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TRIANGULATION METHODS FOR AUTOMATED DOCKING

Prepared by:                John W. Bales, Ph. D.
Academic Rank:             Associate Professor
Institution and Department: Tuskegee University
                           Department of Mathematics

NASA/MSFC:

Directorate:                Science and Engineering
Laboratory:                 Astrionics
Division:                   Avionics Simulation
Branch:                     Orbital Systems and Robotics

MSFC Colleague:            Fred Roe, Jr.
Introduction

An automated docking system must have a reliable method for determining range and orientation of the passive (target) vehicle with respect to the active vehicle. This method must also provide accurate information on the rates of change of range to and orientation of the passive vehicle. The method must be accurate within required tolerances and capable of operating in real time.

The method being developed at Marshall Space Flight Center employs a single TV camera, a laser illumination system and a target consisting, in its minimal configuration, of three retro-reflectors. Two of the retro-reflectors are mounted flush to the same surface, with the third retro-reflector mounted to a post fixed midway between the other two and jutting at a right angle from the surface. For redundancy, two additional retro-reflectors are mounted on the surface on a line at right angles to the line containing the first two retro-reflectors, and equally spaced on either side of the post. (Figure 1) The target vehicle will contain a large target for initial acquisition and several smaller targets for close range.

There are other target configurations which might provide information on range and orientation [for example see Ref. 1, or see the cross-ratio of projective geometry, Ref. 2]. However, these configurations fail to provide reliable estimates of target yaw— the angle at which the target tilts away from the line of sight. With one of the three retro-reflectors mounted to a center post aligned (ideally) with the line of sight, reliable estimates of yaw angles may be computed.

This report will detail the mathematics required in the computation of accurate range and orientation measurements for a target configured as in Figure 1.

Detector Hardware Components

The target detector consists of a TV camera, frame grabber and associated computer. The camera contains a lens which focuses an image of the target onto an image plane. Located in the image plane is a rectangular array of individual photo-detectors called "picture elements" or "pixels". The amount of light falling on each individual pixel can be measured and digitized into a number of "grey levels" (in the case of a black and white image). The number of grey levels is typically a power of two, with 256 being the highest number of grey levels commonly used, and 2 being the least. The frame grabber is a digital device which takes successive "snapshots" of the image coming from the camera and stores these "frames" in a block of memory accessible to the associated computer. The computer is programmed to detect the target in the frame and compute the range and orientation of the target, and the related velocities.
Geometric Model of the Imaging System

For the purpose of analysis, the lens of the camera is modelled as a pinhole. In a pinhole camera, every object is in focus, regardless of its distance from the camera. For actual lenses, only objects at a given distance, determined by the lens equation, are in perfect focus. Points at other distances from the camera are imaged as "blur circles" whose diameters are proportional to the distance of the point from the ideal distance and to the lens diameter while inversely proportional to the focal length of the lens. The target detection system being developed, however, uses the centroids of detected images. In a statistical sense, the centroid of such an image should be the same whether or not it is in perfect focus. Thus, for purposes of geometrical analysis, the pinhole model is adequate.

While the image plane lies behind the lens at a distance $f$ equal to the focal length of the lens, an imaginary projected image plane may lie at any distance behind or in front of the lens. For ease of illustration, a projected image plane is frequently used. We will use a projected image plane lying a distance $f$ in front of the lens (Figure 2). A right-handed $xyz$ coordinate system is used, with the positive $x$-axis extending from $C$ through the center of the projected image plane, and with the positive $y$ and $z$-axes extending vertically upward and horizontally to the right, respectively.

Determination of Target Range

In Figure 3, $C$ denotes the geometrical center of the lens, $P_1', P_2', P_3'$ represent the retro-flectors in the target, and $P_1, P_2, P_3$ represent the respective points on the target and on the image plane. The symbols $\overrightarrow{P}_1', \overrightarrow{P}_2', \overrightarrow{P}_3', \overrightarrow{P}_1', \overrightarrow{P}_2', \overrightarrow{P}_3'$ represent the vectors from $C$ to the respective points on the target and on the image plane. The vector components of $\overrightarrow{P}_1', \overrightarrow{P}_2', \overrightarrow{P}_3'$ are, respectively, $(f, a_1, b_1), (f, a_2, b_2), (f, a_3, b_3)$. The magnitudes of the vectors $\overrightarrow{P}_1', \overrightarrow{P}_2', \overrightarrow{P}_3'$, representing the distances to the retro-reflectors, are $r_1, r_2, r_3$, respectively. The fixed distance from retro-reflector 1 (on the center post) to retro-reflectors 2 and 3 is $D$. The fixed distance between retro-reflectors 2 and 3 is $L$. The height of the center post is $H$. The angle between vectors $\overrightarrow{P}_1'$ and $\overrightarrow{P}_2'$ is $\theta_{12}$. The angle between vectors $\overrightarrow{P}_1'$ and $\overrightarrow{P}_3'$ is $\theta_{13}$. The angle between vectors $\overrightarrow{P}_2'$ and $\overrightarrow{P}_3'$ is $\theta_{23}$.

