Advancements in Engineering Turbulence Modeling

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ABSTRACT

Some new developments in two-equation models and second order closure models will be presented. Two-equation models (e.g., $k$-$\varepsilon$ model) have been widely used in CFD for engineering problems. Most of low-Reynolds number two-equation models contain some wall-distance damping functions to account for the effect of wall on turbulence. However, this often causes the confusions and difficulties in computing flows with complex geometry and also needs an ad hoc treatment near the separation and reattachment points. In this paper, a set of modified two-equation models is proposed to remove abovementioned shortcomings. The calculations using various two-equation models are compared with direct numerical simulations of channel flows and flat boundary layers.

Development of second order closure model will be also discussed with emphasis on the modeling of pressure related correlation terms and dissipation rates in the second moment equations. All the existing models poorly predict the normal stresses near the wall and fail to predict the 3 dimensional effect of mean flow on the turbulence (e.g., decrease in the shear stress caused by the cross flow in the boundary layer). The newly developed second order near-wall turbulence model to be described in this paper is capable of capturing the near-wall behavior of turbulence as well as the effect of three dimension mean flow on the turbulence.
1. k-ε model

The two-equation model, especially k-ε model, is still the most widely used model for computing engineering flows. We first list some of the commonly used two-equation models,\[^1,2,4,5,6\] and their predictions on the fully developed channel flows and boundary layer flows compared with the corresponding direct numerical simulations. Then, we propose a modified k-ε model which does not contain any wall distance. The proposed k-ε model has been also tested using direct numerical simulation data.

The eddy viscosity $\nu_T$ is assumed in two-equation models as follows:

$$\nu_T = C_\mu f_\mu \frac{k^2}{\bar{\varepsilon}}$$

or

$$\nu_T = C_\mu f_\mu \tau$$

where $\tau = k^2/\bar{\varepsilon}$

The general k-ε (or k-τ) model equations are of the following forms:

$$k_{,t} + U_j k_{,j} = \left[ \left( \frac{\nu_T}{\sigma_k} + \nu \right) k_{,j} \right]_{,j} + \Pi + \nu_T (U_{i,j} + U_{j,i}) U_{i,j} - \epsilon + D$$

$$\epsilon_{,t} + U_j \epsilon_{,j} = \left[ \left( \frac{\nu_T}{\sigma_\epsilon} + \nu \right) \epsilon_{,j} \right]_{,j} + C_1 \frac{\epsilon}{k} \nu_T (U_{i,j} + U_{j,i}) U_{i,j} - C_2 f_2 \frac{\epsilon \bar{\varepsilon}}{k} + E$$

$$\tau_{,t} + U_j \tau_{,j} = \left[ \left( \frac{\nu_T}{\sigma_\tau} + \nu \right) \tau_{,j} \right]_{,j} + \frac{2}{k} \left( \frac{\nu_T}{\sigma_{r_1}} + \nu \right) k_{,i} \tau_{,i} \tau_{,i} - \frac{2}{\tau} \left( \frac{\nu_T}{\sigma_{r_1}} + \nu \right) \tau_{,i} \tau_{,i}$$

$$+ (1 - C_{s_1}) \frac{\tau}{k} \nu_T (U_{i,j} + U_{j,i}) U_{i,j} + (C_{s_2} f_2 - 1)$$
This table lists the model terms, damping functions and model constants appeared in various two-equation models.

