Advanced Environmental Barrier Coating Development for SiC/SiC Ceramic Matrix Composites: NASA’s Perspectives

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Praxair Surface Technologies – John Anderson and Li Li
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in supporting the coating processing

Engine OEM Companies including GE Aviation, Rolls Royce (Kang Lee), Honeywell, Pratt & Whitney
Outline

— Environmental barrier coating system development: NASA’s perspectives

— Environmental barrier coating system development: challenges and limitations
  • Thermomechanical, environment and thermochemical stability issues
  • Prime-reliant EBCs for CMCs, a turbine engine design requirement

— Advanced environmental barrier coating systems (EBCs) for CMC airfoils and combustors
  • NASA EBC systems and material system evolutions
  • Current turbine and combustor EBC coating emphases
  • Advanced EBC development: processing, testing and durability

— Design tool and life prediction perspectives of coated CMC components

— Advanced CMC-EBC performance demonstrations
  • Fatigue – Combustion and CMAS environment durability
  • Component demonstrations

— Summary and future directions
NASA Environmental barrier coatings (EBCs) development objectives

- Help achieve future engine temperature and performance goals
- Ensure system durability – towards prime reliant coatings
- Establish database, design tools and coating lifing methodologies
- Improve technology readiness

Durable Environmental Barrier Coating Systems for Ceramic Matrix Composites (CMCs):
Enabling Technology for Next Generation Low Emission, High Efficiency and Light-Weight Propulsion

Fixed Wing Subsonic Aircraft
Supersonics Aircraft
**NASA Environmental Barrier Coating Development Goals**

- Emphasize temperature capability, performance and durability
- Develop innovative coating technologies and life prediction approaches
- 2700°F (1482°C) EBC bond coat technology for supporting next generation
- 2700-3000°F (1482-1650°C) turbine and CMC combustor coatings
  - Meet 1000 h for subsonic aircraft and 9,000 h for supersonics/high speed aircraft hot-time life requirements

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**Temperature Capability**

- 2800°F combustor TBC
- 2500°F Turbine TBC

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**Single Crystal Superalloy**

**Increase in ΔT across T/EBC**

- 2700°F (1482°C)
  - 3000°F (1650°C+): 3000°F SiC/SiC CMC airfoil and combustor technologies
  - 2700°F SiC/SiC thin turbine EBC systems for CMC airfoils

- 2400°F (1316°C): Gen I and Gen II SiC/SiC CMCs

- 2000°F (1093°C)

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**Ceramic Matrix Composite**

**Gen I** – Current commercial

**Gen II**

**Gen III**

**Gen IV**

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* Recession: <5 mg/cm² per 1000 hr (40-50 atm., Mach 1~2)
** Component strength and toughness requirements
NASA EBC Technology Development - Retrospectives
- Also Supported Other National SiC/SiC CMC and Si-base Ceramic Development Programs

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<th>FY99</th>
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<td>NASA - EPM 2300 - 2400 F EBC (TRL of 3)</td>
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<td>NASA- UEET-2700°F EBC Development, NASA 3000°F Multifunctional T/EBC Development New Compositions, SiC/SiC Vane, Cooled Si₃N₄ Vane (TRL of 4)</td>
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<td>NASA Steam Rig Testing High Pressure Burner Rig, Atm. Burner rig, Laser, Furnace (TRL of 5)</td>
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<td>DOE - EBC Improvements (TRL of 4-5)</td>
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<td>DOE - Field Tests (TRL of 6 and higher)</td>
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0 3100°F CMC vane testing
1 Si₃N₄ vane HPBR test
2 3000°F CMC demonstration

DoD-IHPTET Core and Engine Test (TRL of 6) - DUST
DoD - Honeywell, Rolls Royce, GE components (TRL 6)
NASA Supersonics Turbine Engine CMC Thin Blade Coating Development (TRL-2 to 5)
NASA Turbine Environmental Barrier Coating Development: Major Accomplishments and Emphases

