ANALYSIS OF THREE-FLUID, CROSSFLOW HEAT EXCHANGERS

by Noel C. Willis, Jr.
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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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ABSTRACT

The detailed behavior of three-fluid, crossflow heat exchangers has been investigated. The equations governing the two-dimensional temperature distributions of the three fluids have been derived and nondimensionalized. Performance characteristics have been determined for a wide range of operating parameters for single-pass heat exchangers. The performance of two-pass heat exchangers for both cocurrent and countercurrent flow has been studied for selected operating conditions. Results have been presented graphically in terms of the temperature effectiveness of the two outer fluids as functions of heat-exchanger size for sets of fixed operating conditions. Nondimensional operating parameters have been defined which allow an efficient presentation of the large volume of performance data required to represent a practical range of operating conditions. Sample problems are included to illustrate the use of the performance graphs for design applications.
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SUMMARY

The detailed behavior of three-fluid, crossflow heat exchangers has been investigated. The equations governing two-dimensional temperature distributions of the three fluids have been derived and nondimensionalized. The performance characteristics have been determined for a wide range of operating parameters for single-pass heat exchangers. Performance of two-pass heat exchangers for both cocurrent and countercurrent flow has been studied for selected operating conditions. Results have been presented graphically in terms of the temperature effectiveness of the two outer fluids as functions of heat-exchanger size for sets of fixed operating conditions. Interpolation techniques have been used to obtain performance data for intermediate values. Nondimensionalized operating parameters have been defined which allow an efficient presentation of the large volume of performance data required to represent a practical range of operating conditions. Sample problems are included to illustrate the use of the performance curves and the interpolation techniques.

An expression for overall effectiveness has been derived which compares the heat transferred by a particular exchanger with that transferred by one of infinite size. Isolated cases, corresponding to poor design, are cited in which the overall effectiveness may be greater than unity. This effect emphasizes the importance of using the temperature effectiveness of the two outer fluids as the primary design variables and the overall effectiveness as an auxiliary parameter.

A computer program has been developed for the study of both single- and multiple-pass heat exchangers. Output options are available for detailed studies of temperature distributions within a particular exchanger and for generation of performance data for a large number of heat exchangers.

INTRODUCTION

Considerable effort has been expended in previous investigations to define performance characteristics of heat exchangers involving energy transfer between two fluids. Now that industrial processes have been developed which require simultaneous heat exchange between more than two fluids, analytical techniques are needed to describe the performance of multifluid heat exchangers. One example of such a process is the large-scale production of oxygen in an air separation plant which requires heat exchange between oxygen, nitrogen, and air at very low temperatures. There are also
possibilities for combining several separate two-fluid heat-exchanging operations more economically in a single multifluid arrangement.

Several investigators (refs. 1 to 5) have pursued the problem of multifluid heat exchangers in parallel or counterflow in which only one physical dimension of the exchanger is considered. The purpose of this investigation is the detailed study of three-fluid heat exchangers in crossflow as a completely two-dimensional problem.

In this study, the performance of three-fluid crossflow heat exchangers is determined and presented graphically in terms of the temperature effectiveness of two of the fluids referred to the third fluid. The effectiveness is determined as a function of heat-exchanger size for sets of fixed operating conditions. The introduction of nondimensional operating variables reduces the volume of data required to represent a practical range of operating conditions. The number of boundary conditions for the temperatures is reduced from three to one by the introduction of a nondimensional inlet temperature parameter.

An expression for overall effectiveness is derived which compares the performance of a heat exchanger to that of an infinitely large exchanger operating at the same conditions. A study of the two-dimensional temperature distributions reveals circumstances in which the overall effectiveness may be greater than unity. This result implies that in a three-fluid, crossflow heat exchanger, total heat transfer is not always maximized by increasing the size of the exchanger.

Effectiveness factors are determined for a wide range of operating parameters for single-pass, three-fluid heat exchangers. Performance of multiple-pass, three-fluid heat exchangers for both cocurrent and countercurrent flow is studied for selected operating conditions.

Sample problems are used to illustrate the application of the effectiveness curves to heat-exchanger design problems. Since some of the performance data can be explained only in terms of the two-dimensional variation of the temperatures of each fluid, these problem solutions are also used to provide insight into the detailed behavior of the fluids within the heat exchangers.

The basic differential equations for the spatial distribution of the temperatures of the three fluids were solved numerically using a digital computer. A program is available for both single- and multiple-pass calculations. An automatic-integration step-size control was developed through the consideration of overall conservation of energy so that multiple cases may be run continuously with the optimum step size used for each individual case. Output options are available for a detailed study of spatial temperature distribution within the exchanger or for the determination of the overall performance using only the average exit temperatures and effectiveness values.
SYMBOLS

A \[ \frac{u_1,2X_o}{m_1c_p,1} \]

B \[ \frac{u_2,3X_o}{m_3c_p,3} \]

C \[ \frac{u_1,2X_o}{m_2c_p,2} \]

c_p \quad \text{specific heat of fluid}

c_{p,j} \quad \text{specific heat of fluid (j)}

D \[ \frac{u_2,3X_o}{m_2c_p,2} \]

E \[ \frac{Q_a}{Q_\infty} \quad \text{overall effectiveness} \]

K_1 \[ \frac{m_1c_p,1}{m_2c_p,2} \quad \text{capacity rate ratio for fluid (1)} \]

K_3 \[ \frac{m_3c_p,3}{m_2c_p,2} \quad \text{capacity rate ratio for fluid (3)} \]

M \quad \text{largest value of the set (A, B, C, D)}

\dot{m} \quad \text{mass flow rate of fluid}

NTU_1 \quad \text{number of transfer units of a heat exchanger referred to fluid (1) (equal to A)}

NTU_3 \quad \text{number of transfer units of a heat exchanger referred to fluid (3) (equal to B)}

\bar{Q} \quad \frac{Q}{m_2c_p,2(t_{1,i} - t_{2,i})} \quad \text{nondimensional heat-transfer rate}

Q_a \quad \text{total heat-transfer rate in a heat exchanger of finite size}
$Q_{\infty}$ \hspace{1cm} total heat-transfer rate in a counterflow heat exchanger of infinite size

$q_j$ \hspace{1cm} heat transferred to fluid (j) per unit time

$T$ \hspace{1cm} nondimensional temperature, $\frac{t - t_{2,i}}{t_{1,i} - t_{2,i}}$ (all subscripts listed for $t$ are applied to $T$ also)

$t$ \hspace{1cm} local temperature of fluid

$t_{1,3,\text{mix}}$ \hspace{1cm} inlet mixing temperature of fluids (1) and (3), $\frac{m_1 c_p_1 t_{1,i}^1 + m_3 c_p_3 t_{3,i}^3}{m_1 c_p_1 + m_3 c_p_3}$

$t_{2,e,\infty}$ \hspace{1cm} exit temperature of fluid (2) for an infinitely large heat exchanger

$t_{2,\text{max}(X=0)}$ \hspace{1cm} maximum value of $t_2$ along the y-axis for an infinitely large heat exchanger, $\frac{U t_{1,i} + t_{3,i}}{U + 1}$

$t_j$ \hspace{1cm} local temperature of fluid (j)

$t_j,e$ \hspace{1cm} exit temperature of fluid (j)

$t_j,\text{em}$ \hspace{1cm} average exit temperature of fluid (j)

$t_j,i$ \hspace{1cm} inlet temperature of fluid (j)

$U$ \hspace{1cm} conductance ratio, $\frac{u_{1,2}}{u_{2,3}}$

$u_{1,2}$ \hspace{1cm} overall conductance between fluids (1) and (2)

$u_{2,3}$ \hspace{1cm} overall conductance between fluids (2) and (3)

$X$ \hspace{1cm} nondimensional coordinate of heat-exchanger surface, $\frac{x}{X_0}$

$x$ \hspace{1cm} coordinate of heat-exchanger surface

$x_0$ \hspace{1cm} x-dimension of heat exchanger
\( Y \) non-dimensional coordinate of heat-exchanger surface, \( \frac{y}{y_o} \)

\( y \) coordinate of heat-exchanger surface

\( y_o \) y-dimension of heat exchanger

\( \Delta t_i \) inlet temperature parameter, \( \frac{t_{1,i} - t_{2,i}}{t_{3,i} - t_{2,i}} \)

\( \theta_1 \) temperature effectiveness of fluid (1), \( \frac{t_{1,i} - t_{1,em}}{t_{1,i} - t_{2,i}} \)

\( \theta_3 \) temperature effectiveness of fluid (3), \( \frac{t_{3,i} - t_{3,em}}{t_{3,i} - t_{2,i}} \)

Subscripts:

1 fluid (1)
2 fluid (2)
3 fluid (3)
c cold fluid
e exit (temperature)
em average exit (temperature)
h hot fluid
i' inlet
ident identical order
inv inverted order
j fluid (j); general or typical reference to fluid (1), (2), or (3)
m average value (of temperature normal to fluid flow direction (appendix A))
max maximum value
min minimum value
mix inlet mixing (temperature)
N number of integration step in x direction (appendix A)

Superscripts:
c corrected
p predicted

PROBLEM FORMULATION

Derivation of the Governing Equations for Three-Fluid, Crossflow Heat Exchangers

Figure 1 is a schematic representation of a single-pass, three-fluid, crossflow heat exchanger. Heat is transferred between the center fluid (2) and outer fluids (1) and (3); however, there is no heat directly transferred between the two outer fluids. The immediate objective is to determine the temperature distributions of the three fluids in the heat exchanger for a given size and operating condition. Once the temperature distributions are known, the heat transferred to each fluid may be calculated from average exit temperatures; subsequently, the performance of the heat exchanger may be evaluated.

In this investigation, the following simplifying assumptions have been made to reduce the complexity of the equations.

1. Steady flow exists for the three fluids.

2. Fluid properties are constant. This assumption is adequate where large differences do not exist between the temperatures of the fluid and the heat-transfer surface. In most cases, evaluation of properties at a mixed mean temperature is sufficient to correct for property variations. A discussion of the effect of temperature-dependent fluid properties may be found in reference 6.

3. For a particular surface, the local conductance is constant and equal to the overall conductance. This assumption is consistent with steady flow and constant fluid properties if entrance effects are neglected.

4. The heat exchanger is considered to be adiabatic. If the performance of any heat exchanger is degraded because of heat exchange with the surroundings, it can be insulated. Effects caused by such heat exchange are not of interest in this investigation.

5. The effects of longitudinal and lateral conduction in the heat exchanger are neglected. These effects are important if large temperature gradients exist and will reduce heat-exchanger effectiveness.
6. There is no lateral mixing in any fluid. This behavior is closely approxi-
mated in plate-fin heat exchangers and when flows are not baffled. This assumption
preserves the two-dimensional character of the problem. If mixing were assumed, the
analysis would be simplified considerably.

Under the previous assumptions, the governing equations for the temperature dis-
tributions in three-fluid, crossflow heat exchangers will be derived. Figure 2 rep-
resents the heat-transfer surface between fluids (1) and (2). For a properly designed
exchanger, outer fluids (1) and (3) will be either both hotter or both colder than the
center fluid (2). For purposes of discussion during this derivation, the center fluid is
arbitrarily assumed to be hotter than the two outer fluids; however, the resulting equa-
tions are independent of the assumed temperature levels.

In figure 2 the heat transferred per unit time into fluid (1) from fluid (2) across
the elemental area $dx \, dy$ is

$$dq_1 = u_{1,2}(t_2 - t_1)dx \, dy \quad (1)$$

where $t_1$ and $t_2$ are both functions of $x$ and $y$.

This expression may be equated to the energy increase per unit time of the ele-
ment of fluid (1) between $y$ and $y + dy$ as it moves from $x$ to $x + dx$, which is

$$dq_1 = c_p, 1 \left( \frac{m_1 \, dy}{y_0} \right) \frac{\partial t_1}{\partial x} \, dx \quad (2)$$

Introducing nondimensional coordinates $X = \frac{x}{x_0}$ and $Y = \frac{y}{y_0}$ and equating the above ex-
pressions for $dq_1$, the resulting differential equation is

$$\frac{\partial t_1}{\partial X} = \frac{u_{1,2} \, x \, y_0}{m_1 \, c_p, 1} \left( t_2 - t_1 \right) \quad (3)$$

Following a similar procedure for fluid (3) gives

$$\frac{\partial t_3}{\partial X} = \frac{u_{2,3} \, x \, y_0}{m_3 \, c_p, 3} \left( t_2 - t_3 \right) \quad (4)$$
A differential volume element of fluid (2) is bounded by two surfaces and is in thermal communication with both fluids (1) and (3). The energy transferred to this element of fluid (2) from the outer fluids is

\[ dq_2 = \left[u_{1,2}(t_1 - t_2) + u_{2,3}(t_3 - t_2)\right] dx \, dy \]  

(5)

As the elemental volume of fluid (2) between \( x \) and \( x + dx \) moves from \( y \) to \( y + dy \), its thermal energy increase may be expressed as

\[ dq_2 = c_p,2 \left(\frac{m_2 \, dx}{x_0}\right) \frac{\partial t_2}{\partial y} \, dy \]  

(6)

Equating these two expressions and introducing the nondimensional coordinates yields

\[ \frac{\partial t_2}{\partial Y} = \frac{u_{1,2} \, x \, y_0}{m_2 c_p,2} (t_1 - t_2) + \frac{u_{2,3} \, x \, y_0}{m_2 c_p,2} (t_3 - t_2) \]  

(7)

Three simultaneous partial differential equations have been derived which define the temperatures of each of the three fluids as functions of both space coordinates \( x \) and \( y \). The resulting equations are

\[ \begin{align*}
\frac{\partial t_1}{\partial X} &= A(t_2 - t_1) \\
\frac{\partial t_2}{\partial Y} &= C(t_1 - t_2) + D(t_3 - t_2) \\
\frac{\partial t_3}{\partial X} &= B(t_2 - t_3)
\end{align*} \]  

(8)
where

\[
\begin{align*}
A &= \frac{u_1,2x_{10}y_0}{m_1c_p,1} \\
B &= \frac{u_2,3x_{10}y_0}{m_2c_p,3} \\
C &= \frac{u_1,2x_{10}y_0}{m_2c_p,2} \\
D &= \frac{u_2,3x_{10}y_0}{m_2c_p,2}
\end{align*}
\]

(9)

and

\[
t_j = t_j(x, y)
\]

(10)

Under the assumptions of the problem, the nondimensional terms \( A, B, C, \) and \( D \) are constants which depend upon the heat-capacity rates of the fluids, the heat-exchanger dimensions, and the values of conductance at the two heat-transfer surfaces. When \( A, B, C, \) and \( D \) are specified, along with the inlet temperatures of the three fluids, the equations may be solved for \( t_1, t_2, \) and \( t_3 \) as functions of position throughout the heat exchanger.

