Overview of Heatshield for Extreme Entry Environment Technology (HEEET)

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International Conference on Flight Vehicles, Aerothermodynamics and Re-entry Missions & Engineering, 30 September – 3 October 2019, Monopoli, Italy
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**NASA Facilities:**
- Ames:
  - Arcjet Complex
  - STAR Lab
  - EEL
  - Main Shop
- JSC:
  - ES4/Manufacturing
- LaRC:
  - James H. Starnes, Jr., Structures and Materials Laboratory
  - Light Alloy Lab
  - Materials Research Lab
  - Model Shop
  - Systems Integration and Test Branch Laboratory

**External Partners:**
- Bally Ribbon Mills
- Fiber Materials Inc.

**External Test Facilities:**
- Laser Hardened Materials Evaluation Laboratory (LHMEL)
- Arnold Engineering Development Center (AEDC)
- NTS

**External NDE:**
- Hadland
- NSI
- VJ Technologies

**Carrier Structures:**
- AASC
Outline

• HEEET = Heatshield for Extreme Entry Environment Technology
• Motivation for HEEET
• Implementation (2014 – 2019)
  – Requirements
  – Manufacturing
  – Aerothermal
  – Structural
• Documentation
  – Design Data Book
• Final TRL Assessment
Motivation for HEEET

- Address a shortfall in available TPS to meet NASA’s needs for planetary science missions with very high heating entry environments
- Desire to develop a system that would avoid some of the sustainability challenges related to “heritage” TPS (i.e. Carbon Phenolic)
What is the HEEET Material?

Mid-density 3D woven dual layer carbon phenolic

• 3D layer to layer weave
• Dual Layer:
  – OML Layer = Recession Layer (RL) – manages recession
    – Higher density all carbon fiber weave, exposed to entry environment
  – IML Layer = Insulation Layer (IL) – manages heat load
    – Lower density, lower thermal conductivity, blended carbon/phenolic yarn
  – 2 layers are integrally woven together,
    – mechanically interlocked (not bonded)
• Woven material has medium density phenolic resin infusion
  – Higher phenolic loading than PICA
  – Open porosity
Seams in the HEEET Architecture

- Target vehicle sizes range from <1m – >3.5m base diameter
- A tiled heatshield design is required due to weaving width limitations
  - Results in seams between tiles – the most challenging part of HEEET development
- The HEEET project has baselined a gap filler between tiles to perform two primary functions:
  - Provide structural relief for all load cases by increasing compliance in the joint
  - Provide an aerothermally robust joint
- Two factors inherent to the HEEET material and its mission applications drive requirements at the seams in the system.
  - Aerothermal environments for HEEET mission architectures require unsupported adhesive joint widths be minimized to prevent runaway failure at the seam
    - IHF 3” nozzle testing at ~3500 W/cm² and 5 bar suggest joints ≤ 0.010” are required
  - HEEET in-plane modulus is high
    - As the carrier structure deflects the HEEET architecture must have sufficient compliance to maintain compatibility with the carrier without inducing excessive stress in the system
HEEET Manufacturing Overview

Fiber Manufacturing (Raw Materials) → Carbon Fiber (Recession Layer) → Weaving → Cutting → Forming

Kynol Japan

Carding → Blended Yarn (Insulation Layer) → Schappe

Bally Ribbon Mills

Fiber Materials Inc.

Tile Infusion → Gap Filler Infusion → HEEET Softening Process → Machining → HEEET TPS Assembly & Integration

NASA ARC (During Development)

Fiber Materials Inc.

MDU/ETU Test Coupons

NASA JSC

Carrier Structure / Sub-straight Fabrication → Applied Aerospace Structures Co (AASC)
Bally Ribbon Mills (BRM) Weaving

• 2 Phase scale up in weaving capability
  – Phase 1: From 1” thickness x 6” width to 2.1” thickness x 13” width
  – Phase 2: Increased width to 24” (2.1” thickness)
• Forming, resin infusion and machining processes were initially developed in-house
• Established processes were Tech Transferred to Fiber Materials Inc. (FMI)
• FMI performed an upgrade to Infusion Vessel to support HEEET infusion process
• FMI successfully fabricated acreage tiles and gap fillers for the ETU
1m ETU Successfully Built and Inspected by CT Scan
Aerothermal Test Campaign