**Advanced EBCs**
- Durable CMC w/EBC developed - 2700F turbine coating for 2400°F CMC
- Demo EBC for CMC subelement
- Develop creep resistant turbine EBC with advanced 2700°F bond coats
- Impingement & Film cooled recession
- Turbine EBC on CMC blade subcomponents
- **Initial environment and fatigue interactions**
- Develop Life Models for EBC on CMC blade
- Rig Demo Optimized 3D EBC-CMC blades

**CMC Development Supporting Advanced EBC-CMC Development**
- 2.5D CVI CMC rig demo
- 3D CVI/MI Architecture Airfoil
- Develop advanced architecture hollow CMC blade subelements

**EBC/CMC Component Development Program – NASA ERA Program**
- 2700°F turbine EBC on 2400-2500°F CMC turbine vanes Rig Demo (TRL 4-5)
- 2700°F Combustor EBC on 2400°F CMC Combustor – Rig Demo 250 hr (TRL 4-5)
- Develop Life Models for EBC on CMC blade
- 2700°F EBC-Advanced architecture hollow CMC blade subelements

**Turbine TBC Erosion/CMAS (in collaboration with DOE and Air Force, Army, Navy)**
- 2X Erosion resistant turbine TBC
- Luminance sensing TBC
- Advanced CMAS Resistant TBC
- Advanced CMAS Resistant Turbine Coating Rig Demo
## NASA Turbine Environmental Barrier Coating
### Development: Advanced Systems

#### Turbine and combustor EBCs

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<tr>
<th>Combustor Liner (medium heat flux)</th>
<th>HPT Vane (high heat flux)</th>
<th>HPT Blade (very high heat flux)</th>
<th>LPT Blade (low heat flux)</th>
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<tr>
<td><strong>Gen II CMC</strong></td>
<td><strong>2400 °F CMC, cooled, 2700 °F ** <strong>thick</strong> EBC (ERA)</strong></td>
<td><strong>2400 F CMC, cooled, 2700 °F ** <strong>thin</strong> EBC (ERA)</strong></td>
<td><strong>2400 °F CMC, cooled, 2400-2700 °F ** <strong>thin</strong> EBC</strong></td>
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<td><strong>Gen III CMC – Option 1</strong></td>
<td><strong>2700 °F CMC, uncooled, 2700 °F ** <strong>thick</strong> EBC (ERA + FAP)</strong></td>
<td><strong>2700 F CMC, uncooled, 2700 °F ** <strong>thin</strong> EBC</strong></td>
<td><strong>2400 °F CMC, uncooled, 2400 °F ** <strong>thin</strong> EBC</strong></td>
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<td><strong>Gen III CMC – Option 2</strong></td>
<td><strong>2700 °F CMC, cooled, 3000 °F ** <strong>thick</strong> EBC (ERA + FAP)</strong></td>
<td><strong>2700 °F CMC, cooled, 3000 °F ** <strong>thin</strong> EBC</strong></td>
<td><strong>2700 °F CMC, uncooled, 2700 °F ** <strong>thin</strong> EBC</strong></td>
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Environmental Barrier Coating Development: Challenges and Limitations

- Current EBCs limited in their temperature capability, water vapor stability and long-term durability, especially for advanced high pressure, high bypass turbine engines

- Advanced EBCs also require higher strength and toughness
  - In particular, resistance to combined high-heat-flux, engine high pressure, combustion environment, creep-fatigue, loading interactions

- EBCs need improved erosion, impact and calcium-magnesium-alumino-silicate (CMAS) resistance and interface stability
  - Critical to reduce the EBC Si/SiO\textsubscript{2} reactivity and their concentration tolerance

- EBC-CMC systems need advanced processing for realizing complex coating compositions, architectures and thin turbine configurations for next generation high performance engines
  - Advanced high temperature processing of high stability nano-composites using advanced Plasma Spray, Plasma Spray - Physical Vapor Deposition, EB-PVD and Directed Vapor EB-PVD, and Polymer Derived Coating processing
  - Economical
Fundamental Recession Issues of CMCs and EBCs