Reduction of the number of boundary conditions. - To nondimensionalize the basic equations with respect to temperature \( t_j \), all temperatures can be referred to the inlet temperature of the center fluid \( t_{2,i} \) by subtracting \( t_{2,i} \) from the temperature \( t_j \) and dividing this quantity by the difference between the inlet temperatures of fluids (1) and (2), or by \( t_{1,i} - t_{2,i} \). The resulting equations are

\[
\begin{align*}
\frac{\partial T_1}{\partial X} &= A(T_2 - T_1) \\
\frac{\partial T_2}{\partial Y} &= C(T_1 - T_2) + D(T_3 - T_2) \\
\frac{\partial T_3}{\partial X} &= B(T_2 - T_3)
\end{align*}
\]

(11)
where

\[
\begin{align*}
T_1 &= \frac{t_1 - t_{2,i}}{t_{1,i} - t_{2,i}} \\
T_2 &= \frac{t_2 - t_{2,i}}{t_{1,i} - t_{2,i}} \\
T_3 &= \frac{t_3 - t_{2,i}}{t_{1,i} - t_{2,i}}
\end{align*}
\]  

(12)

The advantage of the above formulation is apparent when the boundary conditions are examined. They become

\[
\begin{align*}
T_1(X=0) &= 1 \\
T_2(Y=0) &= 0 \\
T_3(X=0) &= \frac{t_{3,i} - t_{2,i}}{t_{1,i} - t_{2,i}}
\end{align*}
\]  

(13)

The boundary conditions for any problem may be specified by a single quantity called the inlet temperature parameter

\[
\Delta t_i = \frac{t_{1,i} - t_{2,i}}{t_{3,i} - t_{2,i}}
\]  

(14)

This parameter is the ratio of the temperature levels of the two outer fluids referred to the temperature level of the center fluid. The third boundary condition becomes

\[
T_{3,i} = \frac{1}{\Delta t_i}
\]

The outer fluids may be numbered so that \( \Delta t_i \) varies between zero and unity. As an example, in the case of both outer fluids being hotter than the center fluid, fluid (1) is always the colder of the two hot fluids. When \( \Delta t_i \) is unity, \( t_{1,i} \) equals \( t_{3,i} \); and when \( \Delta t_i \) is very small, \( t_{3,i} \) is considerably greater than \( t_{1,i} \).
For example, consider two sets of inlet temperatures

\[
\begin{align*}
  t_{1,i} &= 300^\circ F \\
  t_{2,i} &= 100^\circ F \\
  t_{3,i} &= 500^\circ F
\end{align*}
\]

and

\[
\begin{align*}
  t_{1,i} &= 50^\circ F \\
  t_{2,i} &= 0^\circ F \\
  t_{3,i} &= 100^\circ F
\end{align*}
\]

In both cases, \( \Delta t_i \) equals 0.5, and the problems are equivalent in the foregoing non-dimensional formulation.

Now that the specification of the inlet temperatures has been reduced to a single parameter, any problem may be completely defined by the five quantities \( A, B, C, D, \) and \( \Delta t_i \).

Multiple-pass, three-fluid, crossflow heat exchangers. - The use of multiple passes has long been recognized as a possible method of improving heat-exchanger performance. The previous investigations reported in references 7 and 8 have considered the problem of multiple-pass, two-fluid, crossflow heat exchangers.

While the previous derivation and discussion has been applied to determining the temperature distributions in a single-pass heat exchanger, the basic procedure can also be applied to each pass of a multiple-pass heat exchanger. The extension of the analysis to multiple passes involves only the proper specification of boundary conditions for each pass for the several possible flow arrangements. The configuration for a two-pass, three-fluid, crossflow heat exchanger is illustrated in figure 3. This particular arrangement is called countercurrent. A cocurrent arrangement is obtained by reversing the indicated direction of fluid (2). The flow detail for each pass is the same as that illustrated in figure 1.
The solution of the cocurrent case is straightforward; the outlet temperatures of the first pass become inlet temperatures of the second pass, and so on, for all subsequent passes. The solution in any pass is independent of the solutions of all subsequent passes. The temperature distribution in any pass is found in the same manner as in the single-pass heat exchanger, with the exception that the initial temperature generally will not be constant along the inlet boundaries after the first pass.

The problem is somewhat more difficult for the countercurrent heat exchanger. Figure 4 represents the mathematical configuration for this case. The difficulty arises because the initial temperature distributions are not completely known for either pass. Using the terminology in reference 7, there are "outer" boundaries where the initial conditions for the whole exchanger are given in "inner" boundaries which are effectively common to the two passes. The inlet temperature for fluid (2) in pass 1 along an inner boundary is dependent upon the solution in pass 2. Since it is evident that the solution in pass 2 is dependent in turn on pass 1, some iterative scheme is suggested using assumed distributions along inner boundaries.

Following the basic scheme outlined in reference 7, an inlet value of $T_2$ is assumed for pass 1, and the resulting exit values of $T_1$ and $T_3$ are used as input for pass 2. The exit value of $T_2$ for pass 2 is used in the second calculation for pass 1. This iterative procedure is continued until the average exit values of $T_2$ for pass 2 (for consecutive iterations) differ by less than a given convergence criterion. For the calculations in this study, the convergence criterion selected was that the average values of $T_2$ for consecutive iterations would differ by less than 1 percent. Depending upon the particular case, the number of iterations required for convergence was from three to five.

For more than two passes, values of $T_2$ would have to be assumed on all inner boundaries where needed, the number of such boundaries being one less than the number of passes. Numerical calculations in this investigation were confined to two-pass heat exchangers.

Discussion of the numerical solution of the basic equations. - The equations have been solved numerically by a first-order, predictor-corrector integration scheme. A FORTRAN program has been developed for use with the IBM 7094 or Univac 1107/1108 computers. The program can handle single-pass and multiple-pass calculations. An automatic step-size control, governed by the values of certain input parameters, was developed so that a large number of cases could be run continuously with the optimum step size used for each individual case. Output options are available which allow the user to study either detailed temperature distributions or overall performance characteristics. The details of the numerical procedure are described in appendix A, and the computer program is discussed in appendix B.
RESULTS AND DISCUSSION

The performance of a two-fluid heat exchanger may be expressed by a single dependent variable which is a function of two independent variables. For example, the overall effectiveness can be expressed as a function of the number of transfer units NTU of the heat exchanger and the capacity rate ratios of the two fluids. An investigation of three-fluid heat exchangers requires consideration of two dependent variables and five independent variables.

Nondimensional Independent Variables

In the foregoing section entitled "Problem Formulation," it was noted that the five independent parameters which can be used to define a specific problem are A, B, C, D, and Δt. However, these are not easily associated with the physical variables of the problem.

To specify a particular problem in terms of quantities which are more useful to a designer, the quantities A, B, C, and D may be combined into a new set of parameters which are more amenable to physical interpretation. The new parameters are

\[ NTU_1 = A = \frac{u_{1,2} x_0 y_0}{\dot{m}_1 c_p, 1} \]  \hspace{1cm} (17)

\[ U = \frac{C}{D} = \frac{u_{1,2}}{u_{2,3}} \] \hspace{1cm} (18)

\[ K_1 = \frac{C}{A} = \frac{\dot{m}_1 c_p, 1}{\dot{m}_2 c_p, 2} \] \hspace{1cm} (19)

and

\[ K_3 = \frac{D}{B} = \frac{\dot{m}_3 c_p, 3}{\dot{m}_2 c_p, 2} \] \hspace{1cm} (20)

The constant A is retained as the basic size parameter and is called NTU, or the number of transfer units of the heat exchanger referred to fluid (1). This parameter represents the ability of the heat exchanger to change the temperature of fluid (1). A large value of NTU can result from a large physical size \( x_0 y_0 \), a high conductance...
between fluids (1) and (2) \( u_{1,2} \) and a small capacity rate for fluid (1) \( \dot{m}_1 c_p, 1 \). All of these factors would make fluid (1) relatively easy to heat or cool. Therefore, the non-dimensional input parameter \( \text{NTU}_1 \) is a good representation of the size of the exchanger. Since a similar parameter based on either fluid (2) or (3) also could have been defined, the choice of fluid (1) as a reference for size is arbitrary. For example, a size parameter based on fluid (3) could have been defined as \( \text{NTU}_3 = \frac{u_{2,3} x_0 y_0}{\dot{m}_3 c_p, 3} \), which is equal to the quantity \( B \).

The parameters \( K_1 \) and \( K_3 \) are nondimensional heat-capacity flow rates of the outer fluids (1) and (3) referred to the center fluid (2) and will be called capacity rate ratios. For a well-designed heat exchanger, the combined heat-capacity flow rates of the outer two fluids should not be significantly different from the capacity flow rate of the center fluid. This implies that \( K_1 + K_3 \) should be near unity for proper design.

The parameter \( U \) is called the conductance ratio, and indicates the relative ability of fluids (1) and (3) to transfer heat to fluid (2).

Problems may be specified now by the five independent parameters \( \text{NTU}_1, K_1, K_3, U, \) and \( \Delta t \).

Discussion of Nondimensional Dependent Variables

The solution of the basic equations provides two-dimensional distributions of the temperatures of all three fluids throughout the heat exchangers. Some of the phenomena which occur in three-fluid heat exchangers can be explained only by a study of these detailed distributions. Particular examples will be discussed in later sections. However, the designer is interested mainly in the overall performance characteristics of the heat exchanger, for example, the average exit temperatures of the fluids.

The dependent variables chosen to represent the performance of three-fluid heat exchangers are the temperature effectivenesses of the two outer fluids. These variables are defined by the following expressions.

\[
\theta_1 = \left( \frac{t_{1,i} - t_{1,em}}{t_{1,i} - t_{2,i}} \right) \times 100\% \\
\theta_3 = \left( \frac{t_{3,i} - t_{3,em}}{t_{3,i} - t_{2,i}} \right) \times 100\%
\]

(21)
The quantities $t_{1,em}$ and $t_{3,em}$ are the average exit temperatures of fluids (1) and (3). They are obtained by averaging the local values for the exit temperatures obtained from the two-dimensional numerical integration of the basic equations.

The variables $\theta_1$ and $\theta_3$ represent the degree to which the temperatures of the outer fluids have approached the inlet temperature of the center fluid when they leave the heat exchanger. The effectiveness $\theta_1$ or $\theta_3$ will be 100 percent when the average exit temperature of fluid (1) or fluid (3) equals the inlet temperature of fluid (2). The effectiveness will be zero when there is no change in temperature. There are circumstances when one of the temperature effectivenesses actually can be negative. It has been assumed that for proper design, the center fluid (2) will either heat or cool both outer fluids. Consider the case for which $t_{1,i}$ and $t_{3,i}$ are both greater than $t_{2,i}$ and for which the function of the heat exchanger is to cool fluids (1) and (3). If the inlet temperature and heat capacity rates of fluid (3) are considerably greater than those of fluid (1), heat will be transferred through fluid (2) to fluid (1) in a large part of the heat exchanger. Fluid (1) will leave the heat exchanger at a temperature above its inlet value, the opposite of the desired effect. Therefore, a negative temperature effectiveness indicates that a fluid intended to be cooled was actually heated, or vice versa. A designer must use $\theta_1$ and $\theta_3$ to determine the effect of the heat exchanger on both fluids.

An auxiliary dependent variable, the overall effectiveness, has been defined to compare the performance of a particular heat exchanger to one of infinite size. The overall effectiveness is $E = \frac{Q^a}{Q^\infty}$ where $Q^a$ is the total heat transferred by an exchanger under fixed operating conditions and $Q^\infty$ is the heat that would be transferred by an infinitely large counterflow heat exchanger operating at the same conditions. It will be shown in a succeeding section that the maximum heat transfer does not necessarily occur for an infinitely large heat exchanger and that with the previous definition, the overall effectiveness can actually be greater than unity.

