Abstract—There is a high need for >2 THz room temperature direct-detectors/harmonic-mixers to characterize THz optical sources, phase lock THz-QCLs as LO sources for multi-pixel receivers, and realize absolute frequency calibration sources for applications in astrophysics, earth science, and remote sensing. Thus, we have developed a WM-52 (WR-0.22) harmonic mixer for the 3 - 5 THz operation. The design, fabrication and assembly of the THz mixer are discussed.

INTRODUCTION

THz technology spanning the Far-Infrared (FIR) and Sub-Millimeter (SMM) wavelengths has applications in astrophysics, earth and planetary science and a stabilized Local Oscillator (LO) is a critical component to build Terahertz (THz) instruments that enable airborne and ground based science investigations [4][6]. Compact and stable THz receivers can be mounted on a spacecraft, aircraft, balloon or in a cubesat to measure dynamics in the atmosphere, trace gas distribution, radiation balance and thermal structure [5]. Due to intervening dusty materials in space, it is difficult to use visible-light telescopes to perform astrophysical measurements to address key questions such as the process of star formation in our galaxy and in galaxies of the earlier universe. However, the effect of obscuration in FIR and SMM wavelength regions is nearly negligible and probing star forming region dynamics and content via high-resolution spectroscopy is feasible using THz instruments.

Therefore, a high-output-power and highly stable 2-6 THz Local Oscillator (LO) with low phase noise is necessary to build a multi-pixel receiver (n > 10), a tunable heterodyne spectrometer and an interferometer with high spectral resolution (\( R = \lambda / \Delta \lambda > 10^7 \)) and < kH\( z \) long term stability. This can be achieved by phase locking a Quantum Cascade Laser (QCL) to a highly stable microwave reference to produce a high power and stable LO source using a room temperature harmonic mixer [3].

THz HARMONIC MIXER

Previously, we demonstrated a 2 - 3.2 THz harmonic mixer with a conversion loss of ~27 dB and used the mixer to phase lock a 2.5 THz and 2.7 THz QCLs [2]. To realize such an implementation at higher frequencies, we designed and fabricated a WR-0.22 harmonic mixer with GaAs-based substrate, and thickness of 2\( \mu m \) and width of 18\( \mu m \). The integrated THz circuit is fabricated at Chalmers University and the diode process is based on electron beam lithography, with a beam spot of less than 5 \( \mu m \), allowing precise and repeatable anode and air bridge formation [1]. Anode areas of ~ 0.28 \( \mu m^2 \) were fabricated for approximately 3 – 4 \( \mu m \) finger length structures. The mixer also contained a WR-1.0 LO waveguide that allows 750-1100 GHz signal and couples to the quartz based LO probe. To maintain the LO termination, the transmission line length is kept a half wavelength away from the diode to the short circuited beam lead. When the mixer is pumped through the LO port, it is important to deliver maximum power by isolating the LO and IF channel; therefore, an IF circuit containing a Hi-Z and Low-Z based low pass filter is used to block the LO signal propagation into the IF channel. Fig. 1 depicts the internal circuitry and the machined block of the WR-0.22 harmonic mixer.

Machining the mixer’s block is performed using CNC milling machine. The block has an E-plane split between the base and the cover, and the base contained the THz channel, which is the smallest dimensions, approximately 6 \( \mu m \) by 26 \( \mu m \). Due to the smaller dimensions, assembling the circuits by hand within 2 – 3 \( \mu m \) accuracy is a very challenging task to achieve. For the targeted design of a THz circuit floating height of 6 \( \mu m \), machining error in the THz circuit channel could introduce 2 – 3 \( \mu m \) variation which can leads to a 3 – 9 \( \mu m \) final floating height. The mixer is assembled at Virginia Diodes, Inc. under a microscope. First the mixer block is cleaned properly, followed by mounting the LO probe, IF filter, IF circuit and THz supporting substrate circuits into their proper channels. Bonding the LO probe with the IF circuit and IF filter with IF circuit is done using 16 \( \mu m \) and 24.5 \( \mu m \) bond wires respectively. Once those circuits are stably positioned, the THz circuit is placed on top for the LO probe and the THz supporting circuit and connected using conductive epoxy. Once all the circuits are mounted in a mixer block as shown in Fig. 1, the two halves of the block are aligned, fastened together and the block is ready for RF testing.

Figure 1. WM-52 (WR-0.22) harmonic mixer design.
The initial characterization of the mixer is performed by testing the mixer’s current-voltage (I-V) relationship (Fig. 2), and the diode DC-parameters are extracted by curve fitting to an ideal diode model. The diode parameters are series resistance $R_s = 25 \, \Omega$, ideality factor $\eta = 1.45$ and saturation current $I_0 = 13 \, \mu A$.

![I-V curve of the THz diode.](image)

Figure 2. I-V curve of the THz diode.

To realize the LO coupling efficiency, the mixer’s return loss is measured using VDI’s WR-1.0 extender modules for 750-1100 GHz. The systematic errors are removed by calibrating the extender modules using VDI’s standard TRL calibration kit. The return loss measurement is repeated for different current biases between 16-275 µA. The performance improved for higher current biases, and the test result shows a nominal return loss of 10 dB for frequencies above 900 GHz, Fig. 3.

![LO return loss for 750-1100 GHz using WR-1.0 extender module.](image)

Figure 3. LO return loss for 750-1100 GHz using WR-1.0 extender module.

LO video response at 830 GHz is measured actively for a range of input powers by pumping the mixer with LO power while modulating the LO signal and measuring the output voltage on a lock-in amplifier. To perform this measurement, a high power WR-1.0 amplifier multiplier chain (AMC) is used to drive the mixer and a coupler is used to actively measure the input power to the mixer. The mixer is also current biased at 16 µA and 135 µA and the LO-responsivity of the mixer is estimated to be 500 V/W. Due to the relatively improved return loss performance above 900 GHz, the LO video response and responsivity are expected to perform more than 500 V/W.

![LO video response vs. input power for current bias of 16 µA and 135 µA.](image)

Figure 4. LO video response vs. input power for current bias of 16 µA and 135 µA.

From the HFSS model, the RF probe has a return loss of greater than 15 dB. Moreover, the mixer’s RF responsivity and conversion loss performance will be tested using 3.8 THz and 4.7 THz QCLs. The mixer will be utilized to phase lock the QCLs to use as stable frequency source and THz LO oscillator.

CONCLUSION AND FUTURE WORKS

A WR-0.22 harmonic mixer is designed and fabricated to phase lock QCLs. Once the mixer is assembled, the initial performance, such as I-V, LO return loss and LO video response at different current biases are measured. Future work includes characterizing the RF video response, conversion loss of the mixer and phase locking of QCLs within the WR-0.22 harmonic mixer band, particularly 3.8 THz and 4.7 THz.

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REFERENCES