<table>
<thead>
<tr>
<th>Model</th>
<th>$E$</th>
<th>$\epsilon$</th>
<th>$C_1$</th>
<th>$C_2$</th>
<th>$f_1$</th>
<th>$f_2$</th>
</tr>
</thead>
<tbody>
<tr>
<td>JL</td>
<td>$2\nu\nu_t(\frac{\partial u}{\partial y})^2$</td>
<td>$\epsilon$</td>
<td>1.45</td>
<td>2.0</td>
<td>1.0</td>
<td>$1 - \frac{3e(-R_l)}{R_l}$</td>
</tr>
<tr>
<td>LB</td>
<td>0</td>
<td>$\epsilon$</td>
<td>1.44</td>
<td>2.0</td>
<td>$1 + (\frac{R_l}{\nu})^2$</td>
<td>$1 - e(-R_l)$</td>
</tr>
<tr>
<td>Chien</td>
<td>$-\frac{2\nu t}{k^2}$</td>
<td>$\epsilon$</td>
<td>1.35</td>
<td>1.8</td>
<td>1.0</td>
<td>$1 - \frac{22e(-R_l/36)}{R_l}$</td>
</tr>
<tr>
<td>NH</td>
<td>$\nu\nu_t(1 - f_\mu)(\frac{\partial u}{\partial y})^2$</td>
<td>$\epsilon$</td>
<td>1.45</td>
<td>1.9</td>
<td>1.0</td>
<td>$1 - \frac{3e(-R_l)}{R_l}$</td>
</tr>
<tr>
<td>Shih</td>
<td>$\nu\nu_t(\frac{\partial u}{\partial y})^2$</td>
<td>$\epsilon - \frac{\nu t}{2k^2}\frac{(v_k)}{\partial z}$</td>
<td>1.45</td>
<td>2.0</td>
<td>1.0</td>
<td>$1 - \frac{22e(-R_l/36)}{R_l}$</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Model</th>
<th>$\Pi$</th>
<th>$D$</th>
<th>$f_\mu$</th>
<th>$\sigma_k$</th>
</tr>
</thead>
<tbody>
<tr>
<td>JL</td>
<td>0</td>
<td>$-2\nu(\frac{\partial u}{\partial y})^2$</td>
<td>$e^{\frac{\nu t}{1 + \frac{R_l}{\Pi}}}$</td>
<td>1.0</td>
</tr>
<tr>
<td>LB</td>
<td>0</td>
<td>0</td>
<td>$[1 - e^{(-0.025R_l)}] + (1 + \frac{0.5R_l}{\Pi})$</td>
<td>1.0</td>
</tr>
<tr>
<td>Chien</td>
<td>0</td>
<td>$-2\nu k/y^2$</td>
<td>$1 - e^{(-0.0155y^+)}$</td>
<td>1.0</td>
</tr>
<tr>
<td>NH</td>
<td>0</td>
<td>$-2\nu(\frac{\partial u}{\partial y})^2$</td>
<td>$[1 - e^{-y^+/26.5}]^2$</td>
<td>1.0</td>
</tr>
<tr>
<td>SAA</td>
<td>0</td>
<td>0</td>
<td>$(1 + \frac{3.45}{\sqrt{\nu t}})\tanh(\frac{y^+}{1.7})$</td>
<td>1.36</td>
</tr>
<tr>
<td>Shih</td>
<td>$\frac{0.5\nu k\nu_t}{\sigma_k f_\mu[1 - \exp(-y^+)]}$</td>
<td>0</td>
<td>$1 - e^{(-6 \times 10^{-3}y^+ - 4 \times 10^{-4}yp^+ + 2.5 \times 10^{-6}y^3 - 4 \times 10^{-9}y^4)}$</td>
<td>1.3</td>
</tr>
</tbody>
</table>

$$\nu_l = C_\mu f_\mu \frac{k^2}{\epsilon} \quad y^+ = \frac{u+}{\nu} \quad R_l = \frac{k^2}{\nu \epsilon} \quad R_k = \frac{\sqrt{\nu t}}{\nu}$$
The following figures show the predictions on fully develop channel flow using various two-equation models compared with the direct numerical simulation data. Plotted quantities include the mean velocity $U$, turbulent shear stress $(uv)$, turbulent kinetic energy $k$ and dissipation rate $\epsilon$. The open circle represents direct numerical simulation, and the solid line represents the model prediction.
The figures below show the model predictions on flat plate boundary layer flow. A direct numerical simulation of boundary layer flow is used for comparison. The skin friction coefficient $C_f$ is also included in the comparisons.
Overall, Shih's k-ε model gives better prediction in both fully developed channel flows and flat plate boundary layer flows according to the comparisons with corresponding direct numerical simulations. However, this model has the same problem as the others, that is it contains the wall distance parameter \( y^+ \), which is defined as

