tr>
</tbody>
</table>
Cruiser Mining (1)
Combined Miner and Aerospacecraft

- Cruiser: mining aerospacecraft (a)
- Cruiser: departs atmosphere (b)
- OTV
- Fuel storage facility
- Uranus atmospheric mining altitude
- Uranus atmospheric interface
- Uranus orbit
- Earth orbit
Mining Scenarios and OTVs

• Using cruiser aerospacecraft for mining in the atmosphere at subsonic speeds.
• Cruiser aerospacecraft then ascends to orbit, transferring propellant payload to orbital transfer vehicles (OTV).
• OTV will be the link to interplanetary transfer vehicle (ITV) for return to Earth.
• Moon bases for a propellant payload storage option was investigated.
AMOSS GCR Designs
Gas Core Design and Analysis Overview

• Total aerospacecraft vehicle delta-V is 20 km/s.
• Single stage aerospacecraft.
• Gas core Isp values = 1800 and 2500 seconds.
• Vehicles mass estimated over a broad range of dry masses.
• Dry mass (other than tankage) = 1,000, 10,000, 100,000, and 1,000,000 kg.
  – Typical gas core dry mass = 80,000 to 200,000 kg.
• Tankage mass = 2% and 10% of propellant mass.
• Comparative case: solid core NTP Isp = 900 seconds.
Gas core, Isp = 1,800 s, Tankage = 2% Mp

Nuclear Aerospacecraft, OC Gas Core; 1,800-s Isp; 20-km/s delta-V capability; 1,000-kg payload

Initial mass (Mo)
Final mass (Mf)
Tankage mass fraction = 2% Mp, for H2

Aerospacecraft mass, initial and final (kg)
Dry mass, without tankage (kg)
AMOSS NTP Designs: Solid Core and Gas Core

Nuclear Aerospacecraft:
Dry mass = 100,000 kg, Tankage mass = 2% \( M_p \)

Aerospacecraft initial mass (kg)

- 900 s
- 1800 s
- 2500 s

Engine specific impulse (s)
Time for 3He Capture at Uranus

Time needed for capturing 3He, 500 kg of 3He captured, 3He concentration = $1.52 \times 10^{-5}$ in total atmosphere (Uranus)

3He Mining time (days)

Atmospheric capture rate (kg/s)
Time for 3He Capture at Neptune

Time needed for capturing 3He, 500 kg of 3He captured, 3He concentration = $1.9 \times 10^{-5}$ in total atmosphere (Neptune)
Resource Capturing – Hydrogen, Helium 4, and Helium 3 Comparison, Uranus
AMOSS, Hydrogen Production at Uranus

AMOSS 3He mining time and hydrogen capturing requirements,
$3\text{He} = 1.52e^{-5}$, $M_{\text{dry}} = 100,000$ kg

- Time needed for capturing 3He (days)
- Mass of hydrogen produced per day
- Gas core, 1800 s
- Gas core, 2500 s

Graph showing the relationship between atmospheric gas capturing rate (kg/s) and time for 3He capturing (days) along with hydrogen production requirements.
Aerospacecraft (ASC) as an Observational Unmanned Aerial Vehicle (UAV) (1/2)

• In the 2014 AMOSS studies, a series of UAVs for data gathering near atmospheric phenomena was suggested.

• While the UAV idea is attractive, the size of many of the storms may make data gathering in the atmosphere an arduous task.

• Orbital monitoring, as with Earth observing satellite may be the key.

• If very long term in-situ operations are needed with a UAV, perhaps the mining ASC would be the best solution.
Aerospacecraft (ASC) as an Observational Unmanned Aerial Vehicle (UAV) (2/2)

- The ASC has a longer range and the lifetime of its gas core reactor may exceed the solid core reactors.
- The 2014 results implied a reactor lifetime of approximately 30 hours (Refs. 1 and 21).
- Circumnavigating the large planetary storms may require much longer periods of time.
- Uranus and Neptune “geostationary” satellites could provide the needed global weather data and other visual observations.
- After determining the most important science target(s), the ASC derived UAV would do the more detailed measurements, having the ability to loiter in the storm area.
AMOSS Transportation Infrastructure and Implications – Uranus System