Method of Presentation of Results

The independent variables $\theta_1$, $\theta_3$, and $E$ are functions of the independent, dimensionless exchanger parameters $K_1$, $K_3$, NTU, $U$, and $\Delta t_i$. Since much heat-exchanger design work involves sizing an exchanger for a particular application, the performance factors $\theta_1$, $\theta_3$, and $E$ are presented as functions of NTU for fixed $K_1$, $K_3$, and $U$ with $\Delta t_i$ as a parameter. Results for single-pass exchangers are presented in figures 5 to 31 and results for two-pass exchangers in figures 32 to 37.

Single-Pass Results

A range of values for the independent variables has been chosen to cover a realistic spectrum of operating conditions for the single-pass calculations. The variation
of the inlet temperature parameter can be confined to the range 0 to 1 by appropriately numbering the fluids. For example, in the case for which \( t_{1,i} \) and \( t_{3,i} \) are greater than \( t_{2,i} \), \( \Delta t_i \) will always be 1.0 or less if the colder of the two outer fluids is designated as fluid (1). The conductance ratio \( U \) may vary from 0 to \( \infty \); however, the selected values of 0.5, 1.0, and 2.0 should be sufficient to cover the range of practical interest. The heat-capacity rate ratios \( K_1 \) and \( K_3 \) may also vary from 0 to \( \infty \); however, \( K_1 + K_3 \) must be reasonably close to unity for a balanced heat exchanger. Therefore, the values for \( K_1 \) and \( K_3 \) of 0.25, 0.5, and 1.0 should adequately cover the range of interest. The variation of \( NTU_1 \) from 0 to 7.5 is also sufficient to cover the range of practical sizes. The multiple-run option of the computer program was used to determine performance factors for heat exchangers represented by all possible combinations of the following set of independent parameters.

\[
\begin{align*}
NTU_1 &= 0.25 \quad NTU_1 &= 0.50 \quad NTU_1 &= 1.0 \\
NTU_1 &= 2.0 \quad NTU_1 &= 3.0 \quad NTU_1 &= 5.0 \quad NTU_1 &= 7.5 \\
K_1 &= 0.25 \\
K_1 &= 0.50 \\
K_1 &= 1.00 \\
K_3 &= 0.25 \\
K_3 &= 0.50 \\
K_3 &= 1.00
\end{align*}
\]
\[ U = 0.50 \]
\[ U = 1.00 \]
\[ U = 2.00 \]

and

\[ \Delta t_i = 0.25 \quad \Delta t_i = 0.50 \]
\[ \Delta t_i = 0.75 \quad \Delta t_i = 1.00 \]

This set of parameters required 756 separate calculations of the two-dimensional variations of all three-fluid temperatures. The printout option which restricted the output to the overall performance factors \( \theta_1 \), \( \theta_3 \), and \( E \) was used. Automatic step-size control was used to obtain the required accuracy and to minimize computation time.

In the previous set of independent parameters there are three values each for \( K_1 \), \( K_3 \), and \( U \); therefore, there are 27 resulting performance charts for single-pass heat exchangers. Even with this many charts, only discrete values of the independent parameters are represented. The succeeding section entitled "Application of Performance Curves for Design" presents an interpolation technique for investigating problems defined by intermediate values of these parameters.

The general trends of the data presented in figures 5 to 31 are similar to most heat-exchanger performance data with some exceptions. In most cases, the effectiveness factors increase with size, rapidly at first, then more slowly tending to some upper limit. This is always true for \( E \) and \( \theta_3 \); however, in some cases \( \theta_1 \) begins to decrease as size increases and even becomes negative at times (fig. 11, for example). This effect may be explained as follows. Assuming an original intent to cool fluids (1) and (3), fluid (1) will be the coolest of the hot fluids. When \( \theta_1 \) decreases as size increases, fluid (1) has been actually heated in some portion of the heat exchanger which has been added, thereby reducing the effectiveness of the exchanger with respect to fluid (1). This occurs whenever fluid (2), by virtue of receiving heat from fluid (3), has been heated locally to a temperature greater than that of fluid (1). This effect will be discussed in detail in the succeeding section entitled "Overall Effectiveness." Whenever the overall effect of the heat exchanger has been the heating of fluid (1) and the original intent was to cool fluid (1), the temperature effectiveness \( \theta_1 \) will be negative.

Other trends can be noted which may be interpreted in terms of physical variables. The patterns of behavior of the performance factors are dependent upon the relative size of the heat exchanger referred to fluids (1) and (3). When the size variable
NTU\textsubscript{1} was previously defined as \( \frac{u\textsubscript{1}, 2 x_o y_o}{m\textsubscript{1} c_p, 1} = A \), it was also noted that a similar variable NTU\textsubscript{3} could be defined as \( \frac{u\textsubscript{2}, 3 x_o y_o}{m\textsubscript{3} c_p, 3} = B \). These parameters are measures of the ability of the heat exchanger to heat or cool fluid (1) or (3) per degree of temperature difference between that of fluid ((1) or fluid (3)) and fluid (2).

The key to interpreting the behavior of the performance factors is the relative magnitude of \( A \) and \( B \). Different patterns are noted for \( A > B \), \( A = B \), and \( A < B \). In terms of the variables used in the performance charts, these criteria become \( \frac{K\textsubscript{1}}{K\textsubscript{3}} < U \), \( \frac{K\textsubscript{1}}{K\textsubscript{3}} = U \), and \( \frac{K\textsubscript{1}}{K\textsubscript{3}} > U \). From the definition of the previous parameters, \( \frac{K\textsubscript{1}}{K\textsubscript{3}} = U \).

The performance curves which fall under the above classifications are \( \frac{K\textsubscript{1}}{K\textsubscript{3}} < U \), \( A > B \) (figs. 7, 9, 10 to 13, 19, 21, 22, and 31); \( \frac{K\textsubscript{1}}{K\textsubscript{3}} = U \), \( A = B \) (figs. 6, 8, 16, 18, 20, 28, and 30); and \( \frac{K\textsubscript{1}}{K\textsubscript{3}} > U \), \( A < B \) (figs. 5, 14, 15, 17, 23 to 27, and 29). In cases where \( A = B \), the ability of the exchanger to heat or cool fluids (1) and (3) depends only on the temperature differential with the center fluid. When the inlet temperatures \( t\textsubscript{1, i} \) and \( t\textsubscript{3, i} \) are equal (\( \Delta t\textsubscript{i} = 1 \)), \( \theta\textsubscript{1} \) and \( \theta\textsubscript{3} \) are identical. For smaller values of \( \Delta t\textsubscript{i} \), the temperature differential between fluids (3) and (2) is greater than that between fluids (1) and (3). The result is that heat is more easily transferred to fluid (3), and \( \theta\textsubscript{3} \) is always greater than \( \theta\textsubscript{1} \).

When \( A < B \), heat is transferred more easily to fluid (3) than to fluid (1). Therefore, in all cases when \( A < B \), \( \theta\textsubscript{3} \) will be higher than \( \theta\textsubscript{1} \), even for \( \Delta t\textsubscript{i} = 1 \). It should be recalled that fluid (3) has been numbered so that \( \Delta t\textsubscript{i} \) is never greater than unity.

There are two effects to consider when \( A \) is greater than \( B \), the relative size (NTU) and the temperature differential. The size effect tends to make \( \theta\textsubscript{1} \) greater than \( \theta\textsubscript{3} \). When \( \Delta t\textsubscript{i} = 1 \), \( \theta\textsubscript{1} \) will always be greater than \( \theta\textsubscript{3} \); however, as \( \Delta t\textsubscript{i} \) decreases,
the temperature differential between fluid (3) and fluid (2) becomes great enough to overcome the effect of $\text{NTU}_1$ being greater than $\text{NTU}_3$. The net result is that as actual size increases, $\theta_3$ eventually becomes greater than $\theta_1$, when $\Delta t_1$ is less than 1.0.

**Multiple-Pass Results**

Numerical results have been obtained for the performance of representative configurations of two-pass, three-fluid, crossflow heat exchangers.

For both the cocurrent and countercurrent cases there are several possibilities for the behavior of the fluids in the elbow sections of multiple-pass exchangers. A fluid may be completely mixed so that it enters one pass at a constant temperature — the average of the exit distribution from the other pass. The fluid may be completely unmixed in the elbow and approach the next pass with the identical temperature distribution with which it left the previous pass. Another possible condition would be no mixing in the elbow with a flow arrangement to invert the fluid prior to entering the next pass. Thus, for each fluid the following possibilities for the behavior in the elbow can be considered.

1. Mixed
2. Unmixed, identical order
3. Unmixed, inverted order

All possible combinations would give 27 different cases to consider for each set of input variables $K_1$, $K_3$, and $U$. To restrict the amount of data presented and still obtain an insight into the performance of three-fluid, multiple-pass, crossflow heat exchangers, numerical results have been obtained for a countercurrent exchanger under the conditions $K_1 = 0.5$, $K_3 = 0.5$, and $U = 0.5$, 1.0, and 2.0 with all fluids mixed in the elbows. To provide comparisons for some of the other possibilities, the following cases have been considered for $K_1 = 0.5$, $K_3 = 0.5$, and $U = 1.0$:

1. Cocurrent mixed
2. Countercurrent, unmixed identical
3. Countercurrent, unmixed inverted

Figures 32 to 37 are the performance curves for the preceding cases.

The size parameter $\text{NTU}_1$ for multiple-pass cases is $\text{NA}$ where $N$ is the number of passes and $A$, as previously defined, is $\frac{u_1, 2x_0v_0}{m_1c_p, 1}$. All other parameters are defined in the same manner as in the single-pass analysis.
To compare the performance of two-pass, countercurrent heat exchangers with single-pass exchangers operating at the same conditions, one can compare figures 17, 18, and 19 with figures 32, 33, and 34, respectively. Although all of the effectiveness terms are increased in the two-pass, countercurrent case, the most significant increases occur in $\theta_1'$ for the smaller values of $\Delta t_1$, particularly 0.25. To obtain a direct comparison, the results for $K_1 = 0.5$, $K_3 = 0.5$, $U = 1.0$, and $\Delta t_1 = 0.25$ are presented in figure 38.

It was noted previously in the case of the single-pass heat exchanger that for small $\Delta t_1$, the possibility existed for fluid (1) to be heated in some parts of the exchanger, although the original intent was to cool fluids (1) and (3). This effect was the result of fluid (2) being heated by fluid (3) to a level that exceeded the local temperature of fluid (1). This tendency is decreased by the use of multiple passes in a countercurrent arrangement. Fluid (1) may still be heated in pass 1; but in pass 2, fluid (3) has been cooled sufficiently so that it no longer heats fluid (2) above the level of fluid (1). The result is that fluid (1) is well cooled in pass 2; therefore, a significant increase in $\theta_1'$ is obtained for small $\Delta t_1$.

Figure 35 presents the performance factors for a two-pass cocurrent arrangement for $K_1 = 0.50$, $K_3 = 0.50$, and $U = 1.0$, with mixed flow in the elbows. This configuration is considerably less effective than the single-pass exchanger for similar conditions (fig. 18). The effect of the second pass was to reheat fluid (1) after it had been cooled in pass 1. The effectiveness decreased with an NTU greater than 2.0. These results for a specific case should not categorically condemn the multiple-pass, cocurrent arrangement, but they definitely illustrate the potential problem of reheating (or recooling) associated with this configuration.

Figure 36 represents the performance factors for a two-pass, countercurrent arrangement for $K_1 = 0.50$, $K_3 = 0.50$, and $U = 1.0$ for unmixed, identical-order flow in the elbows. Figure 37 represents a similar case for inverted flow; and figure 33, for mixed flow. Inspection of the curves indicates that all performance factors are highest for inverted order and lowest for identical, with mixed being slightly above identical. The differences are most pronounced for $\theta_1'$, when $\Delta t_1 = 0.25$. Differences in overall effectiveness are slight; for example, for NTU = 4.0, $E_{\text{inv}} = 78$ percent, $E_{\text{mix}} = 76$ percent, and $E_{\text{ident}} = 75$ percent. However, for $\Delta t_1 = 0.25$, $\theta_1', \text{inv} = 45$ percent, $\theta_1', \text{mix} = 39$ percent, and $\theta_1', \text{ident} = 37$ percent for NTU = 4.0. Again, general conclusions may not be drawn from this specific case. The case does indicate that the differences between the three possibilities for flow in the elbow are worth considering in design and may significantly affect some of the performance factors of the exchanger.