Objectives for aerothermal test campaign:
1. Support development and validation of the TPS sizing tools
2. Exercise the system (acreage and seams) under mission relevant conditions to establish system capability
   • Looking for failure modes
• 12 arcjet test series conducted
• >140 coupons tested
• First testing in the IHF 3” nozzle
  • 3500 W/cm² and 5 bar
• First NASA testing in AEDC H3 facility
  • 4000 Pa shear
• FIAT code adapted to support dual layer TPS sizing
• Novel dual layer margins policy developed
HEEET Arcjet Testing Covers Some Mission Options for All Target Destinations

Limits in ground based test facilities to achieve relevant conditions for some steep and high latitude entries. This issue applies to any TPS concept, not just HEEET.
TPS sizing is the process for determining the thickness of the TPS.

Bondline is the interface between the inner surface of the TPS (IML) and the structure to which it is typically adhesively bonded.

For single layer TPS, the constraint is not to allow the bondline to exceed the temperature limit of adhesive or structure.

Dual Layer TPS introduces a new constraint, not to allow the insulation layer to be exposed.

Current HEEET implementation requires uniform TPS thickness for both layers.

Max thickness for each layer may occur at different body points and trajectories.

Sizing RL and IL independently and then stacking max RL thickness from one location on max IL thickness from another location is not mass efficient:
- Excess RL at some locations can serve as insulation.

More mass efficient to size IL after fixing RL to max sized thickness across all locations.
Example Sizing from a Venus Reference Mission

Sizing done at 9 locations on the heatshield
- Figure on left: RL and IL sized independently
- Figure on right: RL sized first; then IL sized while for fixed RL thickness

Taking advantage of the nonessential portion of RL thickness at locations that don’t drive RL sizing provides mass benefits
- 62% reduction in IL thickness, 19% reduction in areal mass

*Sizing and Margin Methodology for Dual-Layer Thermal Protection Systems, Mahzari and Milos, 15th International Planetary Probe Workshop*
Structural Test Campaign

- **Element Level Testing**
  - Material Properties and allowables
    - Different Layers
    - Gap Filler
    - Adhesives
    - Composite structure

- **Component Level Testing**
  - 4-pt Bend (LaRC)
  - LHMEL 4pt-Bend
    - Developed novel test approach
    - Adopted by Orion
  - Shock Testing (NTS)

- **Subsystem Testing (LaRC)**
  - 1m Engineering Test Unit (ETU)
Subsystem (ETU) Testing Overview

79 Total Strain Gages
For Test:
• 24 Biaxial
  – 17 on Reccession layer
  – 7 on Composite
• 17 Uniaxial
  – 14 on Composite
  – 3 on Ring
For Defect Tracking: 14 Uniaxial

Static Pressure Test in Autoclave

ETU in Thermal Vac Chamber

MDU Carrier Structure Proof Test
ETU Carrier Structure Proof Test
Pre-Integration

Integrate TPS on Carrier Structure

Static Pressure

Thermal-Vacuum

Static Point Load (Rd1)

Static Point Load (Rd2)

Point Load Locations

12 load locations are shown
23 total tests, 2 at each location minus nosecap

Pt 12: Under Closeout Plug
Final Technical Readiness Level (TRL) Self Assessment

Have we built high-fidelity prototypes that address scaling issues? Yes

Have we operated in relevant environments?
- Aerothermal (arc-jets) Yes
- Thermostructural (combined loading of flexures at LHMEL) Yes
- Structural (pressure, thermal-vacuum and point loads on 1 m ETU) Yes

Have we documented test performance demonstrating agreement with analytic predictions? Yes

HEEET system is assessed to be at TRL 6

Limitations
- Not at TRL 6 for thickness much greater than 2”
- Not at TRL 6 for applied environments above 5 bar and 3500 W/cm2
- No mission opportunity (except Jupiter) appears to require these levels

But don’t just take our word for it - HEEET Independent Review Board (IRB) Assessment:
- “The IRB concurs [...] that the overall objective of achieving TRL 6 has been completed”
Any Questions?