- Recession of Si-based Ceramics
  (a) Convective; (b) Convective with film-cooling
  - Low SiO$_2$ activity EBC system development emphasis
- Advanced rig testing and modeling
  More complex recession behavior of CMC and EBCs in High Pressure Burner Rig

Recession rate = const. $V^{1/2} \frac{P_{(H2O)}^2}{(P_{total})^{1/2}}$

Recession of SiO$_2$-based Ceramics

Combustion gas

SiO$_2$ + 2H$_2$O(g) = Si(OH)$_4$(g)

Cooling gas

(a)

(b)
Fundamental Recession Issues of CMCs and EBCs - Continued

Weight Loss of SiC in High Pressure Burner Rig
6 atm 20 m/s

- Early generations of environmental barrier coatings - EBC systems

Robinson and Smialek, J. Am. Ceram Soc. 1999

Combustor coating
Turbine coating

HfO$_2$ based low k - APS
HfO$_2$ based low k - EB-PVD
Environmental Stability of Selected Environmental Barrier Coatings Demonstrated in NASA High Pressure Burner Rig

- EBC stability evaluated on SiC/SiC CMCs in high velocity, high pressure burner rig environment
- More stable turbine coatings developed under NASA programs
- HfO\(_2\)-Rare Earth (RE) silicate-based coatings showed significantly improved stability and durability

Stability and temperature capability improvements through coating composition and architecture innovations

Specific weight change, mg/cm\(^2\)-h vs. 1/T, K\(^{-1}\)

Gas pressure 6 atm
Gas velocity 30m/s
Gas velocity 200m/s

Stability of selected coatings systems
EBC Bond Coat: Degradation Mechanisms for Current State of the Art Silicon Bond Coat

- Silicon bond coat melts at 1410°C (melting point)
- Fast oxidation rates (forming SiO₂) and high volatility at high temperature
- Low toughness at room temperature (0.8-0.9 MPa m¹/²; Brittle to Ductile Transition Temperature about 750°C)
- Low strength and high creep rates at high temperatures, leading to coating delamination
- Interface reactions leading to low melting phases
  - A significant issue when sand deposit Calcium- Magnesium – Alumino-Siliacte (CMAS) is present
- Si and SiO₂ volatility at high temperature (with and without moisture)

Brittle to Ductile transition in polycrystalline Si
Degradation Mechanisms for Si Bond Coat – Interface reactions

- Significant interfacial pores and eutectic phases formation due to the water vapor attack and Si diffusion at 1300°C
- Heat flux condition further limit the use temperatures

**SEM images** Interface reactions at 1300°C; total 200 hot hours

**BaO-Al2O3-SiO2 ternary phase diagram**

Si bond coat after 1350°C, 50 hr furnace test in air; 1” dia plasma sprayed EBC button specimen

Hot pressed BSAS+Si button specimen after 1350°C, 50 hr furnace test in air

Interface Si bond coat melting of selected coating systems, under laser heat flux tests, 1” dia button specimen
Degradation Mechanisms for Si Bond Coat – Interface reactions

- Continued

- Significant interfacial pores and eutectic phases formation due to the water vapor attack and Si diffusion at 1300°C

- Heat flux condition further limits the use temperatures

![Graph showing cycles to failure vs. interface temperature.]

Delamination of EBC under heat flux test

Two layer ytterbium mono- and di-silicates

YSZ

Mullite

Mullite+BSAS

Si

Biaxial heat flux tested ytterbium silicate / Si EBC: surface cracking and interface reaction
Advanced EBC Developments

- Fundamental studies of environmental barrier coating materials and coating systems, stability, temperature limits and failure mechanisms

- Focus on high performance and improving technology readiness levels (TRL), high stability HfO\(_2\) and ZrO\(_2\) -RE\(_2\)O\(_3\)-SiO\(_2\)/RE\(_2\)Si\(_{2-x}\)O\(_{7-2x}\) environmental barrier systems
  - More advanced composition and composite EBC systems focusing temperature capability, strength and toughness