Figure 39 is an illustration of the convergence of $T_{2,1}$ to pass 1 for the case of countercurrent flow with the inverted order $K_1 = 0.5$, $K_3 = 0.5$, $U = 1.0$, NTU = 3.0, and $\Delta t_1 = 0.25$. Four iterations were required. The initial estimate for
OVERALL EFFECTIVENESS OF THREE-FLUID, CROSSFLOW HEAT EXCHANGERS

It is useful to define a parameter which compares the performance of a particular heat exchanger to a counterflow heat exchanger of infinite heat-transfer area operating at the same conditions. While the temperature effectivenesses $\theta_1$ and $\theta_3$ are of primary interest to the designer, the overall effectiveness provides additional insight into heat-exchanger performance. The following discussion presents some interesting properties of three-fluid, crossflow heat exchangers that are most easily recognized and explained in terms of overall effectiveness. The overall effectiveness has been previously defined as $E = \frac{Q_a}{Q_\infty}$ where $Q_a$ is the heat transferred by a particular exchanger and $Q_\infty$ is the heat transferred by an infinitely large counterflow exchanger operating at the same conditions. The heat transfer $Q_a$ is obtained from the solution of the basic equations and may be expressed as either

\[ Q_a = \dot{m}_2 c_p \left( t_2,_{em} - t_2,_{i} \right) \]  \hspace{1cm} (27)

or

\[ Q_a = \dot{m}_1 c_p \left( t_1,_{i} - t_1,_{em} \right) + \dot{m}_3 c_p \left( t_3,_{i} - t_3,_{em} \right) \]  \hspace{1cm} (28)

In nondimensional form the two previous expressions become

\[ \overline{Q}_a = \frac{Q_a}{\dot{m}_2 c_p \left( t_2,_{i} - t_2,_{em} \right)} = \frac{t_2,_{em}}{T_2,_{em}} \]  \hspace{1cm} (29)

or

\[ \overline{Q}_a = K_1 \left( 1 - T_1,_{em} \right) + K_3 \left( \frac{1}{At_1} - T_3,_{em} \right) \]  \hspace{1cm} (30)
Since there is some numerical inaccuracy in the computer program, $Q_a$ is equated to the average of these two quantities.

In deriving an expression for $Q_\infty$ for a three-fluid heat exchanger, it is instructive to consider a similar problem for a two-fluid heat exchanger, as illustrated in figure 40. In the two-fluid, counterflow case, the exit temperature of the fluid with the smaller capacity rate will approach the inlet temperature of the fluid with the larger capacity rate as the heat-transfer area becomes infinite. If the hot fluid is denoted by the subscript $h$ and the cold fluid by the subscript $c$, then for $\dot{m}_h c_p, h < \dot{m}_c c_p, c'$

$\text{t}_h, e = \text{t}_c, i'$; and for $\dot{m}_h c_p, h > \dot{m}_c c_p, c'$, $\text{t}_c, e = \text{t}_h, i'$. Therefore, the heat transfer for an exchanger of infinite area is

$$Q_\infty = (\dot{m}_c c_p)_{\text{min}} (\text{t}_h, i - \text{t}_c, i)$$

Figure 41 depicts the analogous situation for three-fluid, counterflow heat exchangers. In the case for which the capacity rate of the center fluid is greater than the sum of the capacity rates of the outer fluids, the exit temperatures of the outer fluids both approach the inlet temperature of the center fluid.

For $(\dot{m}_1 c_p, 1 + \dot{m}_3 c_p, 3) < \dot{m}_2 c_p, 2'$, $\text{t}_1, e, \infty = \text{t}_3, e, \infty = \text{t}_2, i$ and

$$Q = \dot{m}_1 c_p, 1(\text{t}_1, i - \text{t}_2, 1) + \dot{m}_3 c_p, 3(\text{t}_3, i - \text{t}_2, i)$$. The equivalent nondimensional quantities for $(K_1 + K_3) < 1$ are

$$T_1, e, \infty = T_3, e, \infty = T_2, i = 0$$

and

$$\overline{Q}_\infty = \frac{Q_\infty}{\dot{m}_2 c_p, 2(\text{t}_1, i - \text{t}_2, i)} = K_1 + \frac{K_3}{\Delta t_i}$$

(33)

For the situation in which $(\dot{m}_1 c_p, 1 + \dot{m}_3 c_p, 3) > \dot{m}_2 c_p, 2'$, $\text{t}_2, e, \infty$ approaches a limiting value $\text{t}_2, e, \infty$ which lies somewhere between $\text{t}_1, i$ and $\text{t}_3, i'$. This limiting value should correspond to a single, effective inlet temperature of fluids (1) and (3). This effective inlet temperature is assumed to be the mixing temperature of fluids (1) and (3) defined as

$$t_2, e, \infty = t_1, 3, \text{mix} = \frac{\dot{m}_1 c_p, 1 t_1, i + \dot{m}_3 c_p, 3 t_3, i}{\dot{m}_1 c_p, 1 + \dot{m}_3 c_p, 3}$$

(34)
\[ Q_\infty = \dot{m}_2 c_p 2 (t_2, e, \infty - t_2, i) \] (35)

The equivalent nondimensional expressions for \((K_1 + K_3) > 1\) are

\[ T_{2, e, \infty} = \frac{K_1 T_{1, i} + K_3 T_{3, i}}{K_1 + K_3} = \frac{K_1}{K_1 + K_3} \]

(36)

and

\[ \frac{Q_\infty}{\dot{m}_2 c_p 2 (t_1, i - t_2, i)} = T_{2, e, \infty} = \frac{K_1 + 1}{K_3 + 1} \]

(37)

It should be noted that \(T_{2, e}\) depends only on the ratio \(\frac{K_1}{K_3}\) and \(\Delta t_1\) and is independent of \(U\).

To understand the variations of the overall effectiveness expression for three-fluid, crossflow heat exchangers, it is necessary to discuss the individual fluid temperature distributions for certain limiting situations. For two-fluid heat exchangers, the effectiveness can never be greater than 100 percent; however, using the above definition, there are isolated cases corresponding to poor design practice for which the overall effectiveness of a three-fluid heat exchanger in crossflow can actually exceed 100 percent. A specific sample will be used to explain the behavior of the fluids when \(E\) is greater than 100 percent and to show why this somewhat anomalous result corresponds to poor design practice. The case under consideration will be one of using the center fluid to cool the two outer fluids.

Values of effectiveness greater than 100 percent occur when \((K_1 + K_3) > 1\) and the configuration is such that \(T_{2, e, \infty}\) is greater than \(T_{2, e, \infty} = T_{1, 3, \text{mix}}\). Figure 42 represents the performance of a three-fluid, crossflow heat exchanger in terms of \(\theta_1\), \(\theta_3\), and \(E\) for \(K_1 = 2.0\), \(K_3 = 0.5\), and \(U = 2.0\). The value of \(E\) reaches a maximum of 101.5 percent at \(NTU_1 = 4\) for \(\Delta t_1 = 0.25\) and begins to decrease toward
100 percent as NTU$_1$ continues to increase. To understand why it is possible for $T_{2,e}$ to be greater than $T_{2,e,\infty}$, consider the distribution of $T_2$ along $X = 0$ from $Y = 0$ to $Y = 1.0$. Along this line, $T_1$ and $T_3$ are constant at their inlet values $T_{1,i}$ and $T_{3,i}$. Along the narrow strip at $X = 0$, fluids (1) and (3) act as infinite sources between which fluid (2) must flow. If the heat exchanger becomes infinitely large, there is a maximum temperature which fluid (2) may reach along the y-axis. Consider the case for $T_{3,i} > T_{1,i} > T_{2,i}$.

The maximum value of $T_2$ along the y-axis, $T_{2,\text{max}}(X=0)$, is reached when the heat flow rate into fluid (2) from fluid (3) is equal to heat flow rate from fluid (2) into fluid (1). This condition is expressed by

$$u_{1,2}(T_{2,\text{max}} - T_{1,i}) = u_{2,3}(T_{3,i} - T_{2,\text{max}})$$

Solving for $T_{2,\text{max}}$

$$T_{2,\text{max}}(X=0) = \frac{U T_{1,i} + T_{3,i}}{U + 1}$$

or since $T_{1,i} = 1$ and $T_{3,i} = \frac{1}{\Delta t_1}$

$$T_{2,\text{max}}(X=0) = \frac{U + \frac{1}{\Delta t_1}}{U + 1}$$

The value $T_{2,\text{max}}$ is a function of $\Delta t_1$ and $U$, and is independent of $K_1$ and $K_3$; therefore, $T_{2,\text{max}}$ is independent of $T_{2,e,\infty}$ for fixed $\Delta t_1$. If the value of $T_{2,\text{max}}$ is greater than $T_{2,e,\infty}(T_{1,3,\text{mix}})$, the effectiveness $E$ may be greater than 100 percent for sufficiently large values of NTU$_1$ (the size parameter).

Figure 43 illustrates the distribution of $T_1$, $T_2$, and $T_3$ along the y-axis for NTU$_1 = 7.5$. $T_1$ and $T_3$ are constant, and $T_2$ asymptotically approaches 2. For
\[ \Delta t_1 = 0.25 \text{ and } U = 2 \]

\[ T_{2, \text{max}}(X=0) = \frac{U + \frac{1}{\Delta t_1}}{U + 1} = \frac{2 + 4}{3} = 2 \]

Figures 44 to 47 illustrate the temperature distributions as functions of \( Y \) for \( X = 0.1, 0.25, 0.5 \) and 1.0. As \( X \) becomes larger, all fluids approach a nondimensional temperature of 1.6 at \( Y = 1.0 \). This is more clearly illustrated in figure 48 in which all temperatures are plotted versus \( X \) at \( Y = 1 \). For these conditions,

\[ T_{2, e, \infty} = T_{1, 3, \text{mix}} = \frac{K_1}{K_3 + \frac{1}{\Delta t_1}} = \frac{2}{0.5 + 0.25} = 1.6 \]

If the heat-exchanger size were made infinite, the exit temperature of fluid (2) would be \( T_{2, e, \infty} \) as defined previously, since the amount of fluid at a temperature greater than \( T_{2, e, \infty} \) would be negligible. For \( T_{2, \text{max}}(X=0) \) greater than \( T_{2, e, \infty} \), the overall effectiveness \( E \) will rise as \( \text{NTU}_1 \) increases, will reach a maximum value, and will decrease asymptotically to 100 percent as \( \text{NTU}_1 \) becomes infinite. If \( T_{2, \text{max}}(X=0) \) is less than \( T_{2, e, \infty} \), the average exit temperature of fluid (2) approaches \( T_{2, e, \infty} \) as a maximum, and \( E \) increases monotonically to 100 percent as \( \text{NTU}_1 \) becomes infinite.

Examining the behavior of \( \theta_1, \theta_3, T_1, \) and \( T_3 \) for this case, it can be seen that this behavior corresponds to poor design. The average temperature of fluid (1) is not affected and actually exceeds its inlet value at many points in the heat exchanger. Also, it can be seen that very little heat transfer is accomplished after \( X = 0.5 \), indicating a highly oversized exchanger.

This example should help emphasize the fact that while the overall effectiveness \( E \) is a very useful parameter, a designer should direct his attention to \( \theta_1 \) and \( \theta_3 \) to analyze effectively the actual performance of the exchanger.
The following tables will assist the designer in quickly identifying the cases for which \( T_{2, \text{max}} (X=0) \) is greater than \( T_{2, e, \infty} \):

\[
U + \frac{1}{\Delta t_i} = \frac{T_{2, \text{max}} (X=0)}{U + 1}
\]

(41)

<table>
<thead>
<tr>
<th>( U )</th>
<th>( \Delta t_i = 0.25 )</th>
<th>( \Delta t_i = 0.50 )</th>
<th>( \Delta t_i = 0.75 )</th>
<th>( \Delta t_i = 1.0 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.5</td>
<td>3.00</td>
<td>1.667</td>
<td>1.22</td>
<td>1.00</td>
</tr>
<tr>
<td>1.0</td>
<td>2.50</td>
<td>1.50</td>
<td>1.167</td>
<td>1.00</td>
</tr>
<tr>
<td>2.0</td>
<td>2.00</td>
<td>1.33</td>
<td>1.11</td>
<td>1.00</td>
</tr>
</tbody>
</table>

\[
T_{2, e, \infty} = \frac{K_1}{K_3 + 1} + \frac{1}{\Delta t_i}
\]

(42)

<table>
<thead>
<tr>
<th>( \frac{K_1}{K_3} )</th>
<th>( \Delta t_i = 0.25 )</th>
<th>( \Delta t_i = 0.50 )</th>
<th>( \Delta t_i = 0.75 )</th>
<th>( \Delta t_i = 1.0 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.25</td>
<td>3.40</td>
<td>1.80</td>
<td>1.267</td>
<td>1.00</td>
</tr>
<tr>
<td>1.0</td>
<td>2.50</td>
<td>1.50</td>
<td>1.167</td>
<td>1.00</td>
</tr>
<tr>
<td>2.0</td>
<td>2.00</td>
<td>1.33</td>
<td>1.111</td>
<td>1.00</td>
</tr>
<tr>
<td>4.0</td>
<td>1.60</td>
<td>1.20</td>
<td>1.067</td>
<td>1.00</td>
</tr>
</tbody>
</table>

Since \( T_{2, \text{max}} \) depends only on \( U \) and \( \Delta t_i \), and \( T_{2, e, \infty} \) depends only on the ratio \( \frac{K_1}{K_3} \) and \( \Delta t_i \), the preceding tables provide an easy means of checking the
possibility of $E$ being greater than 100 percent for a given problem. For the case previously discussed, $K_1 = 2.0$ and $K_3 = 0.5$; therefore, $\frac{K_1}{K_3} = 4.0$. For $\Delta t_1 = 0.25$, the table indicates $T_{2,e,\infty} = 1.6$. Since $U = 2.0$, the tables indicate $T_{2,\text{max}}(X=0) = 2.0$. Therefore, the possibility exists for an overall effectiveness greater than 100 percent, and there will eventually be a decrease in $E$ for an increase in size.