- Aerospacecraft (ASC) enter atmosphere and begins mining
- Lander(s) place the ISRU factories on Titania.
- ISRU factory begins oxygen and hydrogen production.
- Lander is fueled with ISRU oxygen and hydrogen.
- Lander is loaded with hydrogen payload for OTV.
- OTV and lander rendezvous, OTV is fueled for round trip mission to Saturn.
- OTV picks up helium 3 from ASC.
- OTV delivers helium 3 to Lander (in Titania orbit).
- Lander refuels OTV and delivers helium 3 to ISRU factory (PPack).
OTV Design and Masses (Initial Mass)

NEP, delta-V = 31.5 km/s (round trip),
Payload and dry mass = 21 MT, Isp = 5,000 s, eta = 0.5

- Alpha = 40
  - Power level (MWe) vs. NEP OTV initial mass (MT)
  - NEP OTV initial mass: 2,320.71 MT
- Alpha = 20
  - Power level (MWe) vs. NEP OTV initial mass (MT)
  - NEP OTV initial mass: 1,560.44 MT
- Alpha = 10
  - Power level (MWe) vs. NEP OTV initial mass (MT)
  - NEP OTV initial mass: 610.11 MT
OTV Design and Masses (Propellant Mass)

NEP, delta-V = 31.5 km/s (round trip), Payload and dry mass = 21 MT, Isp = 5,000 s, eta = 0.5

- Alpha = 40: 1,099.71
- Alpha = 20: 739.44
- Alpha = 10: 289.11

Power level (MWe)

NEP OTV propellant mass (MT)

0 10 20 30 40
OTV Design and Masses (Trip Time)

NEP, delta-V = 31.5 km/s (round trip),
Payload and dry mass = 21 MT, Isp = 5,000 s, eta = 0.5

NEP OTV trip time (days)

Power level (MWe)

- Alpha = 40: 1,055.86, 303.47
- Alpha = 20: 1,029.53, 277.13
- Alpha = 10: 1,020.75, 268.35
OTV Design and Masses (Lander Payloads)

NEP, delta-V = 31.5 km/s (round trip),
Payload and dry mass = 21 MT, Isp = 5,000 s, eta = 0.5

- Alpha = 40
- Alpha = 20
- Alpha = 10

Number of lander flights
for OTV refueling (50 MT per flight)

Power level (MWe)

0 10 20 30 40

0 5 10 15 20 25

22.00

8.00

6.00

3.00
OTV Design and Masses (Lander Payloads)

NEP, delta-V = 31.5 km/s (round trip),
Payload and dry mass = 21 MT, Isp = 5,000 s, eta = 0.5

Number of lander flights
for OTV refueling (200 MT per flight)

Power level (MWe)

Alpha = 40
Alpha = 20
Alpha = 10
Lander Design and Masses

• The lander’s mission is to deliver hydrogen to the OTV and return to the moon with the helium 3 or deuterium payload(s).
• The round trip delta-V would be 0.8 x 2 or 1.60 km/s.
• This 0.8 km/s delta-V value represents the energy to reach escape conditions from the moon Titania.
• Thus, the lander has the capability to reach escape conditions to rendezvous with the OTV.
• The lander was designed with an oxygen hydrogen main propulsion system.
• The lander Isp was varied from 400 to 480 seconds. The dry mass scaling equation was:
  – \( M_{\text{dry}, \text{stage}} \text{ (kg)} = M_{\text{dry}, \text{coefficient}} \times M_p \text{ (kg)} \)
  – \( M_{\text{dry}, \text{coefficient}} = 0.2 \) and 0.4
ISRU Factory Design and Masses

• The masses of the propellant factories were based on four design options:
  – Lightweight factory (all external storage and processing),
  – Heavy factory (also with external storage and processing),
  – Lightweight factory with propellants fed to the lander,
  – Super lightweight factory, using integral propellant storage on the lander (with no external lander propellant or fluid storage).

• The range of masses were from 7 MT for the super lightweight case (using integral propellant storage on the lander) to 21 MT for the heavy factory.
Preliminary Transportation Optimization (1/4)

• Establishing an optimum transportation system will be influenced by many factors: the OTV mass and power level, the payload mass of the lander and the selection of the moon for the mining factories.

