Abstract Submitted: The NASA Orion Crew Module Reference Design was produced to address large scale thermal runaway (TR) hazard with specific safety controls for the Orion Spacecraft. The design presented provides the description of a full scale battery design reference for implementation as a drop in replacement to meet all spacecraft energy requirements with compatible 120 Vdc electrical and mechanical interface using small cell technology (18650) packaging. The 32V SuperBrick incorporates unique support features and an electrical bus bar arrangement that allows cells negative can insertion into heat sink that is compressively coupled to the battery enclosure to promote good thermal management. The housing design also provides an internal flame suppression “filter tray” and positive venting path internal to the enclosure to allow hot effluent ejecta to escape in the event of single cell TR. Virtual cells (14P Banks) that are supported to provide cell spacing with interstitial materials to prevent side can failures that can produce cell to cell TR propagation. These features were successfully tested in four separate TR run with the full scale DTA1 test article in February 2016. Successfully Completed Test Objectives - Four separate TR test runs with Full-Scale DTA1 housing with Two SuperBricks, Two SuperBrick Emulators All Tests resulted in “clean” gas with less than 6°C rise at Battery vent All Tests resulted in less than 2°C temperature rise on cold-plate outlet All Tests resulted in less than 6 psi pressure rise in the battery housing Test Run 1 – One neighbor cell TR, highest remaining neighbor 139°C. Ejecta shorted to bus caused prolonged additional heating, One shorted cell did experience TR after 12 minutes, remaining cells had adequate thermal margin Test Run 2 – No cell to cell propagation, highest neighbor cell 112°C; Test Run 3 – No cell to cell propagation, highest neighbor cell 96°C; Test Run 4 – No cell to cell propagation, highest neighbor cell 101°C; Primary TR testing and analysis were completed and reviewed for endorsement by NASA Engineering and Safety Center team members. All Key Test Objectives were met and the small cell design alternative was demonstrated and selected to be a feasible drop in replacement for the MPCV Orion CM Battery for EM2 mission.
NASA Alternative Orion Small Cell Battery Design Support
November 16, 2016

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CM Battery On-Ramp Decision for EM-2
Background

- MPCV Orion proposed design for CM Battery that would put in place specific controls to prevent thermal run-away (TR) propagation after a single cell TR event and thereby avoid a large scale fire/explosive hazard, and eliminate potentially cascading concerns to the ATCS cooling loop and other Spacecraft systems.

- NASA JSC Power and Wiring was authorized by MPCV APS IPT to perform development of a small cell battery as an alternative, with the intent to demonstrate fail safe features that would preclude TR propagation without impact to Spacecraft systems.

- NASA performed a first set of feasibility tests in early 2015 that showed enough promise and interest to gain collaborative funding from the Orion Program and the NESC to perform further development and testing approaching flight-like design.

- The Orion Small Cell Battery (OSCB) Development Test Article phase 1 (DTA1) project team analyzed, designed, built and completed testing of the DTA1 full-scale hardware.

- A summary of the OSCB DTA1 project results were provided to the Orion Program, as a design reference for an inherently safe small cell battery design for EM2.

- OSCB DTA phase 2 DTA2 updated design and development tests were funded in FY16 to further design and perform Struct & Mech environmental testing to support PDR readiness.
CMB Large Cell TR Propagation Testing

- Thermal runaway tests performed in Sept 2014 demonstrated that single cell TR ruptures burst disc and causes venting, and propagates to neighboring cells
  - Flight type battery case, populated with 14 of 32 cells
  - Single cell forced into TR
  - TR propagated to all cells in affected bay, base case temperatures exceed 300deg C, Flame through burst disk
Above Video Feb 24 2015 Test Orion Small Cell Battery shows Five independently heater triggered cells in Proto-case housing (left frame) compared side by side with Sept 2014 CMB Large Cell TR propagation with single cell overcharge trigger,

Above Video June 2015 Test Orion Small Cell Battery TR Propagation Proto-case run #9 used to successfully demonstrate Gore Vent approach Small Cell Battery Safety demo notes: Runs 1-6 Performed in succession no TR propagation Run 7 Resulted in TR propagation Most likely Causes Identified: • side can failure mode direct flame impingement • over-test due to collateral damage from 6 prior events • unfairly biasing neighbor cell temperature with slow heater Run 8 TR recreating Run 7 conditions but with insulating foam and resulted in no propagation
Battery SuperBrick Packaging
14P- Virtual Cell Sub-block Components (DTA1 shown)

- UPPER CAPTURE PLATE
  - G10 FR4 FIBERGLASS COMP

- 14X Panasonic NCR 18650B CELLS

- SYNTACTIC FOAM LINER

- LOWER HEAT-SINK CAPTURE PLATE
  - 6061-T651 ALUM

- 304 Stainless Steel Sleeve – 9 mil wall thickness

- MACOR VENT TUBES
Battery SuperBrick Packaging
112-Cell Outer Dimensions: 10.04” x 8.58” x 2.82”