APPLICATION OF PERFORMANCE CURVES FOR DESIGN

A complete graphical presentation of performance data is not practical because of the large number of independent heat-exchanger variables. The approach used in this study is to obtain performance data for selected values of the variables $K_1$, $K_3$, $U$, and $\Delta t_1$ which bracket the range of practical interest and to develop interpolation techniques for intermediate values. While the data presented by the curves are limited, a fundamental understanding of three-fluid, crossflow heat exchangers may be obtained from them.

Three sample problems are solved below to demonstrate the application of the performance curves for design and to illustrate the physical significance of certain trends in the performance data which contribute to an understanding of the performance of three-fluid, crossflow heat exchangers.

Problem 1

This problem will illustrate the use of the performance curves when no interpolation is required. It is desired to predict the outlet temperatures of three fluids for a heat exchanger operating at the following conditions.

<table>
<thead>
<tr>
<th>Fluid</th>
<th>$\dot{m}$, lb/hr</th>
<th>$c_p$, Btu/lb/°F</th>
<th>$t_i$, °F</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>250</td>
<td>0.5</td>
<td>300</td>
</tr>
<tr>
<td>2</td>
<td>500</td>
<td>0.5</td>
<td>100</td>
</tr>
<tr>
<td>3</td>
<td>250</td>
<td>1.0</td>
<td>500</td>
</tr>
</tbody>
</table>

The surface conductances are $u_{1,2} = 50$ Btu/hr/ft$^2$/°F and $u_{2,3} = 25$ Btu/hr/ft$^2$/°F,
while the area $x_0 y_o$ is $5 \text{ ft}^2$. The resulting nondimensional independent variables are

$$
K_1 = \frac{\dot{m}_1 c_p, 1}{\dot{m}_2 c_p, 2} = 0.5 \quad K_3 = \frac{\dot{m}_3 c_p, 3}{\dot{m}_2 c_p, 2} = 1.0 \quad \Delta t_1 = \frac{t_{1, i} - t_{2, i}}{t_{3, i} - t_{2, i}} = 0.5
$$

$$
U = \frac{u_{1, 2}}{u_{2, 3}} = 2.0 \quad \text{NTU}_1 = \frac{u_{1, 2} x_0 y_o}{\dot{m}_1 c_p, 1} = 2.0
$$

Referring to figure 22, the resulting nondimensional dependent variables are $\theta_1 = 48$ percent, $\theta_3 = 30$ percent, and $E = 51$ percent. Average outlet temperatures $t_{1, \text{em}}$ and $t_{3, \text{em}}$ may be obtained using equations (44) and (45).

$$
\theta_1 = \left(\frac{t_{1, i} - t_{1, \text{em}}}{t_{1, i} - t_{2, i}}\right) \times 100 \text{ percent}
$$

(44)

$$
\theta_3 = \left(\frac{t_{3, i} - t_{3, \text{em}}}{t_{1, i} - t_{2, i}}\right) \times 100 \text{ percent}
$$

(45)

Thus, for $\theta_1 = 48$ percent, $t_{1, \text{em}} = 204^\circ \text{ F}$, and for $\theta_3 = 30$ percent, $t_{3, \text{em}} = 380^\circ \text{ F}$. The average exit value of $t_2$ may be obtained from an energy balance

$$
\dot{m}_1 c_p, 1 (t_{1, i} - t_{1, \text{em}}) + \dot{m}_3 c_p, 3 (t_{3, i} - t_{3, \text{em}}) = \dot{m}_2 c_p, 2 (t_{2, \text{em}} - t_{2, i})
$$

(46)

$$
125(300 - 204) + 250(500 - 380) = 250(t_{2, \text{em}} - 100)
$$

thus giving $t_{2, \text{em}} = 268^\circ \text{ F}$.

It is interesting to note the effect of increasing the size of the heat exchanger to $x_o y_o = 10 \text{ ft}^2$ or $\text{NTU}_1 = 4.0$. From figure 22, this change in area results in the following effectiveness factors: $\theta_1 = 46$ percent, $\theta_3 = 44$ percent, and $E = 66$ percent. Both $E$ and $\theta_3$ have increased; however, $\theta_1$ has decreased by 2 percent. This
decrease occurs because the increased size of the heat exchanger allows fluid (3) (hottest) to heat the center fluid (2) to a temperature greater than that of fluid (1) in some parts of the enlarged heat exchanger.

The dotted region in the sketch indicates the part of the heat exchanger in which fluid (2) is hotter than fluid (1). Since fluid (1) is being heated in the dotted region, an increase in size actually decreases the effectiveness of fluid (1). Fluid (1) is cooled for a smaller value of the coordinate Y. However, as fluid (2) moves through the exchanger, it is heated by both fluids (1) and (3). In the dotted region, heat transferred from the hotter fluid (3) increases the temperature of fluid (2) above that of fluid (1).

The detailed temperature distributions for fluids (1), (2), and (3) are presented in figures 49(a), 49(b), and 49(c) respectively. Figure 49(a) indicates that the temperature of fluid (1) is above its inlet value of 300°F in almost one-third of the heat exchanger. For values of Y less than 0.45, fluid (1) is always cooled as it flows in the X direction. For larger values of Y, fluid (1) is first heated and then cooled as it flows through the exchanger. The regions in which it is being heated correspond to the regions in which fluid (2), the "coolant" fluid, is actually hotter than fluid (1).

Figure 49(b) shows that fluid (2) flowing in the Y direction is heated at a very high rate along the Y-axis where the hot fluids enter the exchanger. The cooling rate decreases for larger values of X.

As indicated in figure 49(c), fluid (3) flowing in the X direction is cooled most rapidly along the X-axis where the coolant fluid (2) enters the exchanger. Since fluid (2) is heated as it passes through the exchanger, its ability to cool the outer fluids is decreased. This is illustrated by the isothermal lines for fluid (3) which indicate a decreasing cooling rate for increasing values of Y.
In figure 50, isothermal contours for all three fluids are superimposed. This figure may be used to determine the part of the heat exchanger in which the temperature of the coolant fluid (2) is actually greater than the temperature of fluid (1). This area corresponds to the dotted region.

Figures 49(a), 49(b), 49(c), and 50 graphically illustrate the cause of the reduction of effectiveness for an increase in size which may occur in some three-fluid, crossflow heat exchangers.

This phenomenon is most pronounced for a small $\Delta t_1$ (large $t_{3,i}$), a large capacity rate for fluid (3) (large $K_3$), and a small conductance ratio (large $u_{2,3}$). These factors contribute to a high heat-transfer rate from fluid (3) to fluid (2), with the possible result that fluid (1) is reheated in some part of the heat exchanger. In some cases, for example, $K_1 = 1.0$, $K_3 = 1.0$, and $\Delta t_1 = 0.25$ (figs. 29 and 31), the effect is so pronounced that fluid (1) is actually heated, and $\theta_1$ becomes negative as NTU increases. The preceding discussion has assumed an original intent to cool fluids (1) and (3) with fluid (2).

Problem 2

The conditions of problem 2 are chosen to illustrate how the performance curves may be used when the independent variables are not equal to those chosen for preparing the curves, namely, the combinations resulting from the values listed in the set of independent parameters presented in the section entitled "Single-Pass Results."

It is desired to determine the temperature effectiveness $\theta_1$ and $\theta_3$ for a heat exchanger operating under the following conditions: $K_1 = 0.40$, $K_3 = 0.75$, $U = 1.3$, $\Delta t_1 = 0.85$, and $\text{NTU}_1 = 2.0$.

Since these values of the independent variables do not correspond to those for which the performance curves have been prepared, a straightforward, graphical technique has been used. Figure 51 presents the temperature effectiveness $(\theta_1, \theta_3)$ as a function of the conductance ratio $U$ for $\text{NTU}_1 = 2.0$ and $\Delta t_1 = 0.85$. Nine curves are required to cover all possible combinations of $K_1$ and $K_3$. The data were obtained from the performance charts using visual interpolation for $\Delta t_1 = 0.85$. Points were obtained for the three values of $U$ used in the performance curves, namely, 0.5, 1.0, and 2.0. Figure 51 was used to determine $\theta_1$ and $\theta_3$ as functions for $K_3$ for $U = 1.3$ and $K_1 = 0.25$, 0.50, and 1.0. The results are plotted in parts (a), (b), and (c) of figure 52. These curves were used to determine $\theta_1$ and $\theta_3$ as functions of $K_1$ for $U = 1.3$ and $K_3 = 0.75$. Figure 52(d) may be used to determine $\theta_1$ and $\theta_3$ for $K_1 = 0.40$, $K_3 = 0.75$, $U = 1.3$, and $\Delta t_1 = 0.85$. Entering figure 52(d)
at $K_1 = 0.40$ gives $\theta_1 = 58$ percent and $\theta_3 = 41$ percent. The overall effectiveness $E$ could have been obtained in a similar manner; however, it is easier to return to the basic definition and calculate it as

$$\bar{Q}_a = K_1(1 - T_1, \text{em}) + K_3\left[\frac{1}{\Delta t_1} - T_3, \text{em}\right]$$

or

$$\bar{Q}_a = K_1\theta_1 + K_3\Delta t_1\theta_3 = 0.40(0.58) + 0.75(0.85)(0.41) = 0.492$$

Since $K_1 + K_3 > 1$

$$\bar{Q}_\infty = \left(\frac{1}{K_1 + K_3}\right)\left(K_1 + \frac{K_3}{\Delta t_1}\right) = 1.28 \frac{1}{1.15} = 1.11$$

therefore $E = \frac{\bar{Q}_a}{\bar{Q}_\infty} = 44$ percent. It is evident from examining figures 51 and 52 that linear interpolation is not adequate; hence, at least three points are needed on each curve. An additional point is available on curves which present $\theta_1$ and $\theta_3$ as a function of either $K_1$ or $K_3$ (fig. 52). Whenever $K_j$ approaches zero, $\theta_j$ approaches unity. Physically, this means that as the flow rate of a fluid becomes infinitely small, it can be cooled or heated very easily. It should also be noted that as $U$ becomes very large, $\theta_3$ will approach zero in figure 51. This trend reflects the physical consequence of $u_2, u_3$ approaching zero. Insulation of fluid (2) from fluid (3) will not alter the temperature. At first it may seem that $\theta_1$ should approach zero as $U$ becomes small; however, if $U$ approaches zero, $NTU_1 = \frac{x_0 y_0 u_1, 2}{m_1 c_p, 1}$ could no longer be 2.0 as presumed in the problem. Therefore, it is impossible to consider $U$ approaching zero for a finite, constant value of $NTU_1$.

When solving a problem where conditions do not correspond to those used in the performance curves, a set of figures similar to figures 51 and 52 must be prepared for every set of values for $NTU_1$ and $\Delta t_1$. 

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Problem 3

Problems 1 and 2 involved predicting output conditions for a given heat exchanger operating at specific input conditions. Problem 3 is one which is more frequently encountered by a designer: If the inlet conditions and capacity rates of the two outer fluids (1) and (3) are given, determine the size of the exchanger and the mass flow rate of the center fluid (2) that are required to produce specified outlet conditions for fluids (1) and (3).

Consider fluids (1) and (3) entering the exchanger at the following conditions.

\[
\begin{align*}
\dot{m}_1 &= 250 \text{ lb/hr} \\
\dot{m}_3 &= 250 \text{ lb/hr} \\
c_{p,1} &= 1.0 \text{ Btu/lb/}^\circ F \\
c_{p,3} &= 0.5 \text{ Btu/lb/}^\circ F \\
t_{1,i} &= 300^\circ F \\
t_{3,i} &= 500^\circ F
\end{align*}
\]

Coolant fluid (2) is available at \(T_{2,i} = 100^\circ F\) with \(c_{p,2} = 0.5 \text{ Btu/lb/}^\circ F\). Determine the NTU\(_1\) and \(\dot{m}_2\) required to cool both fluids to 220 F. These temperature changes correspond to the following values of effectiveness.

\[
\begin{align*}
\epsilon_1 &= \frac{t_{1,i} - t_{1,e}}{t_{1,i} - T_{2,i}} = \frac{300 - 220}{300 - 100} = 40 \text{ percent} \\
\epsilon_3 &= \frac{t_{3,i} - t_{3,e}}{t_{3,i} - T_{2,i}} = \frac{500 - 220}{500 - 100} = 70 \text{ percent}
\end{align*}
\]

Possible solutions may be found by studying the design curves for which \(\frac{K_1}{K_3} = 2.0\).

This condition is satisfied for two sets of curves: figures 15 to 17 for which \(K_1 = 0.5\) and \(K_3 = 0.25\) and figures 26 to 28 for which \(K_1 = 1.0\) and \(K_3 = 0.5\). For each of these sets of curves, a table may be prepared to investigate possible solutions. First, the effectiveness \(\epsilon_1\) is fixed at 40 percent and the number of transfer units NTU\(_1\) is
determined for each value of the conductance ratio \( U \). The values of \( \theta_3 \) at this value of \( \text{NTU}_1 \) are tabulated. A similar procedure is followed holding \( \theta_3 \) fixed at 70 percent and determining \( \theta_1 \). The object is to find a combination of \( U \) and \( \text{NTU}_1 \) for which \( \theta_1 \) and \( \theta_3 \) are as close to the desired values as possible. The following table is derived for this problem, for \( K_1 = 1.0 \) and \( K_3 = 0.5 \) (figs. 26 to 28).

\[
\begin{array}{|c|c|c|c|c|}
\hline
U & \theta_1 = 40 \text{ percent} & \theta_3 = 70 \text{ percent} \\
\hline
\text{NTU}_1 & \theta_3 & \text{NTU}_1 & \theta_1 \\
\hline
0.5 & 2.5 & 79 & 0.60 & 21 \\
1.0 & 2.5 & 75 & 1.0 & 30 \\
2.0 & 2.5 & 66 & 3.5 & 43 \\
\hline
\end{array}
\]

For \( U = 2.0 \), a value of \( \text{NTU}_1 \) between 2.5 and 3.5 should be acceptable. Figure 28 shows that for \( U = 2.0 \) and \( \text{NTU}_1 = 3.0 \), \( \theta_1 = 42 \) percent and \( \theta_3 = 68 \) percent, which is close enough for design purposes. For this condition the overall effectiveness \( E \) is 83 percent. The required value of \( \dot{m}_2 c_{p,2} \) is \( \frac{\dot{m}_1 c_{p,1}}{K_1} = 250 \text{ Btu/hr/}^{\circ}\text{F} \). Since \( c_{p,2} = 0.5 \text{ Btu/lb/}^{\circ}\text{F} \), the required \( \dot{m}_2 \) is 500 lb/hr.

