Measurements of Turbulence Convection Speeds in Multistream Jets Using Time-Resolved PIV

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Motivation

• **Goal**: Noise reduction concepts and prediction tools to engineer them on aircraft.

• Explore noise reduction concepts keyed to local convection speed, influenced by modifying flow profiles (*a la* Papamoschou)
  – Offset externally mixed nozzles

• Only a small part of turbulent energy couples to acoustic far-field, and convection speed one aspect of this ‘filter’.

• Convection speed of turbulent eddies play key role in acoustic analogies.
  – To create a design tool, relate $U_c$ to parameters from RANS solutions

• Important to note: convection speed of what?
  – Bulk turbulent velocity, pressure, vorticity, scalar
  – Spatial, frequency modes of these parameters?
Previous experimental work

• Older hot-wire work
  – Two probes, separate in space, measure time delay in correlation
  – Common result shown, radial profile of convection speed $U_c$, mean velocity $\langle u \rangle$
  – Usually measured in potential core region
  – $U_c$ matches $\langle u \rangle$ at $\langle u \rangle / U_{jet} \approx 0.6$
  – $U_c = 0.6U_j$ often used as simple model for convection speed at jet cross-section, including hydrodynamic near-field

Recent experimental efforts

- **Multiple-PIV tests**
  - Dual conventional PIV setups
  - Two velocity fields acquired at discrete time delays
  - Correlations of velocity fields give $R(\xi_1, \xi_2, \tau) \rightarrow Uc$

- **Time-resolved PIV tests**
  - Acquire velocity fields over contiguous time series
  - Limited spatial fields, typically looking at large $x$

- **PLIF/PDV image correlation**
  - Correlation of scalar «==» velocity?

- **Time-resolved DGV**
  - Limited spatial extent

- Most work limited to single-stream jets

- Need to measure convection speed of turbulence in **multi-stream, non-axisymmetric** jets **efficiently**
  - Limited to bulk turbulence, possibly filtered by frequency

Bridges & Wernet, “Measurements of the Aeroacoustic Sound Source in Hot Jets” AIAA 2003-3130
Previous TRPIV Methodology

- Previous time-resolved PIV
  - CCD arrays combined in 20x300mm FoV to compliment narrow axial laser sheet
  - 25kHz dual laser rate
  - Acquire axial strips of velocity map movies along lipline and along centerline
  - Process to space-time correlations of velocities, Reynold stresses
  - Required many moves of optics to capture entire jet

New TRPIV methodology

- Lightsheet in streamwise plane, at 90° to jet axis
- Narrow (axial) sheet width
- Camera vertical FoV: 55x140mm, translated three times to acquire full 360mm cross-section of jet
- Acquire velocity maps at 25kHz.
- Process velocity map movie to get axial profile of convection velocity
Correlation processing

- Basic concept of computing convection velocity is simple:
  - Calculate space-time correlation, track peak $x(t)$, take derivative
- Wide range of convection velocities in same measurement
  - FoV limits maximum time delay $\tau$
  - Acquisition rate limits temporal accuracy
  - Use fitting of single-power exponent to get subsample resolution
Axisymmetric single-stream jets

- Single-stream (internal plug), 95mm ø
- Replicate literature for cold subsonic jets
- Replicate NASA Consensus data
  - Confirm basic velocity statistics, mean $\langle u \rangle$ and variance $\langle uu \rangle$
  - Tanna matrix of velocity, temperature

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Typical result

- Single-stream jet (unheated, $Ma = 0.5$)
Comparison with historical data

- Single-stream jet (unheated, $Ma = 0.5$)
- $x/D_j = 6.5$ (TRPIV) vs $x/D_j = 5$ (hotwire)
- $U_c = \langle u \rangle$ at $\langle u \rangle = 0.6$
- TRPIV measures lower $U_c$ at outer jet edge than hotwire
Features