The coordinates of $\overrightarrow{P}_1', \overrightarrow{P}_2'$, and $\overrightarrow{P}_3'$ are determined directly from the output of the imaging system. The angles $\theta_{12}, \theta_{13}, \theta_{23}$ are determined by the relations

$$\cos \theta_{12} = \frac{\overrightarrow{P}_1' \cdot \overrightarrow{P}_2'}{||\overrightarrow{P}_1'||\overrightarrow{P}_2'||}$$
$$\cos \theta_{13} = \frac{\overrightarrow{P}_1' \cdot \overrightarrow{P}_3'}{||\overrightarrow{P}_1'||\overrightarrow{P}_3'||}$$

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Using the Law of Cosines, it is seen that

\[ r_1^2 + r_2^2 - 2r_1r_2 \cos \theta_{12} = D^2 \]
\[ r_1^2 + r_3^2 - 2r_1r_3 \cos \theta_{13} = D^2 \]
\[ r_2^2 + r_3^2 - 2r_2r_3 \cos \theta_{23} = L^2 \]

In general, a set of three quadratic equations in three variables can have as many as eight distinct solutions. In this case, however, there are at most four solutions where all values of the variables are positive, since, if \((r_1, r_2, r_3)\) is a solution, then so is \((-r_1, -r_2, -r_3)\). In point of fact, there are never more than three distinct all positive solutions. Three solutions occur when \(\theta_{12} = \theta_{13}\). If \(\theta_{12} \neq \theta_{13}\), then there are only two distinct solutions in which all three variables are positive. In either case, only one of the solutions has the reflector on the center post pointed toward the camera. The other solutions represent situations where the center post points away from the camera. Since such a target orientation would be undetectable, such a solution may be discarded.

In fact, the method of solution used by Marshall Space Flight Center avoids the necessity of computing all solutions and then rejecting some. It is assumed that the image of the point halfway between \(P_1'\) and \(P_3'\) (the base of the center reflector post) would lie at the point halfway between the images of those points in the image plane. While this assumption is not true, it is a good approximation in the case of the correct solution, and a bad approximation for the spurious solutions. Using an iterative routine (the Newton-Rafson method), the initial guess is improved upon until the system converges to the correct solution. The iterative routine also computes the pitch, roll and yaw of the target. This information, along with the range to the target, is updated and the corresponding rates of change are computed. All range, orientation and rate of change information is then passed along to the guidance routines so that necessary course corrections can be computed for the docking maneuver.

Alternate Solution Method

While the method described above is sufficient, the following method is presented for possible comparison of speed or accuracy.

Assuming that \(\theta_{12} \geq \theta_{13}\), Figure 4 represents the target geometry relative to the camera, with \(C\) representing the camera, and \(P_1', P_2',\) and \(P_3'\) representing the three retro-reflectors on the target. The segment \(P_1'A\) is perpendicular to \(CP_2'\). The segment \(P_2'D\) is perpendicular to \(CP_3'\). The segment \(P_3'B\) is perpendicular to \(CP_1'\).
\[ CP'2 = CA + P'2A. \] Likewise, \( CP'3 = CD + DP'3 \), and \( CP'_1 = CB - P'_1B. \) Using right triangle trigonometry, and using \( D \) and \( L \) as defined in the previous section, these three equations may be rewritten as follows:

\[
\begin{align*}
    r_2 &= r_1 \cos \theta_{12} + \sqrt{D^2 - r_1^2 \sin^2 \theta_{12}} \\
    r_3 &= r_2 \cos \theta_{23} + \sqrt{L^2 - r_2^2 \sin^2 \theta_{23}} \\
    r_1 &= r_3 \cos \theta_{13} - \sqrt{D^2 - r_3^2 \sin^2 \theta_{13}}
\end{align*}
\]

To solve for \( r_1, r_2, \) and \( r_3 \), one makes an initial guess that \( r_1 = \left( \frac{L}{2} \right) \cot \left( \frac{\theta_{23}}{2} \right) \), then iterates the equations. If \( \theta_{12} < \theta_{13} \), then the 2s and 3s in the above equations should be reversed.

**References**