- Advanced HfO\(_2\)-Si and Rare Earth-Silicon based EBC bond coat systems
  - Develop HfO\(_2\)-Si based + X (dopants) and more advanced bond coat systems for 1482°F (2700°F)+ long term applications
  - Develop prime-reliant Rare Earth (RE)-Si systems for advanced integrated EBC-bond coat systems, improving bond coat temperature capability and reducing silicon/silica-rich phase separations

- Processing optimization for improved composition control and process robustness
Evolution of NASA EBC Technology for SiC/SiC Ceramic Matrix Composites: Current State of the Art

— Major development milestones:

• 1995-2000: BSAS/Mullite+BSAS/Si

• 2000-2004: \( \text{RE}_2\text{Si}_2\text{O}_7 \) or \( \text{RE}_2\text{SiO}_5/\text{BSAS}+\text{Mullite}/\text{Si} \)

• 2000-2004 - 3000°F EBC systems: HfO\(_2\) systems (HfO\(_2\) version four-component low k – no silicon containing) / \( \text{RE}_2\text{Si}_2\text{O}_7 \) or \( \text{RE}_2\text{SiO}_5 / \text{BSAS}+\text{Mullite}/\text{Si} \) and Oxide+Si bond coats; component demonstrations
  – Modified mullite (with transition metal and RE dopants) to replace BSAS+mullite
  – Many compound oxide top coat materials explored

• 2005-2011 - Turbine coating systems: Multi-component, graded HfO\(_2\)-Rare Earth Oxide-SiO\(_2\)/ multi-component Rare earth Silicate/ HfO\(_2\)-Si systems
  – \( \text{RE-HfO}_2\text{-X/Multicomponent RE-silicate} / \text{HfO}_2\text{-Si} +\text{X} \) (doped)

• 2009-present: Improved EBC compositions; RE-Si bond coats
  – e.g., \((\text{Gd,Yb,Y})\text{Si} \) bond coat and top coat
# Evolution of NASA EBC Technology for SiC/SiC Ceramic Matrix Composites: Current State of the Art

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<tr>
<td>Top Coat:</td>
<td>BSAS (APS)</td>
<td>RE$_2$Si$_2$O$_7$ or RE$_2$SiO$_5$ (APS)</td>
<td>- (Hf,Yb,Gd,Y)$_2$O$_3$ - ZrO$_2$/HfO$_2$+RE silicates - ZrO$_2$/HfO$_2$+BSAS (APS and EB-PVD)</td>
<td>RE-HfO$_2$-Alumino silicate (APS and/or 100% EB-PVD)</td>
<td>RE-HfO$_2$-X advanced top coat RE-HfO$_2$-graded Silica (EB-PVD)</td>
<td>Advanced EBC</td>
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<td>Interlayer:</td>
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<td>RE-HfO$_2$/ZrO$_2$-aluminosilicate layered systems</td>
<td>Nanocomposite graded oxide/silicate</td>
<td>Gen IV interlayer not required (optional)</td>
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<tr>
<td>EBC:</td>
<td>Mullite+ BSAS</td>
<td>BSAS+Mullite</td>
<td>RE silicates or RE-Hf mullite</td>
<td>RE doped mullite-HfO$_2$ or RE silicates</td>
<td>Multi-component RE silicate systems</td>
<td>Multicomponent RE-silicate /self grown</td>
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<tr>
<td>Bond Coat:</td>
<td>Si</td>
<td>Si</td>
<td>Oxide+Si bond coat</td>
<td>HfO$_2$-Si-X, doped mullite/Si SiC nanotube</td>
<td>Optimized Gen IV HfO$_2$-Si-X bond coat 2700°F bond coats</td>
<td>RE-Si+X systems</td>
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<tr>
<td>Thickness</td>
<td>10-15 mil</td>
<td>10-15 mil</td>
<td>15-20 mil</td>
<td>10 mil</td>
<td>5 mil</td>
<td>1 - 3 mils</td>
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<td>Surface T:</td>
<td>Up to 2400°F</td>
<td>2400°F</td>
<td>3000°F/2400CMC</td>
<td>2700°F/2400F CMC</td>
<td>3000°F</td>
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<td>Bond Coat T:</td>
<td>Limited to 2462°F</td>
<td>Limit to 2462°F</td>
<td>Limit to 2642°F</td>
<td>Proven at 2600°F +; Advancements targeting 2700°F</td>
<td>2700°F (2011 Goal)</td>
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**Challenges overcome by advancements:**