• Several optima will be created based on the size and mass of the moon selected.

• The moon’s mass will strongly influence the propellant mass needed for the refueling of its oxygen/hydrogen propulsion system and the time needed for creating the fuel for the OTV.
Preliminary Transportation Optimization (2/4)

- With the OTVs, the 10 MWe power level appears to be the most acceptable.
- The initial mass of the OTV with power levels of 20 and 30 MWe is too high, with no significant trip time benefits over the OTV at the 10 MWe power level.
- For the 21 MT dry mass case, at 10 kg/kWe, and at 5,000 seconds of Isp, the trip time for the 30 MWe level is 269 days versus 304 days at the 10 MWe level.
- With the 40 kg/kWe case (with the same Isp and dry mass), the trip time at 30 MWe is 1,021 versus 1,056 for the 10 MWe case.
Preliminary Transportation Optimization (3/4)

- The OTV trip times are a significant issue.
- Many flight times are 100’s of days.
- Initially, a single 1 MT payload of helium 3 or deuterium would fly on each OTV flight.
- Multiple helium 3 or deuterium payloads will have to be manifested on the OTVs.
- While the OTV and the lander can rendezvous at the moon’s escape conditions, it may be more stable to conduct the propellant and payload transfers at a high moon orbit, but not at or beyond the moon’s escape conditions.
Preliminary Transportation Optimization (4/4)

- Lander payloads of 200 MT provide the minimal number of lander flights.
- The processing on the moon of the propellant, the propellant loading, and the cryogenic hydrogen payload loading may favor the largest payload capacity lander.
- With the 200 MT hydrogen payload, the number of lander flights needed to refuel the 21 MT dry mass (5,000 seconds Isp) OTV is 1 flight for the 10kg/kWe case and 2 flights for the 40 kg/kWe case.
- Landers might be further optimized by increasing their payload capacity, which would further reduce the number of flights.
Concluding Remarks (1/2)

• Using outer planet moon bases for mining propellants for OTVs and landers is an important option.

• Storing the AMOSS nuclear fuels away from the atmosphere will minimize the potential for unanticipated deorbiting of the orbiting storage facility.

• Using the moons for storage of the nuclear fuels and base of operations for OTV refueling is an excellent option.

• Though the gravity of these moons are much lower than that of Earth, that gravity will likely assist in any processes for mining and fuel processing.
Concluding Remarks (2/2)

- The 10 MWe power levels for the OTV seems best for providing a relatively short trip time.
- The OTVs and landers will rendezvous near the escape condition of the small moon, shortening the trip time for the OTV (eliminating the need to spiral into low moon orbit).
- Larger landers (of 200 MT payloads) are more attractive than small landers, as the large landers require fewer flights to resupply the OTVs with fuel.
- The OTV trip times may be too long for effective use of the more distant moons. Moons that are closer to the planet may be required.
Neptune, Go ISRU
A DAY ON A JUPITER'S MOON
LAST LESS THAN 5 HOURS

JUST LIKE SATURDAY AND SUNDAY ON EARTH
AMOSS Constellation
Atmospheric Exploration Missions (1/2)

• AMOSS helium 3 (3He) mining produces large amounts of additional hydrogen and helium.
• Given the fact that large amounts of hydrogen and helium are available, new missions can be conceived for vehicles in the outer planet atmosphere(s).
• Fleets of such aerospacecraft (ASC) vehicles could be fueled with AMOSS produced hydrogen and helium.
AMOSS Constellation
Atmospheric Exploration Missions (2/2)

• Potential missions include:
  – Aircraft for weather data gathering, weather warnings.
  – Deep diving subsonic “aircraft” probes that can go to low altitudes with 10X, 20X, 30X atmospheric pressures (a la scoopers).
  – Launching of GPS-ish vehicles to improve mining (ASC) communications.
  – Delivery of samples to orbital assets.
## Exploration UAV size ranges