\[
y^+ = \frac{u_r y}{\nu}
\]

where \( u_r \) is the friction velocity. The difficulty would occur in some situations. For example, near the separation point \( u_r \) approaches zero and hence \( \nu_t \) (through \( f_\mu(y^+) \)) will approach zero everywhere when this \( u_r \) is used. Another example is the flow with complex geometry that the wall distance is not well defined. In the both cases, the ad hoc treatment is needed in the model implementation. We notice that Jonse-Launders's model\(^1\) does not contain \( y^+ \). However, its present form does not perform very well in the simple testing flows. Here, we based on the Shih's k-ε model modify the parts which is related the \( y^+ \) with another parameter \( R = \frac{k^{3/2} \sqrt{\nu}}{\nu} \). \( R \) is a ratio of turbulence length scale to viscous length scale. The modifications\(^9\) made here are:

\[
f_\mu = 1 - \exp \left\{ C_3 \left[ 1 - \exp(C_6 R_t^{1/4}) \right] \right\}
\]

\[
\Pi = \left[ \frac{C_0 \nu_T}{f_\mu^2} \sigma_k \right]_{ij}
\]

\[
\bar{\varepsilon} = \epsilon \left[ 1 - \exp(-R_t^{1/2}) \right]
\]

where \( R_t = k^2/\nu \), \( C_0 = .004 \), \( C_3 = .0004 \), \( C_6 = 1.2 \)
The following figures show the predictions from the present model on fully developed channel flow compared with other models (including Jonse and Launder's model\cite{1}) and direct numerical simulation data.\cite{7} The open symbols represent direct numerical simulation, and the lines represent the model prediction.
2. Second order modeling of near-wall turbulence

Using the near-wall asymptotic behavior of turbulence\(^{10}\) as model constraints, we formed a set of modeled transport equations for the Reynolds-stress tensor and the dissipation rate of turbulent kinetic energy. The main emphasis was on developing a near-wall model for the pressure correlation and dissipation terms in the Reynolds-stress equation. A modeled dissipation rate equation is derived more rationally. Asymptotic analysis shows that near the wall, the viscous diffusion term in the Reynolds-stress equations becomes the leading term and is balanced by the pressure correlation and dissipation terms. We use this as a model constraint in the model development. The proposed models satisfy realizibility and ensure no unphysical behavior will occur. Here, we briefly describe and list the proposed models.

Reynolds stress equation

The exact equation for the Reynolds stress tensor is:

\[
\frac{D}{Dt}(u_i u_j) = P_{ij} + T_{ij} + D_{ij}^{(v)} + \Pi_{ij} - \epsilon_{ij}
\]

where \( \langle \cdot \rangle \) stands for an ensemble average, \( D/Dt = \partial / \partial t + U_k \partial / \partial x_k \). The terms \( P_{ij}, T_{ij}, D_{ij}^{(v)}, \Pi_{ij} \) and \( \epsilon_{ij} \) represent the production, turbulent diffusion, viscous diffusion, velocity pressure-gradient correlation and dissipation tensor, and are identified as follows:

\[
\begin{align*}
P_{ij} &= -\langle u_i u_k \rangle U_{j,k} - \langle u_j u_k \rangle U_{i,k} \\
T_{ij} &= -\langle u_i u_j u_k \rangle,_{k} \\
D_{ij}^{(v)} &= \nu \langle u_i u_j \rangle,_{kk} \\
\Pi_{ij} &= -\frac{1}{\rho} \langle u_i p_j + u_j p_i \rangle \\
\epsilon_{ij} &= 2\nu \langle u_{i,k} u_{j,k} \rangle
\end{align*}
\]

The proposed near-wall model for \( \Pi_{ij} - \epsilon_{ij} \) is:

\[
\Pi_{ij} - \epsilon_{ij} = -f_w \frac{\epsilon}{\langle \sigma^2 \rangle} [2(u_i u_j) + 4(\langle u_i u_k \rangle n_j n_k + \langle u_j u_k \rangle n_i n_k) + 2(u_k u_i) n_k n_i n_j]
\]

where \( n_i \) is a unit vector normal to the surface, and \( f_w = \exp(-(R_t/C_1)^2) \), \( R_t = \frac{(\sigma^2)^2}{\rho \nu \epsilon} \), \( C_1 = 1.358 R_{er}^{0.44} \), \( R_{er} = u_r \delta / \nu \). \( u_r \) is the friction velocity, \( \delta \) is the thickness of the boundary layer or the half width of the channel.

