Hardware Demonstration:
Conducted Transients on Spacecraft Primary Power Lines
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## Acronym List

<table>
<thead>
<tr>
<th>Acronym</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>CE</td>
<td>Conducted Emissions</td>
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<tr>
<td>CMCE</td>
<td>Common Mode Conducted Emissions</td>
</tr>
<tr>
<td>CS</td>
<td>Conducted Susceptibility</td>
</tr>
<tr>
<td>EMC</td>
<td>Electromagnetic Compatibility</td>
</tr>
<tr>
<td>EMI</td>
<td>Electromagnetic Interference</td>
</tr>
<tr>
<td>GEVS</td>
<td>General Environmental Verification Specification</td>
</tr>
<tr>
<td>GSFC</td>
<td>Goddard Space Flight Center</td>
</tr>
<tr>
<td>LISN</td>
<td>Line Impedance Stabilization/Simulation Network</td>
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<tr>
<td>NASA</td>
<td>National Aeronautics and Space Administration</td>
</tr>
</tbody>
</table>
One of the sources of potential interference on spacecraft primary power lines is that of conducted transients resulting from equipment being switched on and off of the bus.

Susceptibility to such transients is addressed by the CS06 requirement of MIL-STD-461/462 prior to 1993.

This demonstration provides:

- Basis for understanding of the sources of these transients
- Analysis techniques for determining their worst-case characteristics (e.g. magnitude and duration)
- Guidelines for minimizing their magnitudes and applying the requirement appropriately
Anatomy of Transients

- Normal transients on primary power bus result from equipment being switched on/off bus
  - Turn-on transient: negative going pulse
  - Turn-off transient: positive going pulse

- Characteristics of transient (magnitude, duration) determined by interaction of common source impedance with load impedance

**TURN-ON TRANSIENT MODEL**
(negative pulse)

**TURN-OFF TRANSIENT MODEL**
(positive pulse)
Power Distribution Harness Impedance Model

- Common distribution impedance generally dominated by distribution wiring
- Modeled as 2-wire transmission line
- Lumped model sufficient for most applications
- Line Impedance Stabilization/Simulation Network (LISN)
  - Used to represent wiring impedance
  - Based on lumped parameters; schematic usually looks like lumped model
  - Generally identified by inductance, e.g. 5 µH, 10 µH, 50 µH, etc.

\[ Z_0 = \sqrt{\frac{L}{C}} \]
Positive (+) and negative (-) bundles can be separated by 10s of cm

Typical distribution wiring length

- Unmanned spacecraft: ~1 meter, ~1 µH
- Larger platforms can have higher impedance buses; use LISNs ranging from 5 µH to 50 µH, depending on application

Typical parameters:
- $R/l = 3 \, \text{mΩ/m}$
- $L/l = 1 \, \text{µH/m}$
- $C/l = 10 \, \text{pF/m}$
- $Z_0 = 350 \, \Omega$
Power Distribution Harness Impedance Model (cont.)

MIL-STD-461 50 μH LISN

MIL-STD-461 5 μH LISN
Discrete Inductors from LISNs

**Space Station LISN**
Pair of 10 µH inductors
(11 µH as-measured)

**Tegam 95300-50 LISN**
50 µH
(51 µH as-measured)
For typical turn-on transients, inductance dominates common source impedance

- Load capacitance is generally many orders of magnitude higher than the wiring capacitance
- Wiring capacitance may generally be ignored
- Common source impedance may be modelled as bulk inductance
Demonstration 1a: Turn-On Transient w/ Discrete Inductor

ΔV_{peak} = \text{bus potential} \\
\text{(pulled to 0 V)} \\
\tau \approx 10 \ \mu\text{sec} \\
\tau \approx 23 \ \mu\text{sec} \\
Good agreement betwixt measurements and simulations for discrete inductors
Demonstration 1b: Turn-On Transient with Added Capacitance at Distribution Point

What happens when we add capacitance $C_D$ at distribution point that is greater than load capacitance $C1$…?

![Circuit Diagram]

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.tran 0.0001
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For typical turn-off transients, common source impedance may be modeled by bulk series inductance and bulk shunt capacitance:

- Javor in [1] and [2] emphasized use of LISN in order to define a repeatable test method.
- This study addresses the physical parameters of the harness, i.e. inductance and capacitance, in order to properly bound the properties of typical transients observed on GSFC platforms in order to assess the applicability of the CS06 positive transient.

When switch opens at t = 0, inductor current continues to flow.
Demonstration 2: Turn-Off Transient w/Discrete Inductors

$I_0$ normalized to 1 A for all measurements and simulations

$$\Delta V_{peak} = I_0 \sqrt{\frac{L}{C}}$$

$$\tau = \sqrt{LC}$$

$\tau = \text{duration of impulsive spike due to opening switch}$

Ringing occurs with period

$$T = 2\pi\tau$$
How about a real cable?