<table>
<thead>
<tr>
<th>Probe design</th>
<th>Mass (MT)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Free fall</td>
<td>1 to 10</td>
</tr>
<tr>
<td>Parachute</td>
<td>1 to 10</td>
</tr>
<tr>
<td>Rocket boost</td>
<td>10 to 100</td>
</tr>
<tr>
<td>Rocket return</td>
<td>10 to 1,000</td>
</tr>
<tr>
<td>Long duration, subsonic</td>
<td>10 to 1,000</td>
</tr>
<tr>
<td>Aerospacecraft (mining)</td>
<td>100 to 10,000</td>
</tr>
</tbody>
</table>
UAV Configurations: High Speed (4a/4)

Nuclear Ramjet Flyer
Figure 8. LODAA Predictions for a Blended Body Shape
UAV Configurations: High Speed (4c/4)

AMOSS: UAV; 10 km/s delta-V, Mtank = 0.1 Mp

![Graph showing UAV mass, initial mass, final mass, and dry mass, without tankage. The graph includes initial and final markers.](image)
Uranus – Outer Planet Atmospheres and Wind Speeds

Sromovsky, L., 2010, Investigating Atmospheric Change on Uranus and Neptune, Award number NNG05GF00G.
UAV Mission Planning: Weather Phenomena, Uranus

Uranus atmospheric phenomena (Reference 24)
UAV Mission Planning: Aurora Phenomena, Uranus

Uranus atmospheric phenomena (Reference 23)
UAV Configurations: Weather (3a/4)

Figure B3. Neptune cloud features (Voyager, Hubble, Ref. 27)
UAV Mission Planning: Weather Phenomena: Neptune

Neptune atmospheric phenomena (Reference 26)
AMOSS UAV Mission Profiles
(Multiple Targets Assessed, One Way)
AMOSS UAV Mission Profiles
(Multiple Targets Assessed, Round Trip)
AMOSS UAV Mission Profiles
(Multiple Targets Assessed, Two Hemispheres, One Way)
AMOSS UAV Mission Profiles
(Multiple Targets Assessed, Two Hemispheres, Round Trip)
Travel Time Across Planet: Uranus

UAV travel time: Uranus

Travel time (hours)

UAV velocity (m/s)

Degrees travelled
Travel Time Across Planet: Neptune

UAV travel time: Neptune

Travel time (hours)

UAV velocity (m/s)

Degrees traveled

- 100.0-120.0
- 80.0-100.0
- 60.0-80.0
- 40.0-60.0
- 20.0-40.0
- 0.0-20.0
Time for Storm Circumnavigation

Time for circumnavigation of outer planet atmospheric storms, standoff distance = 100 km

Circumnavigation time (minutes)

Fraction of Earth’s radius

UAV flight speed (m/s)

- 50
- 100
- 200
- 300
Resource Capturing – Observations (1/2)

- Helium 3 is the primary gas for capturing by aerospacecraft cruisers.
- While capturing helium 3, the cruiser also has the potential for capturing very large amounts of hydrogen and helium 4 (which comprise nearly 100% of the atmosphere).
- Resource capturing of hydrogen and helium 4 can lead to fueling fleets of smaller but specialized exploration and exploitation vehicles.
- New concepts for weather monitoring, cloud exploration, and deep-diving aircraft fueled by these large resources are possible.
Resource Capturing – Observations (2/2)

• Uninhabited Aerial Vehicle (UAV) and drone options may use nuclear ramjets or rockets.
• Sampling of the atmosphere and investigation of short- and long-term storm and weather related phenomena are options.
• Mission planning could allow for surveying many targets per UAV flight.
• Nuclear thermal propulsion reactor life may limit nuclear ramjet based aircraft to less than 40 hours.
• Rocket vehicles that deliver the ramjets to storm locations may allow for rapid responses to unique storms and other phenomena.
Concluding Remarks

• Atmospheric mining can open new frontiers.
• Gas core engines can reduce the vehicle initial mass by 72% to 80% over solid core NTP powered vehicles.
• AMOSS helium 3 capturing leads to processing huge amounts of gas for powering unique UAVs and atmospheric missions.
• Nuclear thermal propulsion reactor life may limit nuclear ramjet aircraft to less than 40 hours of operation.
• Rocket vehicles that deliver the ramjets vehicles to storm locations may allow for rapid responses to unique atmospheric phenomena.
• Let’s go to the stars, as quickly as possible.