- Improved temperature capability, sintering phase stability, recession resistance, and high temperature strength
- Advanced compositions & processing for combined thermomechanical loading and environments, higher stability and increased toughness towards prime-reliant
NASA EBC Processing Developments for SiC/SiC Ceramic Matrix Composites

- Develop processing capabilities, experience and demonstrate feasibilities in various techniques: air plasma spray, Electron Beam - Physical Vapor Deposition (EB-PVD), Plasma Sprayed-Physical Vapor Deposition (PS-PVD)

- Efforts in developing turbine EBC coatings with Directed Vapor Technologies using Directed Vapor EB-PVD: Turbine Airfoils
- NASA APS, and Triplex Pro APS (with Sulzer/Oerlikon Metco) - for Combustor applications
- Cathodic arc and Magnetron PVD processes: bond coat developments
- NASA PS-PVD
- Some planned EBCs DVM/DVC coatings (with Praxair): aiming at combustor EBC

- Other processing techniques such as Polymer Derived Coating composite coatings (Ceramtec), and laser processing for improved stability
Air Plasma Spray Processing of Environmental Barrier Coatings for Combustor Liner Components

— Focused on advanced composition and processing developments using state-of-the-art techniques

— Improved processing envelopes using high power and higher velocity, graded systems processing for advanced TEBCs and thermal protection systems
Development and Processing of Directed Vapor Electron Beam - Physical Vapor Deposition (EB-PVD)

- NASA programs in supporting processing developments and improvements with Directed Vapor Technologies International, Inc.
  - Multicomponent thermal and environmental barrier coating vapor processing developments
  - High toughness turbine coatings
  - Affordable manufacture of environmental barrier coatings for turbine components

Advanced multi-component and multilayer turbine EBC systems

Directed Vapor Processing systems

Processed EBC system
Plasma Sprayed-Physical Vapor Deposition (PS-PVD)
Processing of Environmental Barrier Coatings

- NASA PS-PVD and PS-TF coating processing using Sulzer newly developed technology
  - High flexibility coating processing – PVD - splat coating processing at low pressure (at ~1 torr)
  - High velocity vapor, non line-of-sight coating processing for complex-shape components
  - Significant progress made in processing the advanced EBC and bond coats

100 kW power, 1 torr operation pressure

NASA PS-PVD coater system

Processed coating systems
Advanced EBC Coating Material Strength Evaluations

- EBC and bond coat constituents are designed with high strength and high toughness to improve coating durability
  - Advanced EBC 150-200 MPa strength achieved at high temperature
  - Multicomponent silicates showed excellent high temperature properties
  - Toughness 3-4 MPa m\(^{1/2}\) also achieved (tested at room temperature)

- HfO\(_2\)-Si based systems showed promising strength and toughness

- More advanced bond coats showed higher temperature capabilities and improved strength
Developing 3000°F (1650°C) EBCs

- NASA Hybrid 3000°F EBC system (2007 R&D 100 Award)

  Highlighted coating material systems:
  - High stability multicomponent HfO₂ Top Coat (Patented Hf-RE-SiO₂ systems)
  - Graded and Layer graded interlayers
  - Advanced HfO₂-Rare Earth-Alumino-Silicate EBC (tetragonal t’ ZrO₂ toughened rare earth silicate EBC)
  - Ceramic HfO₂-Si composite bond coat capable up to 2700°F

Multicomponent Rare Earth (RE) doped HfO₂
(HfO₂-11Y₂O₃-2.5Gd₂O₃-2.5Yb₂O₃)

Strain tolerant interlayer
HfO₂-Rare Earth-Alumino-Silicate EBC

HfO₂-Si or RE modified mullite bond coat
Advanced HfO$_2$-Si+X Bond Coats

- Coating architecture and HfO$_2$ contents can be effectively controlled and optimized
- Low oxygen activity in the HfO$_2$-Si bond coats
NASA Turbine Environmental Barrier Coating Developments – Environmental Testing Validations