- Previous simulations and measurements were performed using discrete components
- We wanted to see if the lumped model accurately predicted the transients on actual cable
- **RG58 used as case study**
  - Coax never used for power wiring
  - Used because of well-defined and well-controlled impedance characteristics
- Used lengths of 16.8 m, 25.4 m, and 31.5 m

\[
\begin{align*}
R/l &= 51 \text{ mΩ/m} \\
L/l &= 0.25 \text{ µH/m} \\
C/l &= 100 \text{ pF/m}
\end{align*}
\]

**Frequencies for transients considered in this study**
Demonstration 3: Turn-Off Transient w/RG58 Coax

Bulk parameter model provides good agreement with measured results

\[ Z_0 = \sqrt{L/C} = 50 \, \Omega \]

\( \Delta V_{\text{peak}} \) independent of pulse width

\[ \tau = \sqrt{LC} = 5 \, \text{nsec/m} \]

\[ \text{Period} = 2\pi \sqrt{LC} = 31 \, \text{nsec/m} \]
Now that we have established confidence in our models, we can extrapolate them to predict typical transients on spacecraft.

Recall typical power wiring characteristics:
- (+) and (-) bundles separated by 10s of cm
- ~1 meter from battery to distribution point
- Parameters:
  - \( R = 3 \, \text{m}\Omega \)
  - \( L = 1 \, \mu\text{H} \)
  - \( C = 10 \, \text{pF} \)
  - \( Z_0 = 350 \, \Omega \)

We can plug these values into our models...
Turn-On Transient: Typical

Representative Turn-On Transient Circuit Model

\[ \Delta V_{\text{peak}} = \text{bus potential} \]

(pulled to 0 V; does not go negative)

\( \sim 10 \, \mu\text{sec} \)
Tailored CS06 (-) pulse good representation for turn-off transient

- 10 µsec pulse width
- Magnitude
  - Tailor to equal line potential to pull bus to 0 V (no lower)
  - MIL-STD-461A default is lesser of 2x line voltage or 100 V
  - WILL pull the bus negative; not desired
Turn-Off Transient: Typical (open circuit)

Representative Turn-Off Transient Circuit Model

\[ \Delta V_{\text{peak}} > 200 \text{ V} \]

for \( I_0 = 1 \text{ A} \)

Pulse width \( \approx 10 \text{ nsec} \)
Turn-Off Transient With Filter at Distribution Point

Representative Turn-Off Transient Model With Filter in Power Distribution Unit (PDU) or equivalent

Transient at distribution point

$\Delta V \approx 0.1 \ V$

Transient easily “snubbed” with additional capacitance at distribution point
CS06 Positive (+) Pulse

- CS06 (+) pulse NOT good representation for turn-on transient
  - Magnitude: tailorable; not really an issue
  - 10 µsec pulse width much longer than that of typical transients
  - Source impedance < 1 ohm; much lower than that of typical transients (not as easily “snubbed”)

\[ E = 2x \text{ line voltage or 100 V, whichever is less} \]
\[ t = 10 \mu\text{sec} \]
Let's Return to Our Turn-On Transient Model…

Representative Turn-On Transient Model With Filter in Power Distribution Unit (PDU) or equivalent

\[ \Delta V < 1 \text{ V} \]
Summary

● Turn-off transients do not pose significant problem on most spacecraft
  ■ Open-circuit potential can be high, but very short duration
  ■ Easily “snubbed” with modest amount of capacitance on load input filters or at distribution point
  ■ Eliminated with large filter capacitor at distribution point (if used)
  ■ CS06 positive-going pulse need not be applied
  ■ Even if open-circuit large magnitude, short duration turn-off transient were considered real, Javor showed in [3] that it poses no threat to input filter components

● On any spacecraft platform, an analysis of the power subsystem should be performed as early as possible in order to determine the worst-case magnitudes of turn-on and turn-off transients that may be observed at the point of distribution

● If these magnitudes are determined to be sufficiently benign, i.e. on the order of 3 V or less, then CS06 negative-going pulse need not be applied either

● Any concerns sufficiently covered by GEVS tailoring of CS101 and CS114 as below:
  ■ CS101, 1 Vrms (2.8 V peak-to-peak) from 30 Hz to 150 kHz
  ■ CS114, effective limit of 1 Vrms (20 mA into 50 Ω) from 150 kHz to 50 MHz
References


THANK YOU!
Backup
A Proper Switch

- Proper testing of transients requires:
  - Bounce-less, arc-less switch
  - Repeatable rise times that are fast (short) compared to circuit response