Away from the wall, the velocity pressure-gradient correlation \( \Pi_{ij} \) is split into the rapid part \( \Pi_{ij}^{(1)} \) and the slow part \( \Pi_{ij}^{(2)} \):

\[
\Pi_{ij} = \Pi_{ij}^{(1)} + \Pi_{ij}^{(2)}
\]
The proposed model for $\Pi^{(2)}_{ij} - \epsilon_{ij}$ is:

$$\Pi^{(2)}_{ij} - \epsilon_{ij} = -\epsilon(\beta b_{ij} + \frac{2}{3} \delta_{ij})(1 - f_\omega)$$

where

$$\beta = 2 + \frac{F}{9} \left\{ \frac{72}{R_t^{1/2}} + 80.1 \ln[1 + 62.4(-II + 2.3III)] \right\} \exp\left( -\frac{7.77}{R_t^{1/2}} \right)$$

$$F = 1 + 27III + 9II$$

$$II = -\frac{1}{2} b_{ij} b_{ji}$$

$$III = \frac{1}{3} b_{ij} b_{jk} b_{ki}$$

$$b_{ij} = \frac{(u_i u_j)(q^2)}{\epsilon} - \delta_{ij}/3$$

The rapid part of velocity pressure-gradient, $\Pi^{(1)}_{ij}$ is modeled as follows (Shih and Lumley [11,12]):

$$\Pi^{(1)}_{ij} = \frac{1}{5} (1 + 2a_5)(q^2)(U_{i,j} + U_{j,i}) - \frac{2}{3} (1 - a_5)(P_{ij} - \frac{2}{3} P \delta_{ij})$$

$$+ \left( \frac{2}{3} + \frac{16}{3} a_5 \right)(D_{ij} - \frac{2}{3} P \delta_{ij}) + \frac{2}{15} (P_{ij} - D_{ij}) + \frac{6}{5} b_{ij} P$$

$$+ \frac{2}{5(q^2)}([((u_i u_k)U_{i,q} + (u_j u_k)U_{j,q})(u_k u_q) - (u_i u_p)(u_j u_q)(U_{p,q} + U_{q,p})]$$

where,

$$P_{ij} = -(u_i u_k)U_{j,k} - (u_j u_k)U_{i,k}$$

$$D_{ij} = -(u_i u_k)U_{k,j} - (u_j u_k)U_{k,i}$$

$$P = \frac{1}{2} P_{ii}$$

$$a_5 = -\frac{1}{10} (1 + C_2 F^{1/2})$$

$$C_2 = 0.8[1 - \exp(-(R_t/40)^2)]$$

Finally the model for the third moments is modeled as:

$$q^2(\langle u_i u_j u_k \rangle - 0.07 \frac{(q^2)}{2\epsilon} [(u_k u_p)(u_i u_j)_{,p} + (u_j u_p)(u_i u_k)_{,p} + (u_i u_p)(u_j u_k)_{,p}$$

**Dissipation rate equation**

The modeled dissipation rate equation derived in this work is:

$$\epsilon_{,i} + U_i \epsilon_{,i} = (\nu \epsilon_{,i} - (\epsilon u_i))_{,i} - \psi_0 \frac{\epsilon}{(q^2)} \epsilon$$

$$- \psi_1 \frac{\dot{\epsilon}}{q^2} (u_i u_j)U_{i,j} - \psi_2 \frac{\nu(q^2)}{\epsilon} (u_k u_l) (U_{i,jl} - U_{l,ij}) U_{i,jk}$$