It is still necessary to consider the case of \( K_1 = 0.5 \) and \( K_3 = 0.25 \). A similar table is prepared for \( K_1 = 0.5 \) and \( K_3 = 0.25 \) (figs. 14 to 16).

\[
\begin{array}{|c|c|c|c|c|}
\hline
U & \theta_1 = 40 \text{ percent} & \theta_3 = 70 \text{ percent} \\
\hline
\text{NTU}_1 & \theta_3 & \text{NTU}_1 & \theta_1 \\
\hline
0.5 & 0.85 & 85 & 0.40 & 23 \\
1.0 & .80 & 70 & .80 & 40 \\
2.0 & .75 & 45 & 1.80 & 57 \\
\hline
\end{array}
\]
In this case, the values for $U = 1.0$ give the desired result exactly for $NTU_1 = 0.80$. From figure 15 the overall effectiveness $E$ is 55 percent. The required value of $\dot{m}_2$ is 1000 lb/hr.

The two sets of conditions which satisfy the objectives of the problem are

\begin{align*}
NTU_1 &= 3.0 \\
\dot{m}_2 &= 500 \text{ lb/hr} \\
U &= 2.0 \\
E &= 83 \text{ percent}
\end{align*}

(53)

and

\begin{align*}
NTU_1 &= 0.80 \\
\dot{m}_2 &= 1000 \text{ lb/hr} \\
U &= 1.0 \\
E &= 55 \text{ percent}
\end{align*}

(54)

The choice facing the designer is between a large physical size with low flow rate and high effectiveness or small size, larger flow rate, and lower effectiveness. The ultimate choice must be based on factors such as construction, cost, space available, volume of coolant fluid available, and other design factors.

Not all problems which are approached in this manner will have an adequate solution. Consider a case which has the same conditions as the previous problem except that $\frac{K_1}{K_3}$ has the value 0.50 instead of 2.0. That is, assume that the hotter fluid has the higher capacity rate. Performance curves must now be considered for which $K_1 = 0.25$ and $K_3 = 0.50$ (figs. 8 to 10), and $K_1 = 0.50$ and $K_3 = 1.0$ (figs. 20 to 22). A chart is prepared as before for $K_1 = 0.25$ and $K_3 = 0.50$. 

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\[ a_{\theta_1} \] is always above \( \theta_3 \) for \( U = 2.0 \).

The trends indicate that there will be no satisfactory solution. For \( K_1 = 0.5 \) and \( K_3 = 1.0 \), \( \theta_3 \) never even reaches 70 percent. In this case, the performance curves indicate that the objectives of the problem are impossible under the imposed restrictions.

CONCLUDING REMARKS

Performance characteristics have been determined for a wide range of operating parameters for single-pass, three-fluid, crossflow heat exchangers. The performance of two-pass heat exchangers for both cocurrent and countercurrent flow has been studied for selected operating conditions. The results have been presented in terms of the temperature effectiveness of the two outer fluids as functions of heat-exchanger size for sets of fixed operating conditions.

Selected values have been chosen to bracket the range of practical interest because of the infinite possibilities for combinations of operating conditions. Interpolation techniques have been used to obtain performance data for intermediate values. Sample problems are included to illustrate the use of the performance curves and the interpolation techniques.

An expression for overall effectiveness has been derived which compares the heat transferred by a particular exchanger with that which is transferred by one of infinite size. Isolated cases corresponding to poor design are cited for which the overall effectiveness may be greater than unity. This indicates the importance of using the temperature effectiveness of the two outer fluids as the primary design variables and the overall effectiveness as an auxiliary parameter.

While data are necessarily limited to fixed sets of operating conditions, a fundamental understanding of three-fluid, crossflow heat exchangers may be obtained from the performance curves.
A computer program has been developed for the study of both single- and multiple-pass heat exchangers. Output options are available for detailed studies of temperature distributions within a particular exchanger and for generation of performance data for a large number of heat exchangers.

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National Aeronautics and Space Administration
Houston, Texas, November 17, 1967
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APPENDIX A

NUMERICAL PROCEDURE

Basic Logic

To determine the temperature distributions of each fluid in a three-fluid, cross-flow heat exchanger, the partial differential equations which must be solved simultaneously are

\[
\frac{\partial T_1}{\partial X} = A(T_2 - T_1) \quad (A1)
\]

\[
\frac{\partial T_2}{\partial Y} = C(T_1 - T_2) + D(T_3 - T_2) \quad (A2)
\]

\[
\frac{\partial T_3}{\partial X} = B(T_2 - T_3) \quad (A3)
\]

The region of solution of these nondimensionalized equations is the portion of the X-Y plane bounded by X = 0, X = 1, Y = 0, and Y = 1. The boundary conditions are \( T_1 = T_1(Y) \) and \( T_3 = T_3(Y) \) at \( X = 0 \) and \( T_2 = T_2(X) \) at \( Y = 0 \).
The basic logic for solution will be outlined before the details of the integration scheme are discussed.

1. The numerical integration of equations (A1) and (A3) could be initiated in the $X$ direction if $T_2$ were known along the $Y$-axis.

2. To obtain $T_2(0, Y)$, equation (A2) is integrated numerically in the $Y$ direction.

3. Using the initial values of $T_1$ and $T_3$ and the values of $T_2$ at $X = 0$ calculated in step 2, $T_1$ and $T_3$ can be calculated at $X = \Delta X$ using equations (A1) and (A3).

4. At $X = \Delta X$, the same situation exists as before: $T_1$ and $T_3$ are known and $T_2$ is to be calculated from equation (A2).

5. The above procedure is repeated at each increment $\Delta X$ until the solution is obtained over the entire region. The only difference in the initial integration step and all the other steps is that $T_1$ and $T_3$ are no longer constant along an $X = \text{constant}$ line.

Integration Scheme

The numerical technique used was devised as a first-order, predictor-corrector integration scheme. The solution of equation (A2) for $T_2(Y)$ at $X = X_N$ will be used to illustrate the procedure. Assume that $T_1', T_2, \text{ and } T_3$ are known at $X = X_N$, $Y = Y_N$ and the value of $T_2$ is desired at $Y = Y_N + \Delta Y$. It will be recalled, from the outline of the basic logic, that $T_1$ and $T_3$ are known along the line $X = X_N$ from $Y = 0$ to $Y = 1$. Equation (A2) is used to evaluate $\left(\frac{\partial T_2}{\partial Y}\right)_{Y_N}$ at $Y = Y_N$. This derivative will be denoted by $\left(\frac{\partial T_2}{\partial Y}\right)_{Y_N}$. A prediction of the value for $T_2$ at $Y = Y_N + \Delta Y$ is calculated from

$$T_2^P(Y_N + \Delta Y) = T_2(Y_N) + \Delta Y \left(\frac{\partial T_2}{\partial Y}\right)_{Y_N}$$

(A4)
This value of \( T_2^p \) is then used in equation (A2) along with the known values of \( T_1 \) and \( T_3 \) at \( Y = Y_N + \Delta Y \) to predict \( \frac{\partial T_2}{\partial Y} \) at \( Y = Y_N + \Delta Y \). This derivative will be denoted by \( \frac{\partial T_2}{\partial Y} \) \( Y_N+\Delta Y \). A corrected value of \( T_2 = T_2^c \) is calculated from

\[
T_2^c = T_2(Y_N) + \frac{1}{2} \left[ \left( \frac{\partial T_2}{\partial Y} \right)_{Y_N} + \left( \frac{\partial T_2}{\partial Y} \right)_{Y_N+\Delta Y} \right]
\]  
(A5)

This procedure can be shown to be equivalent to using a second order Taylor series expansion of the function \( T_2(Y) \) at the point \( Y_N \) with the required first derivatives \( \frac{\partial T_1}{\partial Y} \) and \( \frac{\partial T_3}{\partial Y} \) approximated by the slopes between \( Y_N \) and \( Y_N + \Delta Y \).

A similar procedure is used to solve equations (A1) and (A3) in the \( X \) direction. In the solution of these equations, \( T_2 \) is assumed to be constant over the interval \( \Delta X \) between \( X_N \) and \( X_N + \Delta X_N \) at the value \( T_2(X_N) \).

Accuracy Check

The accuracy of the computation may be checked at any \( x \) coordinate during the integration by comparing the energy gained (lost) by fluid (2) with that which is lost (gained) by fluids (1) and (3).

The calculation of the energy balance proceeds in the following manner:
At any station \(x_N\), \(t_1\), and \(t_3\) are averaged from \(y = 0\) to \(y = y_o\) while \(t_2\) is averaged from \(x = 0\) to \(x = x_N\). Conservation of energy requires

\[
\frac{\dot{m}_1 c_p}{\dot{m}_2 c_p} \left[ t_{1, i} - t_{1, m(x_N)} \right] + \frac{\dot{m}_3 c_p}{\dot{m}_2 c_p} \left[ t_{3, i} - t_{3, m(x_N)} \right] = \frac{\dot{m}_2 c_p}{\dot{m}_2 c_p} \left[ t_{2, m(x_N)} - t_{2, i} \right]
\]

(A6)

The coordinates \(\frac{x_N}{x_0}\) may be replaced by \(X_N\). Dividing equation (A6) by \(\frac{\dot{m}_2 c_p}{\dot{m}_2 c_p}\), the resulting equation is

\[
\frac{\dot{m}_1 c_p}{\dot{m}_2 c_p} \left[ t_{1, i} - t_{1, m(X_N)} \right] + \frac{\dot{m}_3 c_p}{\dot{m}_2 c_p} \left[ t_{3, i} - t_{3, m(X_N)} \right] = X_N \left[ t_{2, m(X_N)} - t_{2, i} \right]
\]

(A7)

Since \(\frac{\dot{m}_1 c_p}{\dot{m}_2 c_p} = K_1\) and \(\frac{\dot{m}_3 c_p}{\dot{m}_2 c_p} = K_3\), equation (A2) may be written

\[
K_1 \left[ t_{1, i} - t_{1, m(X_N)} \right] + K_3 \left[ t_{3, i} - t_{3, m(X_N)} \right] = X_N \left[ t_{2, m(X_N)} - t_{2, i} \right]
\]

(A8)

Dividing by \(t_{1, i} - t_{2, i}\) gives

\[
K_1 \left[ T_{1, i} - T_{1, m(X_N)} \right] + K_3 \left[ T_{3, i} - T_{3, m(X_N)} \right] = X_N \left[ T_{2, m(X_N)} \right]
\]

(A9)

Since the boundary conditions are \(T_{1, i} = 1\) and \(T_{3, i} = \frac{1}{\Delta t_i}\), the accuracy of the overall computation may be checked at any station \(X_N\) by comparing the quantities

\[
K_1 \left[ 1 - T_{1, m(X_N)} \right] + K_3 \left[ \frac{1}{\Delta t_i} - T_{3, m(X_N)} \right] \quad \text{and} \quad X_N \left[ T_{2, m(X_N)} \right]
\]

This comparison is used to determine the appropriate step size for the different calculations.
An examination of the basic equations

\[ \frac{\partial T_1}{\partial x} = A(T_2 - T_1) \]  \hspace{1cm} (A1)

\[ \frac{\partial T_2}{\partial y} = C(T_1 - T_2) + D(T_3 - T_2) \]  \hspace{1cm} (A2)

and

\[ \frac{\partial T_3}{\partial x} = B(T_2 - T_3) \]  \hspace{1cm} (A3)

would disclose the direct influence of \( A, B, C, \) and \( D \) on the calculation.

For large \( A, B, C, \) or \( D \), the temperature gradients will be large, and a smaller step size will be required to maintain acceptable accuracy. Since any of these constants is a nondimensional representation of the size of the heat exchanger, larger exchangers will require more calculational steps.

It was arbitrarily decided that an acceptable limit for accuracy would be that the two overall energy-balance terms would not differ from each other by more than 2 percent of their average value.

An automatic step-size control was used in the computer program because of the large number of cases which were needed to generate the performance curves. For any calculation, the largest value of the set \( (A, B, C, D) \) is denoted as \( M \). The following criteria for step size were established.