- Lower Frame: G10 FR4 fiberglass composite
- Upper Frame: 6061-T651 alum, hard anodized
- 15X Standoff Supports
- 20 ga nickel bus plates
BUS PLATE ROUTING

NEGATIVE BUS TERMINATION

POSITIVE BUS TERMINATION
Small Cell Crew Module Battery Development Test Article 2 Design Demonstration Abort Vibration and PyroShock Testing – SuperBrick Battery Component

Project Management:
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DTA1 Full-Scale Housing Internal Construction

Gore Vent apparatus allows for pressure management with hydrophobic features to prevent water intrusion. Underneath the Gore Vent there is a layer of Nextel AF14 for enhanced effluent particulate suppression.

Upper Battery volume utilized for mounting electronics and wire harness routing and provides void volume air exchange.

Filter plate in top tray provides vent path from lower battery compartment to upper battery volume. Filter materials are sandwiched between plate and include metal mesh (30 Monel) and Nextel Fabric (AF-14) for flame suppression and heat spreading.

Tie Rods 15x provide SuperBrick mechanical mounting for thermal gap compression.

Housing base for cold-plate mounting of the CM Battery is constructed with vertical ½" thick thermal path for SuperBrick attachment as a single piece of Aluminum.
Side housing is constructed of a single piece of aluminum to form the exterior walls and interior partition between SuperBricks.

Gore Vent apparatus external cover vent port holes 12x provide box pressure management.
DTA1 Full-Scale Housing with SuperBrick

14P-8S 32V Superbrick
DTA1 Full-Scale Housing (CAD & As-Built)
Two live 32Vdc SuperBricks along with Two emulator bricks were installed a full Scale DTA1 housing, connectors not shown but are used to transmit instrumentation signals during the test.

SuperBrick 1
- Superbrick Positive Terminal
- Superbrick Neg Terminal
- Bank 1
- Bank 2
- Bank 3
- Bank 4
- Bank 5
- Bank 6
- Bank 7

SuperBrick 2
- Superbrick Positive Terminal
- Superbrick Neg Terminal
- Bank 1
- Bank 2
- Bank 3
- Bank 4
- Bank 5
- Bank 6
- Bank 7

SuperBrick Positive
- Trigger Cell Location
- Cell TC Location
- TC On the Negative Capture Plate
Test article installed on the cold plate in the test cell and checked out with instrumentation system

SuperBrick Negative power legs were grounded to chassis
Orion Small Cell DTA  14P Sub-block Heater Triggered
February 2016 DTA1 Full-Scale Housing TR Test Run 2

DTA1 TR Test Run 2 - Feb 10, 2016

- Cold Plate Inlet & Outlet
- Trigger Cell
- Vent Air Probes Temps Did not go above 38°C
- Battery and Bank 6 voltages largely unchanged
- Maximum neighbor cell temperature

Time Sec

Temp Deg C
Orion Small Cell DTA - 14P Sub-block Heater Triggered
February 2016 DTA1 Full-Scale Housing TR Test Run 4

Cold Plate Inlet (TC37) & Outlet (TC43) do not go above 41 deg C

SuperBrick 2 Bank 4 Cell 7 Trigger Cell

Vent Air Probes Temps Did not go above 37C

Battery and Bank 4 voltages unchanged

Maximum neighbor cell temperature Bank 4 Cell 3 101 deg C

Bank 4 Negative Capture Plate 72 deg C
Orion Small Cell DTA 14P Sub-block Heater Triggered
February 2016 DTA1 Full-Scale Housing TR Test Run 3

DTA1 TR Test Run 3 - Feb 10, 2016

- Bank 8 cell 2 TC disconnected
- Bank 8 Cell 1 Trigger Cell
- Cold Plate Inlet & Outlet outlet does not climb above inlet temp
- Vent Air Probes Temps Did not go above 37C
- Bank 8 Negative Capture Plate
- Battery and Bank 8 voltages unchanged
- Maximum neighbor cell temperature Bank 8 Cell 6
  IsoTC21, 96.00293
Orion Small Cell DTA 14P Sub-block Heater Triggered February 2016 DTA1 Full-Scale Housing TR Test Run 1

DTA1 TR Test Run 1 - Feb 9, 2016

- Trigger Cell
- 2nd TR about 12 minutes after Trigger Cell on Bank 8 Cell 6
- Cold Plate Inlet & Outlet Stayed below 41°C
- Vent Air Probes Temps Did not go above 41°C
- Bank 8 Volts PTCs engaged
- Bank 8 Cell 2
- Bank 8 Cell 10
- Bank 8 Negative Capture Plate
- Trigger Cell Bank 8 Cell 1
- Bank 8 Volts scaled up X100