- Advanced NASA EBCs tested in coupons under laser heat flux cyclic rigs up 1650°C+
- Coated subelements coating tested up 1500°C under laser thermal gradient for 200 hr
- EBC systems show high stability in High Pressure Burner Rig Tests
- Low thermal conductivity of 1.2 W/m-K for optimized turbine airfoil coatings

High pressure burner rig, 16 atm, 31 hr – no measureable weight loss
NASA EBC Bond Coats for Airfoil and Combustor EBCs

– Advanced systems developed and processed to improve Technology Readiness Levels (TRL)

– Composition ranges studied mostly from 50 – 80 atomic% silicon
  • PVD-CVD processing, for composition downselects - also helping potentially develop a low cost CVD or laser CVD approach
  • Compositions initially downselected for selected EB-PVD and APS coating composition processing
  • Viable EB-PVD and APS systems downselected and tested; development new PVD-CVD approaches

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<tr>
<th>PVD-CVD</th>
<th>EB-PVD</th>
<th>APS*</th>
<th>FurnaceLaser/CVD/PVD</th>
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<td>YSi</td>
<td>YbGdYSi</td>
<td>GdYSi</td>
<td>HfO2-Si; REHfSi YSi+RESilicate</td>
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- Process and composition transitions

- APS*: or plasma spray related processing methods

- Used in ERA components as part of bond coat system

- Used also in ERA components
- Used in ERA components as part of bond coat system

- Hf-RE-Al-Silicate
NASA EBC Bond Coats for Airfoil and Combustor EBCs

- 1500°C (2700°F) capable NASA RESi+X (X is dopants) EBC bond coat compositions and related composite coatings developed for combustor and turbine airfoil applications
- The bond coat systems demonstrated durability in the laser high heat flux rig in air and steam thermal gradient cyclic testing
- The bond coatings also tested in thermal gradient mechanical fatigue and creep rupture conditions

Selected Composition Design of Experiment Furnace Cyclic Test Series 1500°C, in air, Demonstrated 500 h durability

Processed Subelement

Steam heat flux test rig of the bond coat

High heat flux cyclic rig tested Zr/Hf-RE-Si series EBC bond coats on the bond coated woven SiC/SiC CMCs at up to 1500°C in air and full steam environments
Rare Earth (RE) Silicides/Silicates and Effect of the HfO$_2$ Dopant

- Dopants improving oxidation resistance, pesting, and SiO$_2$ separation

YbSi$_x$ (no dopant)
Exposed to 1100°C for 20 h

Undoped system shows separation of Si-rich/silica-rich phase

YbSi$_x$ + Hf
1100°C for 20 h

The Si-rich/silica-rich phases converted to more stable HfO$_2$ rich phases
YbSi$_x$

1450-1500°C exposure for 100 hr
Advanced RE-Si Based EBC Bond Coats: Controlled Oxygen Activities, Dopant Additions

- Advanced compositions improve high temperature stability, environmental resistance, and reduce grain growth

YbSi-YbSi(O) EBC bond coat, 1500°C tested

YbSi-YbSi(O)+Hf EBC bond coat, 1500°C tested
Furnace Cycle Test Results of Selected RESi and ZrSi + Dopant Bond Coats

- Testing in Air at 1500°C, 1 hr cycles

- Multi-component systems showed excellent furnace cyclic durability at 1500°C
Advanced Bond Coats for Turbine EBCs – Oxidation Resistance

- 1500°C (2700°F) capable RESiO+X series EBC bond coat compositions and related composite coatings developed for combustor and turbine airfoil applications.
- Oxidation kinetics studied using TGA in flowing O₂.
- Parabolic or pseudo-parabolic oxidation behavior observed.

Kp as a function of silicon content:

An oxidized bond coat after 1500°C 100 h creep testing.