<table>
<thead>
<tr>
<th>( M )</th>
<th>( \Delta x, \Delta y )</th>
</tr>
</thead>
<tbody>
<tr>
<td>( M &gt; 20 )</td>
<td>0.002</td>
</tr>
<tr>
<td>( 7 &lt; M \leq 20 )</td>
<td>0.005</td>
</tr>
<tr>
<td>( 4 &lt; M &lt; 7 )</td>
<td>0.01</td>
</tr>
<tr>
<td>( 2 &lt; M &lt; 4 )</td>
<td>0.02</td>
</tr>
<tr>
<td>( 1 \leq M \leq 2 )</td>
<td>0.05</td>
</tr>
<tr>
<td>( M &lt; 1 )</td>
<td>0.10</td>
</tr>
</tbody>
</table>
In all cases, this set of criteria was sufficient to insure agreement of the energy balance within 2 percent, and the agreement was considerably better in the majority of cases.
A computer program has been developed to solve the basic differential equations using the numerical procedure described in appendix A. The program is capable of handling calculations for both single- and two-pass heat exchangers.

Since the program is written in FORTRAN, it can be run on the IBM 7094 or Univac 1107/1108 computers. The following pages contain a listing of the complete program.
PROGRAM MAIN

DIMENSION T1(1001), T2(1001), T3(1001), XAVE(14), X1(1001), XI(1001), XAVE(14), XI(1001), Y1(1001), Y1(1001), T1(1001), T2(1001), T3(1001), XAVE(14), XI(1001), Y1(1001), T1(1001), T2(1001), T3(1001), XAVE(14), XI(1001), Y1(1001), T1(1001), T2(1001), T3(1001)

COMMON /AB/ A, B, C, D, DTI

REAL K1, K3

KCOU = 0

READ (5, 16) (XAVE(KJ), KJ=1,14)
DO 40 JO=1,14
40 XAVE(JO) = XAVE(JO) -.001
IF (XAVE(1) .LT. 0.00001) XAVE(1) = 1.0
ZERO = 0
CALL RESET
CONTINUE
READ (5, 995) IPASS, ITYPE, INIX, IDENT, IPLOT, IPRINT, IALL

CONTINUE
READ (5, 16) K1, K3, DTI, A, U
C = A * K1
B = A * (K1/K3) * (1.0/U)
D = (K1/U) * A
WRITE (6, 1000)
IF (ITYPE .EQ. 1) WRITE (6, 1001)
IF (ITYPE .EQ. 2) WRITE (6, 1010) IPASS
IF (ITYPE .EQ. 3) WRITE (6, 1011) IPASS
IF (ITYPE .EQ. 4) GO TO 101
IF (ITYP .EQ. 1) WRITE (6, 1012)
IF (ITY .EQ. 1) WRITE (6, 1013)
IF (IDENT .EQ. 1) WRITE (6, 1014)
IF (IDENT .EQ. 1) WRITE (6, 1015)
CONTINUE

ACD = A
IF (ACD .LT. 0.0) ACD = B
IF (ACD .LT. C) ACD = C
IF (ACD .LT. D) ACD = D
NX = 500
IF (ACD .LE. 20.0) ACD = 0.0
IF (ACD .LE. 2.0) ACD = 0.0
NX = 200
NX = 100
IF (ACD .LT. 4.0) ACD = 0.0
IF (ACD .LT. 4.0) ACD = 0.0
NX = 50
IF (ACD .LT. 2.0) ACD = 0.0
IF (ACD .LT. 2.0) ACD = 0.0
NX = 20
IF (ACD .LT. 1.0) NX = 10
NY = NX
NX = NY + 1
MP1 = NX + 1
DELX = 1.0 / FLOAT(NX)
DELY = 1.0 / FLOAT(NY)
WRITE (6, 10010) K1, K3, U, DTI
WRITE (6, 10012) C, D
WRITE (6, 10161) DELX, DELY
CONTINUE
T11 = 1.0
T22 = 0.0
T33 = 1.0 / DT1
T2GUES = 0.5*( (K1+K3/DT1)/ (K1+K3) )
WRITE(6,100) T33
IF(I TYPE .EQ. 3) WRITE(6,28) T2GUES
IF(I TYPE .EQ. 3) T22 = T2GUES
IF(I PLOT .EQ. 0) GO TO 304
XII(1) = 0.0
YII(1) = 0.0
GO 41 IK=1, MP1
XII(IK+1) = XII(IK) * DELX
YII(IK+1) = YII(IK) * DELY
41 CONTINUE
304 CONTINUE
IAVE = 1
IF( IPASS .EQ. 1) IAVE = 0
WRITE(6,17)
INV = 0
DO 42 I=1,10
42 TN=1,10
I77 = 1
203 CONTINUE
IF(INV .EQ. 1) GO TO 200
DO 1 I=1,NN
1 T1(I) = T11
T2P(I) = T22
1 T3(I) = T33
200 X = 0.0
INV = 0
KX = 1
T2SUM = 0.0
IN xo = KCO(177,2)
IF(IPASS .EQ. 1) GO TO 3
WRITE(6,29) IN6
IF(IN xo .NE. 0) WRITE(6,21)
IF(IN xo .EQ. 0) WRITE(6,22)
3 DO 4 J=1,MP1
CALL AB1 (T1, T2, T3, DELY, NY , T2P(J) )
T2P(J) = T2(J,NN)
T2SUM = T2SUM + T2(J,NN)
KCOU = KCOU + 1
IF(KCOU .NE. IPRINT) GO TO 202
KCOU = 0
WRITE(6,111) X
WRITE(6,12)
WRITE(6,10) (T1 (K),K=1,NN)
WRITE(6,13)
WRITE(6,10) (T2(K),K=1,NN)
WRITE(6,14)
WRITE(6,10) (T3(K),K=1,NN)
202 CONTINUE
IF(XAVE(KK) .LT. 0.1) GO TO 371
IF(XAVE(KK) .LT. 0.1E-01) GO TO 18
IF(XAVE(KK) .GT. X) GO TO 18
IF(I ALL .EQ. 0) GO TO 310
371 CONTINUE
WRITE(6,111) X

45
WRITE(6,12)
WRITE(6,10) (J1(K),K=1,NN)
WRITE(6,13)
WRITE(6,10) (T2(K),K=1,NN)
WRITE(6,14)
WRITE(6,10) (T3(K),K=1,NN)

310  KK = KK + 1
    T25 = T2SUM / FLOAT(J)
    T1SUM = 0.0
    T3SUM = 0.0
    DO 19 IK=1,NN
        T1SUM = T1SUM + T1(IK)
    19   T3SUM = T3SUM + T3(IK)
    T1SUM = T1SUM / FLOAT(NN)
    T3SUM = T3SUM / FLOAT(NN)
    IF (IPLOT .NE. 1) GO TO 302
    CALL GUIKRL (-1, 0.0, 1.0, 0.0, 5.0, 1H1, BCDX, BCDY, N, YII, T1)
    CALL GUIKRL ( 0, 0.0, 1.0, 0.0, 5.0, 1H2, BCDX, BCDY, N, YII, T2)
    CALL GUIKRL ( 0, 0.0, 1.0, 0.0, 5.0, 1H3, BCDX, BCDY, N, YII, T3)
    302  CONTINUE
    WRITE(6,1021)
    WRITE(6,20) T1SUM, T25, T3SUM
    CON = K1 * (1.0 - T1SUM) + K3 * (1.0 / DT1 - T3SUM)
    XX22 = 0.0
    IF (ITYPE .EQ. 2) XX22 = T22
    CON = X * (T25 - XX22)
    IF (IKO .GE. 0) CONH = (T25 - T22) * X
    IF (IKO .LT. 0) CONH = K1 * (T11 - T1SUM) + K3 * (T33 - T3SUM)
    ACC = ADS(CONH-COM1) / (COMH-COM1) * 100.0
    IF (ITYPE .LE. 2) WRITE(6,1004) CON, CONH, ACC

18  CONTINUE
    X = X + DELX
    TIP(J) = T1(JN)
    TIP(J) = T3(JN)
    DO 2 I=1,NN
        DEL = DELX * A * (T2(J) - T1(I) )
        TIP = T1(I) + DEL
        TIP1 = DELX * A * (T2(J) - TIP1)
        T1(I) = (DEL*DELX)/G.5 + T1(I)
        DEL = DELX * B * (T2(J) - T3(I) )
        TIP = T3(I) + DEL
        TIP1 = DELX * B * (T2(J) - TIP1)
        2   T3(I) = T3(I) + (DEL*DELX)/G.5

4  CONTINUE
    CALL GUIKRL (-1, 0.0, 1.0, 0.0, 5.0, 1H1, BCDX, BCDY, N, YII, TIP)
    CALL GUIKRL ( 0, 0.0, 1.0, 0.0, 5.0, 1H2, BCDX, BCDY, N, YII, TIP)
    CALL GUIKRL ( 0, 0.0, 1.0, 0.0, 5.0, 1H3, BCDX, BCDY, N, YII, TIP)
    IF (X .GT. 1.0)
        CALL GUIKRL (-1, 0.0, 1.0, 0.0, 5.0, 1H1, BCDX, BCDY, N, YII, TIP)
    CALL GUIKRL ( 0, 0.0, 1.0, 0.0, 5.0, 1H2, BCDX, BCDY, N, YII, TIP)
    CALL GUIKRL ( 0, 0.0, 1.0, 0.0, 5.0, 1H3, BCDX, BCDY, N, YII, TIP)
    X = 1.0
311  CONTINUE
    T31 = 1.0 - T1SUM
    T32 = DT1 * T2S
    T33 = 1.0 - DT1*T3SUM
    C4 = K1 + K3
    WA = C5 * (COMH-COM1)
\[
\begin{align*}
\text{WHEN } & \ (\texttt{K1} + \texttt{K3} / \texttt{UTI}) * (1.0 / \texttt{GU}) \\
\text{IF } & \texttt{IX} \ LT. \ 1.0 \ \text{QMAX} = \texttt{K1} + \texttt{K3} / \texttt{DTI} \\
\text{E } & = \texttt{CANE} / \texttt{QMAX} \\
\text{WRITE} & (6,1065) \\
\end{align*}
\]

3000 CONTINUE

IF(\texttt{IX}, NE, 0) T25SS = T25
IF(\texttt{IAVE}, EQ, 0) GO TO 100
\texttt{IT} = \texttt{IT} + 1
IF(\texttt{IT}, LT, 2) GO TO 44
IF(\texttt{IMIX}, NE, 0) GO TO 46
\texttt{T}11 = \texttt{T}15
\texttt{T}22 = 0.0
\texttt{T}33 = \texttt{T}35
IF(\texttt{IITYPE}, EQ, 2) T22 = T23
GO TO 203

45 CONTINUE

\texttt{T}22 = T25
\texttt{T}11 = 1.0
\texttt{T}33 = 1.0 / \texttt{DTI}
IF(\texttt{IMIX}, EQ, 1) \texttt{INV} = 1
IF(\texttt{IDENT}, EQ, 0) GO TO 52
\texttt{INV} = 1
\texttt{DO} 9 \texttt{I55} = 1, \texttt{NN}
\texttt{T}1(\texttt{I55}) = \texttt{T}11
\texttt{T}3(\texttt{I55}) = \texttt{T}33
9 \texttt{THPPP} (\texttt{I55}) = \texttt{T}2P(\texttt{I55})
\texttt{DO} 91 \texttt{I55} = 1, \texttt{NN}
\texttt{I551} = \texttt{NN} - \texttt{I55} + 1
91 \texttt{T}2P(\texttt{I55}) = \texttt{THPPP} (\texttt{I551})
GO TO 42