- Single-stream jet (unheated, $Ma = 0.5$)
- $U_c = \langle u \rangle$ where $\langle uu \rangle$ is high. $U_c$ not matching $\langle u \rangle$ where $\langle uu \rangle$ weak.
Trends with axial location

- Single-stream jet (unheated $Ma = 0.5$)
- $U_c \sim \langle u \rangle$ where $\langle uu \rangle >> 0$
- Interesting details around wake of plug on centerline and outside jet near nozzle

![Graphs showing trends with axial location at different x/Dj values](image-url)
Impact of heat

- Single-stream jet \((T_s/T_\infty=2.7, \ U_j/c_\infty = 1.48)\)
- Convection speed roughly same as mean velocity where \(<uu> \neq 0\)
Axisymmetric multi-stream jets

• Nozzle hardware from three-stream externally mixed experiments of Henderson
  – Axisymmetric (C1T1) with $A1:A2:A3 = 1:2.5:1$
• Flow conditions
  – Representative of engines
  – Chosen for variations in shear layers
  – Hope to see variations in convection speed

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Two-stream jet

- ‘Axisymmetric’ jet not so symmetric in reality.
- Where $\langle uu \rangle$ is relatively small, $Uc$ closer to nearest $\langle u \rangle$ where $\langle uu \rangle$ is large.

\[
x = 0.29m\\
\]
Three-stream jet

- Three-stream jet (Velocity ratios 430:275:330:102)
- Tertiary stream mixes out by first measurement station
  - Only two shear layers present
- Strong asymmetry grows
  - Asymmetry in $\langle uu \rangle$ much stronger than in $\langle u \rangle$
- $Uc$ still tracks $\langle u \rangle$
Source of Asymmetry?

- Due to geometric defect? Nonuniform ambient? Unstable hot core?
- Compare with and without flight stream, with and without hot core.
- Asymmetry in all, especially $\langle uu \rangle$.
- Constant in plots is geometry.
- Never assume symmetry!

All unheated
Non-axisymmetric multi-stream jets

- Asymmetric velocity profiles
  - Offset (SDCT) with $\Delta z = 4\text{mm} (D_3 = 294\text{mm} \phi)$
  - Partial duct (PART) with 180° tertiary stream
- Demonstrated non-axisymmetric sound fields


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Three-stream offset jets--SDCT

- Three-stream jet (Velocity ratios 430:330:275:102) with offset tertiary
- Tertiary stream evident on thick side (negative y) at x=0.29m
- Offset peak $\langle u \rangle$ by x=1.14m
- $U_c$ still tracks $\langle u \rangle$.
Three-stream offset jets--PART

- Three-stream jet (Velocity ratios 430:330:275:102) with 180° tertiary (negative y)
- Tertiary stream reduced shear initially.
- Offset peak $\langle u \rangle$ by $x=1.14m$
- $U_c$ still tracks $\langle u \rangle$

![Graphs showing velocity distributions at different $x$ values](image-url)
Conclusion

• **Rule:** $U_c$ follows $\langle u \rangle$, where $\langle uu \rangle$ is strong. Where $\langle uu \rangle$ is not strong, $U_c$ is biased toward $U_c$ where $\langle uu \rangle$ is strong.

• Seems to be true for $U_c$ of near-field hydrodynamic pressure as well.
Summary

• For single jets, $\langle uu \rangle$ peaks around $\langle u \rangle / U_j = 0.6$, hence this value is dominant in most measurements, including local hydrodynamic pressure at jet edge.
• Applying the Rule to multi-stream jets: $U_c$ of near-field hydrodynamic wave packets will be most influenced by closest (outermost) shear layer.
• If convection speed of near-field hydrodynamic wave packet determines source strength, then sound source is controlled by outermost shear layer.
• For engineering use, $U_c = \langle u \rangle$ is a good assumption for bulk turbulence.
  – Where $U_c \neq \langle u \rangle$, then $\langle uu \rangle$ too small to matter anyway.