Oxidation kinetics of a YbGdSi(O) bond coat.
Advanced EBC developments – Some Hybrid APS-PVD Systems and Qualification Tests

- EB-PVD HfO$_2$-RE$_2$O$_2$ (Silicate) top coat EBC with plasma-spayed multi-component advanced silicate sublayer EBC/HfO$_2$-Si bond coat systems
- Low thermal conductivity ranging 1.0 - 1.7 W/m-K
- Demonstrated high pressure environmental stability at 2600-2650°F, 12-20 atm. in the high pressure burner rig

2” diameter ND3 EBC/SiC/SiC specimen after testing in the high pressure burner rig
At 2600°F

Some surface spallation

High pressure burner rig tested new ND series Hybrid EBC systems coated on 2” diameter Gen II Prepreg SiC/SiC CMCs
Thermal Gradient Tensile Creep Rupture Testing of Advanced Turbine Environmental Barrier Coating SiC/SiC CMCs

- Advanced high stability multi-component hafnia-rare earth silicate based turbine environmental barrier coatings being successfully tested for 1000 hr creep rupture
- EBC-CMC creep, fatigue and environmental interaction is being emphasized
Advanced environmental barrier coatings – Prepreg CMC systems demonstrated long-term EBC-CMC system creep rupture capability at stress level up to 20 ksi at $T_{EBC}$ 2700°F (1482°C), $T_{CMC\,\text{interface}}$ ~2500°F (1371°C)

- The HfO$_2$-Si based bond coat showed excellent durability in the long term creep tests

EBCs on Gen II CMC after 1000 h low cycle creep fatigue testing

Hybrid EBCs on Gen II CMC after 1000 h low cycle creep fatigue testing
EBC-CMC Thermal Gradient Creep Rupture and Delamination Modeling

- An equivalent stress model is established for EBC multicrack stress intensity modeling: emphasize creep, thermal gradient and stress rupture interactions
- Benchmark failure modes established in EBC systems

EBC-CMC Thermal Gradient Creep Rupture and Delamination Modeling – Bond Coat Stiffness Effect

- Advanced EBCs designed with higher strength and stiffness to improve creep, fatigue, and cyclic durability
- FEM models showed that a soft bond coat showed larger “spalling” displacements

High Stability and CMAS Resistance: Improved by Advanced High Melting Point, and Multi-Component Coating Compositions

- Demonstrated CMAS resistance of the NASA RESi System at 1500°C, 100 hr
- Silica-rich phase precipitation in CMAS
- Rare earth element leaching into the melts (low concentration ~9 mol%)
High Stability and CMAS Resistance: Improved by Advanced High Melting Point, and Multi-Component Coating Compositions

- Non stoichiometric characteristics of the CMAS – rare earth silicate reacted apatite phases – up to 200 hr testing
- Difference in partitioning of ytterbium vs. yttrium in the apatite phases
  - Average AEO/RE$_2$O$_3$ ratio ~ 0.68 for ytterbium silicate – CMAS system
  - Average AEO/RE$_2$O$_3$ ratio ~ 0.22 for yttrium silicate – CMAS system

Fatigue Tests of Advanced RESi Bond Coats and EBC Systems

- APS and PVD processed 2700°F bond coats on CMCs: focus on fatigue testing at the temperature range of 2400 to 2700°F
- Incorporating CMAS and steam environments

**Creep Test with CMAS**

**Fatigue Tested**

- APS Bond Coat series on CVI-MI SiC/SiC EBC at 1400°C, 10 ksi, 400 hr

- PVD GdYSi coated on Hyper Them 12C-461-002_#17
  1316°C, 10ksi, 1000 h fatigue (3 Hz, R=0.05)

- 1316°C, 15ksi, 1169 h fatigue (3 Hz, R=0.05) on GE Prepreg SiC/SiC

- 1537°C, 10ksi, 300 h fatigue (3 Hz, R=0.05) on CVI-MI SiC/SiC (with CMAS)
Thermomechanical Fatigue Tests of Validating Advanced RESi Bond Coats and EBC Systems

- Strength and Fatigue cycles in laser heat flux rigs in tension, compression and bending
- Fatigue tests at 3 Hz, 2600-2700°F, stress ratio 0.05, surface tension-tension cycles
- Total fatigue-CMAS durability demonstrated