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where

\[ \psi_0 = \frac{14}{5} + 0.98[1 - 0.33\ln(1 - 55I_f)]\exp(-2.83R_t^{-1/2}) \]

\[ \psi_1 \approx 2.1 \]

\[ \psi_2 = -0.15(1 - F) \]

\[ \bar{\varepsilon} = \varepsilon - \frac{\nu(q^2)_i(q^2)_j}{4(q^2)} \]

The turbulent flux term \( \langle \epsilon u_k \rangle \) is modeled as:

\[ \langle \epsilon u_k \rangle = -0.07 \frac{(q^2)}{2\varepsilon} (u_k u_p) \epsilon, p \]

These figures show some existing Reynolds stress models (for example, Launder and Shima\[13\], Lai and So\[14\]) and present model compared with the direct numerical simulations.[7]
UNCLASSIFIED

Mean velocity $U/u^*$

Turbulent kinetic energy $k/u^*$

Intensities

$U$ - MEAN VELOCITY

$K$ - KINETIC ENERGY

U, V, W -- RMS OF FLUCTUATING VELOCITY

$\langle UV\rangle$ PROFILE

UNCLASSIFIED
3. **Second order modeling of a three-dimensional boundary layer**

A study\textsuperscript{[15]} of three-dimensional effects on turbulent boundary layer were achieved by direct numerical simulation of a fully developed turbulent channel flow subjected to transverse pressure gradient. The results show that, in agreement with experimental data\textsuperscript{[16]}, the Reynolds stresses are reduced with increasing three-dimensionality and that, near the wall, a lag develops between the stress and the strain rate. To model these three-dimensional effects on the turbulence, we have tried various two equation models and second order closure models. None of the current models can predict the reductions in the shear stress observed using direct numerical simulations. However, we found that the newly proposed second order closure model listed in the previous section do at least qualitatively capture these three-dimensional effects.
The following figures show the direct numerical simulation of the three dimensional boundary layer flow and the model predictions from Launder and Shima, Lai and So and the present models.

Schematic of three-dimensional channel flow.

Turbulent intensities in fixed coordinates at \( \Delta t = 0.15 \) intervals.

Reynolds stress component in fixed coordinate at \( \Delta t = 0.15 \) intervals.

Distribution across the channel of the mean flow angle (---), the Reynolds shear stress angle (-----), and the mean velocity gradient angle (----).
References


Second Order Modeling of Boundary-Free Turbulent Shear Flows

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Abstract

This paper presents a set of realizable second order models for boundary free turbulent flows. The constraints on second order models based on the realizability principle are re-examined. The rapid terms in the pressure correlations for both the Reynolds stress and the passive scalar flux equations are constructed to exactly satisfy the joint realizability. All other model terms (return-to-isotropy, third moments and terms in the dissipation equations) already satisfy realizability (Lumley 1978, Shih and Lumley 1986). To correct the spreading rate of the axisymmetric jet, an extra term is added to the dissipation equation which accounts for the effect of mean vortex stretching on dissipation. The test flows used in this study are the mixing shear layer, plane jet, axisymmetric jet and plane wake. The numerical solutions show that the new unified model equations (with unchanged model constants) predict all these flows reasonably as the results compare well with the measurements. We expect that these model equations would be suitable for more complex and critical flows.
Evaluation of Turbulence Models for Predicting Buoyant Flows

Experimental data for the buoyant axisymmetric plume are used to validate certain closure hypotheses employed in turbulence model equations for calculating buoyant flows. Closure formulations for the turbulent transport of momentum, thermal energy, kinetic energy, and squared temperature used in the k-ε and algebraic stress models are investigated. Experimental data for the mean velocity, mean temperature, and kinetic energy are used in the closure formulation to obtain Reynolds stresses, heat fluxes, etc., which are then compared with their measured values.