Legend:
- l2
- IsoTC1
- IsoTC2
- IsoTC3
- IsoTC15
- IsoTC16
- V12X100
- V2
- V12
- V18
- V19
- V20
- V21
- IsoTC37
- IsoTC43
- IsoTC52
- IsoTC53
- IsoTC54
Orion Small Cell SuperBrick Heater Trigger Method
February 2016 DTA1 Full-Scale Housing TR Test

• Successfully Completed Test Objectives - Four separate TR test runs with Full-Scale DTA1 housing with Two SuperBricks, Two SuperBrick Emulators
  – All Tests resulted in “clean” gas with less than 6°C rise at Battery vent
  – All Tests resulted in less than 2°C temperature rise on cold-plate outlet
  – All Tests resulted in less than 6 psi pressure rise in the battery housing
  – Test Run 1 – One neighbor cell TR, highest remaining neighbor 139°C.
    • Ejecta shorted to bus caused prolonged additional heating, One shorted cell did experience TR after 12 minutes, remaining cells had adequate thermal margin
    • Fuse design improvement will address isolating this electrical fault
  – Test Run 2 – No cell to cell propagation, highest neighbor cell 112°C;
  – Test Run 3 – No cell to cell propagation, highest neighbor cell 96°C;
  – Test Run 4 – No cell to cell propagation, highest neighbor cell 101°C;

✓ Thermal Runaway events were all completely contained within the battery and demonstrated to have no impact to other spacecraft systems.

✓ Thermal Management design demonstrated control of TR propagation.
Minor collateral damage observed, particulates and flame remained internal to battery enclosure.
Summary - Orion Small Cell Battery (OSCB) Development Test Article 1 (DTA1)
Primary Development and Key Test Objectives Completed

Developed and built an OSCB DTA1 full-scale test article with NESC resources supporting technical design guidance and funding test events:

✔ Demonstrate Structural and mechanical design and battery internal cell packaging has the ability to interface within the Spacecraft existing CM Battery mass, footprint and overall volumetric constraints in the AFT Bay

✔ Demonstrate Candidate Cell quality can meet established Orion EMx CM Battery CT-Scan DPA cell quality requirements for reducing the risk of FOD, defects, contamination causing a TR event

✔ Demonstrate electrical performance can meet power, energy and electrical impedance requirements

✔ Demonstrate thermal management performance has the ability to meet normal and non-normal (TR) temperature regulation requirements without impact to the ATCS cold-plate interface

✔ Demonstrate that vented effluent remains below explosive limits in the Aft – Bay and would be acceptable to Safety

✔ Demonstrate that the housing ventilation, flame and heat suppression features work to prevent flame and contain significant heat from leaving the battery housing with satisfactory pressure management

✔ Demonstrate the combined internal battery features for cell thermal management, physical separation, effective venting, electrical isolation and structural support work to preclude a single cell TR side wall failure from directly impinging flame onto a neighbor cell and that single cell TR will not thermally propagate to remaining cells internal to the battery

✔ Primary TR testing and analysis were completed and reviewed for endorsement by NASA Engineering and Safety Center team members.

✔ All Key Test Objects were met and a small cell design was demonstrated to be a feasible drop in replacement for the MPCV Orion CM Battery for EM2 without the need for an overboard vent.

✔ MPCV Orion Program Manager directed Prime to change the Crew Module Battery Baseline from the EM1 Large Cell Design to the NASA Small Cell Battery Reference Design for EM2
DTA2 Battery Build and Environmental Tests

- Addressed Key Technical Risk Areas (agreed by LM, JSC Engineering and NESC)
  - Shorting of Jelly Roll - to be addressed Nickel Bus Fuse Update/testing and high dielectric surface coating evaluation – Completed Design
    • Completed Design to relocate fuse to isolate on Negative of cell bank
    • Completed adding surface coating to the heat sink
    • Bus Bar protection for fuse blow isolation: Conformal coating vs Al Oxide paint, application testing In Work
  - Corner Cell Side Can Rupture - design robustness to be addressed by Improved 14P Bank Corner Cell Support and Alternative Cell Evaluation – Completed Design
    • Updated design to include thicker sleeves (9 mil to 13 mil)
    • Updates to cell bank heat sink to provide increased thermal contact at base of each cell
    • Introduced LG MJ1 as alternative cell for design with thicker can wall and lower crimped header burst pressure

- Thermal runaway regression testing of alternate cells in updated DTA2 Sub-block configuration
  - Sub-block Heat To Vent Testing.

- Primary Risk to Address for Orion abort vibe and shock environments,
  - Validate Housing and SuperBrick Structural and Mechanical design by test
  - Validate SuperBrick Part Structural Robustness for abort vibe and shock by test
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MPCV Orion Small Cell Battery Project Team

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