**Example of fatigue test EBC systems on Tyrannohex SiC composites**

![Graph showing fatigue or creep hot time in hours vs. maximum stress in MPa](image)

Achieved long-term fatigue lives (near 500 hr) with EBC at 2700°F

Tested, SA Tyrannohex with bond coat only

Tested, SA Tyrannohex with EBC system 188

Creep-fatigue durability test summary
The Advanced EBC on SiC/SiC CMC Turbine Airfoils Successfully Tested for Rig Durability in NASA High Pressure Burner Rig

- NASA advanced EBC coated turbine vane subcomponents tested in rig simulated engine environments (up to 240 m/s gas velocity, 10 atm), reaching TRL of 5
- Turbine EBCs generally intact (some minor partial coating top coat spalling for the coated Prepreg MI SiC/SiC vane)
- Some minor CMC vane degradations after the testing

Uncoated vane tested 15 hr

EBC Coated CVI SiC/SiC vane after 31 hour testing at 2500°F+ coating temperature
EBC Coated Prepreg SiC/SiC vane after 21 hour testing at 2500°F
EBC Coated Prepreg SiC/SiC vane tested 75 hour testing at 2650°F
The EBC Coated SiC/SiC CMC Combustor Liner Successfully Demonstrated for Rig Durability in NASA High Pressure Burner Rig (First Inner Liner Processed at Sulzer with Triplex Pro)

- Tested pressures at 500 psi external for outliner, and up to 220 psi inner liners in the combustion chamber (16 atm), accumulated 250 hours in the high pressure burner rig
- Average gas temperatures at 3000°F (1650°C) based on CEA calculations, the liner EBCs tested at 2500°F (1371°C) with heat fluxes 20-35 W/cm², and the CMC liner component at 1800-2100°F (~1000-1100°C)

![Graph of Ideal Flame Temperature Calculation - Chemical Equilibrium Analysis Codes (CEA)-II](image)

- Hot streaks with possible gas temperature over 2000°C, with minimum back cooling
- Swirl jet flows
- Some minor coating spalling at hot streak impingement
Summary

- Durable EBCs are critical to emerging SiC/SiC CMC component technologies
- The NASA EBC development built on a solid foundation from past experience, evolved with the current state of the art compositions of higher temperature capabilities and stabilities
  - Multicomponent EBC oxide/silicates with higher stabilities
  - Improved strength and toughness
  - HfO$_2$-Si and RE-Si bond coats for realizing 1482°C+ (2700°F+) temperature capabilities and potentially prime-reliant EBC-designs
  - New EBC compositions improved combustion steam and CMAS resistance
- EBC processing and testing capabilities significantly improved, allowing more advanced compositions designed, validated and realized for more complex turbine components
- Improved the understanding of coating failure mechanisms, helping developing coating property databases and validated life models, also aiming at more robust EBC-CMC designs and developments
- Emphasized next generation turbine airfoil EBC developments, demonstrated component EBC technologies in simulated engine environments of TRL 5
Emerging Opportunities for EBC System Research and Development

- High melting point, high toughness, low expansion EBC top coat designs with advanced architectures and grain boundary phase designs to achieve exceptional environment stability and performance
- High stability nano-phase composite bond coat designs involving rare earth, hafnium and silicon-containing dopant alloy clusters for improved oxidation resistance and cyclic durability, minimizing silica separation and crystallization, at high temperature and in larger chemical potential gradients
- Self-repairing and/or self-growing of slow growth adherent EBC coatings
- Superior adhesion and intergraded EBC/CMC interfaces with reaction barriers, potentially integrated additive CMC-coating manufacturing
- High efficiency plasma spray, PVD and/or CVD cost effective and robust processing
- High strength and high toughness, combined with optimized strain tolerance for superior erosion and impact resistance
- Multifunctional compositions
  - High strength and high toughness, combined with optimized strain tolerance for superior erosion and impact resistance, self-healing
  - High temperature sensing, health monitoring, and reduced heat transfer