1 Introduction

Various turbulence models have been formulated for predicting buoyancy-driven flows. Some of the parameters in these models have been determined by keying the solution of the model equations to experimental data for certain basic flows such as decay of grid turbulence. Other parameters have been determined by calibrating closure formulations directly with experimental data. However, this approach may be somewhat inaccurate due to the lack of quality experimental data for certain correlations, especially dissipation. Finally, certain model parameters have been fine tuned or determined by requiring that the computed solution agree with experimental data for more complex flows, such as shear flows. In addition, there have been instances where model parameters have been adjusted or empirical corrective terms added so that agreement with experimental data is accomplished for a particular flow. When model parameters are adjusted to get agreement, say for the mean velocity and temperature fields for a particular flow, little regard is given for the internal integrity of the model. In other words, the various processes such as diffusion transport, pressure-strain interactions, etc., predicted correctly? Or are there compensating assumptions where one process is overpredicted at the expense of another and yet the end predicted result for the mean flow agrees with experiment? The lack of complete sets of data for higher moments, dissipation, and pressure–velocity correlations for various flows has prevented detailed verification of closure models for the various processes that have to be modeled.

The objective of this paper is to use the recently obtained a comprehensive experimental data of Shabbir and George (1987) and Shabbir (1987) on the axisymmetric buoyant plume to assess the various closure relations proposed for the kinetic-energy/dissipation and the algebraic stress models for buoyancy-dominated flows. The usual approach is to solve the modeled differential equations numerically, and then compare the computations with the experiment. However, this method does not help pinpoint the drawbacks in the various terms of the models. In this paper, instead of the usual approach, correlations obtained from measured velocity and temperature are used directly to verify the closure hypotheses for the turbulent transport of momentum, thermal energy, and turbulent kinetic energy.

2 Experimental Data

The data used were taken in an axisymmetric buoyant plume by Shabbir and George (1987) and Shabbir (1987), who measured velocity and temperature fields at several vertical levels above a heated source of air. Here we briefly summarize their experimental technique and results.

The three wire probe used consisted of a cross-wire and a temperature wire. Thus the instantaneous values of the two velocity components (vertical and radial) and temperature were measured. The axisymmetry of the flow was established by using an array of 16 thermocouples and also by rotating the cross-wire by 90 deg. Profiles for the correlations between the velocity components and velocity components with temperature through the fourth order were determined from the instantaneous measurements.

Source conditions were continuously monitored in order to calculate the rate at which buoyancy was added at the source. The source Grashof number was 5.5. By integrating the mean energy equation, an integral constraint can be obtained for a buoyant plume. For a neutral environment this constraint implies that the rate at which buoyancy crosses each horizontal section is constant and must equal the rate at which buoyancy is added at the source, i.e., the ratio

\[
\frac{F_p}{F_c} = \frac{1}{2 \pi} \int_{0}^{2 \pi} \left[ \epsilon \frac{\partial \nabla U \nabla T + \nabla U \nabla T \right]_{\eta} d\eta
\]

must be unity (\(F_c\) is the source buoyancy). This integral constraint was satisfied within 7 percent.

The correlation profiles at various heights were found to be similar in the coordinate \( \eta = \frac{z}{L} \) (\(L\) accounted for the virtual origin) when the velocity is scaled by \( U_c F_c^{2/3} z^{-1/3} \) and the temperature is scaled by \( T_c = F_c^{2/3} z^{-1/3} \). The measurements agreed well with the earlier study by George et al. (1977), who measured only the temperature and the vertical component of velocity. The scatter in the measurements of higher moments is typical for such flows and is also present in previous experiments, such as those of George et al. (1977). The primary reason for the scatter is that when slow timescales of the flow require much longer averaging time for the higher moments in order to obtain the same statistical convergence as for the mean quantities. Other errors in the measurements arise from the flow reversal on the hot wire—a phenomenon most likely to occur toward the outer edges of the flow where local turbulent intensities are considerably higher. These are discussed in Shabbir and George (1987).