46 CONTINUE
IF(\texttt{IDENT}, EQ, 0) GO TO 47
\texttt{DO} 49 \texttt{I55} = 1, \texttt{NN}
49 \texttt{THPPP} (\texttt{I55}) = \texttt{T}1(\texttt{I55})
\texttt{DO} 5 \texttt{I55} = 1, \texttt{NN}
\texttt{I551} = \texttt{NN} - \texttt{I55} + 1
5 \texttt{T}1(\texttt{I55}) = \texttt{THPPP} (\texttt{I551})
\texttt{DO} 6 \texttt{I55} = 1, \texttt{NN}
6 \texttt{THPPP} (\texttt{I55}) = \texttt{T}3(\texttt{I55})
\texttt{DO} 7 \texttt{I55} = 1, \texttt{NN}
\texttt{I551} = \texttt{NN} - \texttt{I55} + 1
7 \texttt{T}3(\texttt{I55}) = \texttt{THPPP} (\texttt{I551})
\texttt{DO} 8 \texttt{I55} = 1, \texttt{NN}
8 \texttt{T}2P(\texttt{I55}) = 0.0
\texttt{T}11 = \texttt{T}15
\texttt{T}22 = \texttt{T}25
\texttt{T}33 = \texttt{T}35
IF(\texttt{IITYPE}, EQ, 2) GO TO 56
GO TO 200
56 \texttt{DO} 57 \texttt{I55} = 1, \texttt{NN}
\texttt{I551} = \texttt{NN} - \texttt{I55} + 1
57 \texttt{T}2P(\texttt{I55}) = \texttt{T}2(\texttt{I551})
GO TO 200
52 \texttt{DO} 53 \texttt{KKO} = 1, \texttt{NN}
\texttt{T}1(\texttt{KKO}) = \texttt{T}11
TJ(KKO) = T3
IF( INIX .EQ. 1) INV = 1
GO TO 42
47 CONTINUE
IF(IATYPE .EQ. 2) GO TO 58
DO 48 IS = 1, NN
48 T2P(IS) = 0.0
GO TO 200
58 DO 59 KKO = 1, NN
59 T2P(KKO) = T2(KKO)
GO TO 200
44 CONTINUE
IF( IATYPE .LE. 2) GO TO 103
T1T(166) = T28
IF( 166 .EQ. 1) GO TO 43
IF( (ABS(TIT(166-1) - TIT(I66-1))/TIT(I66) .LT. 0.01) ) GO TO 103
T1T = 1.0
T2Z = T25
T35 = 1.0 / DTI
IF(IDENT .EQ. 0) GO TO 52
INV = 1
GO 102 IS = 1, NN
T1T(IS) = 1.0
T3(IS) = T33
102 TIPPP(IS) = T2P(IS)
DO 92 IS = 1, NN
92 TIPPP(IS) = TIPPP(IS - 1)
WRITE(6,23)
103 CONTINUE
WRITE(6,1022)
THE10 = 1.0 - T1SUM
THE30 = 1.0 - DTI * T3SUM
Q20 = T2S35
IF( IATYPE .EQ. 2) Q20 = T25
Q130 = K1 * (1.0 - T1SUM) + K3 * (1.0/DTI - T3SUM)
EO = (Q130 + Q20) * 0.5 / CMAX
ACC = ADS(T2K = 0.130) / (Q130 + Q20) * 100.0
QAVEO = (Q20 + Q130) * 0.5
WRITE(6,1004) Q130, Q20, ACC
IF(EO .LT. 1.0) WRITE(6,1003)
IF(EO .GE. 1.0) WRITE(6,1002)
A2 = A + A
WRITE(6,1024) OAVEO, QMAX, A2, EO, THE10, THE30
CALL TIME (ITIME)
IZERO = ITIME - IZERO
WRITE(6,1020) IZERO, ITIME
IZERO = ITIME
1029 FORMAT(10X,1DX,15MTIME FOR THIS CASE, 15,13H MICROSECONDS, //
1 11X,11INTOT TIME, 1B,13H MICROSECONDS )
WRITE(6,1005)
CALL DMPZUF
GO TO 1G0
1G FORMAT( 6(5X,E14.7) )
11 FORMAT(1HO,///,5X,4HX = ,F5.3 )
12 FORMAT(1HO,///,2X,16HT1(I), I = 1,N )
13 FORMAT(1HO,///,2X,16HT2(I), I = 1,N )
14 FORMAT(1HO,///,2X,16HT3(I), I = 1,N )
15 FORMAT(214, 611 )
16 FORMAT(1HO,10.2 )
17 FORMAT(1HO, ///, 5SX,14H>>> OUTPUT <<< )
20 FORMAT(1HO,4SX,24HTHE AVERAGE VALUE OF T1 = ,F8.3, / 41X,
  1 24HTHE AVERAGE VALUE OF T2 = ,F8.3, / 41X,
  2 24HTHE AVERAGE VALUE OF T3 = ,F8.3 )
21 FORMAT(1HO,5SX, 6H0CHAIN I )
22 FORMAT(1HO,5SX, 9H0CHAIN II )
23 FORMAT(1HO,2DX,45HTHE SYSTEM DID NOT CONVERGE IN 10 ITERATIONS)
20 FORMAT(1HO,4SX,24HT2 GUESS FOR DOMAIN I = ,F5.2)
25 FORMAT(1HO,5SX,10HITERATION ,12 )
55 FORMAT(12A6/12A6)
955 FORMAT(7211 )
1000 FORMAT(1HO, ///, 5SX,13H>>> INPUT <<< )
1001 FORMAT(1HO, ///, 59X,11HSINGLE PASS )
1002 FORMAT(1HO,2DX,35HX1 + K3 IS GREATER THAN OR EQUAL TO 1.0 )
1003 FORMAT(1HO,2DX,24HX5 + K3 IS LESS THAN 1.0 )
1004 FORMAT(1HO, ///, 35X, 44HFO4 ACCURACY CHECK ON ENERGY BALANCE COMPARE//
  1 20X, 6X013 = ,F8.3,13H WITH G2 = ,F8.3,5X,5HOR ,F7.4 ,
  2 18N PER CENT ACCURACY )
1005 FORMAT(1HO, ///, 12A6/12A6 )
1006 FORMAT(1HO, ///, 40X, 23H0BOUNDARY CONDITIONS / 43X ,
  1 9HT1 = 1.00,5X,8HT2 = 0.0,5X,5HT3 = ,F4.2 )
1007 FORMAT(1HO, ///, 59X,12H INPUT VALUES / 30X,4HA = ,F4.2,5X,5HK1 = ,
  1 F4.2,5X,5HK3 = ,F4.2,5X,4HU = ,F4.2,5X,11H0DELTA T1 = ,F4.2 ,
1008 FORMAT(1HO, ///, 40X, 30HTHE RESULTING VALUES OF B, C, AND D ARE /
  1 4DX, 4HB = ,F5.2, 5X, 4HC = ,F5.2, 5X, 4HD = ,F5.2 )
1010 FORMAT(1HO, ///, 51X, 15HMULTIPLE PASS ((12, 10H) PARALLEL FLOW )
1011 FORMAT(1HO, ///, 51X, 15H MULTIPLE PASS ((12, 17H) COUNTER FLOW )
1012 FORMAT(1HO, ///, 6X,15H0 )
1013 FORMAT(1HO, ///, 61X, 7H0 )
1014 FORMAT(1HO, ///, 37X, 14H0 )
1015 FORMAT(1HO, ///, 5X, 15H0 )
1016 FORMAT(1HO, ///, 50X,10H0DELTA X = ,F5.3, 5X,10H0DELTA Y = ,F5.3 )
1017 FORMAT(1HO, ///, 40X,4HDATA IS PRINTED OUT AT EACH CALCULATED POINT. )
1018 FORMAT(1HO, ///, 40X,4HDATA IS PRINTED OUT AT THE FOLLOWING VALUES OF X
1019 FORMAT( ///, 51X,2HX(12,4H) , , F3.3 )
1020 FORMAT(1HO, ///, 40X,14H0AVE = ,F8.3 , 10X,14H0MAX = ,F8.3 // 50X ,
  1 4MX = ,F8.3 / 30X,4HC = ,F8.3 ,10X,5H0THETA1 = ,F8.3 ,10X ,
2, 5H0THETA2 = ,F8.3 )
1021 FORMAT(1HO, ///, 33X,33H0THE AVERAGE EXIT TEMPERATURES ARE )
1022 FORMAT(1HO, ///, 41X,32HTHE OVERALL OUTPUT VARIABLES ARE)
1023 FORMAT(1HO, ///, 35X,44HFO4 ACCURACY CHECK ON ENERGY BALANCE COMPARE //
  1 20X, 7H015 = ,F8.3,14H WITH G0 = ,F8.3 ,5X,5HOR ,F7.4 ,
  2 18N PER CENT ACCURACY )
1024 FORMAT(1HO, ///, 35X, 6H0AVE = ,F8.3 ,10X,7H0MAX = ,F8.3 // 40X ,
  17NH01 = ,F6.3/2X,5H0E0 = ,F8.3,10X,10H0THETA0 = ,F8.3,10X ,
  2 10H0THETA30 = ,F8.3 )
END
SUBROUTINE AB1 (T1, T2, T3, DELY, NX, T2G)
COMMON /AB/ A, B, C, D, DT
DIMENSION T1(1001), T2(1001), T3(1001)
T2(1) = T2G
DO 1 N=1,NX
   DEL = DELY * (C*T1(N) + D*T3(N) - (C+D) * T2(N))
   TEMPT2 = T2(N) + DEL
   DEL1 = DELY * (C*T1(N+1) + D*T3(N+1) - (C+D) * TEMPT2)
1   T2(N+1) = T2(N) + (DEL+DEL1) * 0.5
RETURN
END
REFERENCES


BIBLIOGRAPHY


Figure 1. - Schematic representation of a single-pass, three-fluid heat exchanger in crossflow.
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$K_1 = 0.50$, $K_3 = 0.50$, and $U = 0.50$. 
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\[ NTU_1 \]
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$\theta_1$ and $\theta_3$ denote temperature effectiveness, $\bar{\theta}$, percent. $\Delta t_i$ represents various values such as $0.25$, $0.50$, $0.75$, $1.0$, and $1.0$. Overall effectiveness, $E$, percent, is also shown with $\Delta t_i$ values.
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Figure 44. - Temperature distributions as functions of $Y$ for $X = 0.10$. 

- $K_1 = 2.0$
- $K_2 = 0.5$
- $U = 2.0$
- $\Delta t_i = 0.25$
- $NTU_1 = 7.5$
Figure 45. - Temperature distributions as functions of $Y$ for $X = 0.25$. 
Figure 46. - Temperature distributions as functions of $Y$ for $X = 0.50$. 

$K_1 = 2.0$
$K_3 = 0.5$
$U = 2.0$
$\Delta t_1 = 0.25$
$NTU_1 = 7.5$
Figure 47. - Temperature distributions as functions of $Y$ for $X = 1.0$. 

- $K_1 = 2.0$
- $K_3 = 0.5$
- $V = 2.0$
- $\Delta t_1 = 0.25$
- $NTU_1 = 7.5$
Figure 48. - Temperature distributions as functions of $X$ for $Y = 1.0$. 

- $T_1 = 2.0$
- $K_3 = 0.5$
- $U = 2.0$
- $\Delta t_i = 0.25$
- $NTU_1 = 7.5$
<table>
<thead>
<tr>
<th>Fluid</th>
<th>( \dot{m}_r )</th>
<th>( c_p )</th>
<th>( t_j )</th>
<th>Notes</th>
</tr>
</thead>
<tbody>
<tr>
<td>(1)</td>
<td>250 lb/hr</td>
<td>0.5</td>
<td>300°F</td>
<td>( U_{1,2} = 50 \text{ Btu/hr/ft}^2/°F )</td>
</tr>
<tr>
<td>(2)</td>
<td>500 lb/hr</td>
<td>0.5</td>
<td>100°F</td>
<td>( U_{2,3} = 25 \text{ Btu/hr/ft}^2/°F )</td>
</tr>
<tr>
<td>(3)</td>
<td>250 lb/hr</td>
<td>1.0</td>
<td>500°F</td>
<td>( x_0 y_0 = 10 \text{ ft}^2 )</td>
</tr>
</tbody>
</table>

(a) Fluid (1).

Figure 49. - Isothermal contours.
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<table>
<thead>
<tr>
<th>Fluid</th>
<th>( \dot{m}_r ) lb/hr</th>
<th>( c_{p,r} ) Btu/lb°F</th>
<th>( t_{i,r} ) °F</th>
<th>( U_{1,2} = 50 \text{ Btu/hr/ft}^2/°\text{F} )</th>
<th>( U_{2,3} = 25 \text{ Btu/hr/ft}^2/°\text{F} )</th>
<th>( x_0 y_0 = 10 \text{ ft}^2 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>(1)</td>
<td>250</td>
<td>0.5</td>
<td>300</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>(2)</td>
<td>500</td>
<td>0.5</td>
<td>100</td>
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<tr>
<td>(3)</td>
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<td>1.0</td>
<td>500</td>
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</tbody>
</table>

Figure 49. - Continued.
<table>
<thead>
<tr>
<th>Fluid</th>
<th>( \dot{m}_r )</th>
<th>( c_p )</th>
<th>( t_i )</th>
</tr>
</thead>
<tbody>
<tr>
<td>(1)</td>
<td>250</td>
<td>0.5</td>
<td>300</td>
</tr>
<tr>
<td>(2)</td>
<td>500</td>
<td>0.5</td>
<td>100</td>
</tr>
<tr>
<td>(3)</td>
<td>250</td>
<td>1.0</td>
<td>500</td>
</tr>
</tbody>
</table>

\( U_{1,2} = 50 \text{ Btu/hr/ft}^2/\circ\text{F} \)
\( U_{2,3} = 25 \text{ Btu/hr/ft}^2/\circ\text{F} \)
\( x_0 y_0 = 10 \text{ ft}^2 \)

(c) Fluid (3).

Figure 49. - Concluded.
<table>
<thead>
<tr>
<th>Fluid</th>
<th>$\dot{m}_r$ (lb/hr)</th>
<th>$c_{pr}$ (Btu/lb/°F)</th>
<th>$t_i$ (°F)</th>
</tr>
</thead>
<tbody>
<tr>
<td>(1)</td>
<td>250</td>
<td>0.5</td>
<td>300</td>
</tr>
<tr>
<td>(2)</td>
<td>500</td>
<td>0.5</td>
<td>100</td>
</tr>
<tr>
<td>(3)</td>
<td>250</td>
<td>1.0</td>
<td>500</td>
</tr>
</tbody>
</table>

$U_{1,2} = 50$ Btu/hr/ft²/°F

$U_{2,3} = 25$ Btu/hr/ft²/°F

$x_0y_0 = 10$ ft²

Figure 50. - Isothermal contours for fluids (1), (2), and (3).
Figure 51. - Temperature effectiveness as a function of conductance ratio for $NTU_1 = 2.0$ and $\Delta t_1 = 0.85$. 
Figure 52. - Temperature effectiveness as a function of capacity-rate ratio for $u = 1.3$, $NTU_1 = 2.0$, and $\Delta t_1 = 0.85$. 
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—NATIONAL AERONAUTICS AND SPACE ACT OF 1958

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