The various correlations in similarity variables were fitted with curves using a least-squares fitting procedure. This representation allows easy evaluation of the terms in the governing equations and closure formulations when they are cast in similarity variables. Using these profiles the balances for the mean momentum and energy differential equations were carried out to check whether the flow satisfied the equations of motion it is supposed to represent. Within the thin shear layer and the Boussinesq assumption the mean momentum and energy equa-
tions can be respectively written as
\[ \frac{1}{r} \frac{d}{dr} (r \Delta U) + V \frac{\partial U}{\partial r} = -\frac{1}{r} \frac{\partial}{\partial r} (r \bar{u} \bar{v}) - g \beta \Delta T \]
\[ \frac{U}{\Delta T} + V \frac{\partial \Delta T}{\partial r} = -\frac{1}{r} \frac{\partial}{\partial r} (r \bar{u} \bar{v}) \]

Since all the quantities appearing in these equations are measured, their profiles were substituted to see whether the measurements balance the equations. Figure 1(a), taken from Shabbir and George (1987), shows that the experiment satisfies this nontrivial test within 10 percent. An error of such magnitude is typical of turbulent shear flows.

The dissipation of mechanical energy was determined by balancing the turbulent energy equation

\[ U_j \frac{\partial \Delta T}{\partial x_j} = \frac{\partial}{\partial x_j} \left( -\frac{1}{2} \frac{\partial U}{\partial x_j} + \frac{1}{\rho} \frac{\partial \bar{p} \bar{u}}{\partial x_j} \right) + P + G - \epsilon \]

where \( P = -\bar{u} \bar{v} \frac{\partial U}{\partial x_j} \) is the mechanical production and \( G = -\beta g \bar{T} \) is the production due to buoyancy. Each term except for the dissipation \( \epsilon \) and the pressure transport \( \bar{p} \bar{u} \) is determined from the experimentally determined correlations. The pressure transport was evaluated from \( \bar{p} \bar{u} / \rho = -\bar{q} \bar{u} / \bar{z} \), a formula given by Lumley (1973). Although this closure relation has not been verified experimentally, it was felt that since the pressure transport is significant, some correction should be included rather than simply neglecting it, as is often done. The dissipation determined from the balance of the turbulent kinetic energy equation is shown in Fig. 1(a) as a solid line.

By a similar procedure the dissipation of the mean-square temperature \( \bar{T} \) is determined from

\[ U_j \frac{\partial^2 \bar{T}}{\partial x_j} = -\frac{\partial}{\partial x_j} \frac{\bar{u} \bar{v}^2}{3} - 2 \bar{u} \bar{v} \bar{T} \frac{\partial T}{\partial x_j} - \epsilon \]

All terms are evaluated from experimental data and the resulting thermal dissipation is shown in Fig. 1(b).

The time scales \( T_\epsilon \) and \( T_\bar{T} \) for the relaxation of the mechanical and thermal dissipation, respectively, are shown in Fig. 2, along with their ratio

\[ R = (T_\bar{T} / \epsilon) / (T_\epsilon / \epsilon) \]
By invoking the thin shear layer assumption for a buoyant plume, the above relations reduce to

\[
\overline{u'u'} = -r_T \frac{\partial U}{\partial r}
\]

\[
\overline{uT} = - (r_T/Pr_T) \frac{\partial T}{\partial z}
\]

\[
\overline{uT} = - (r_T/Pr_T) \frac{\partial T}{\partial r}
\]

Taking \( Pr_T = 1.0 \), the right-hand sides of the above equations were evaluated experimentally. These are compared with measured values of \( \overline{u'u'} \), \( \overline{uT} \), and \( \overline{uT} \) in Figs. 3-5. The points are experimental values and the chain lines are from the model.

The modeled values of \( \overline{u'u'} \) and \( \overline{uT} \) compare reasonably with the experimental profiles except in the outer portion of the curves. On the other hand, the modeled profile of vertical heat flux \( \overline{uT} \) is much smaller than the experimental one. It is well known that the simple gradient models given by equations (7) and (8) with an isotropic eddy viscosity are inadequate for determining streamwise turbulent momentum and heat fluxes. Usually these quantities do not influence the prediction for shear layers since only the radial fluxes are important in these flows. However, in the case of the buoyant plume the flux \( \overline{uT} \) is a dominant production term in the turbulent kinetic energy.
equation and its correct calculation is very important for accurate prediction of \( k \).

The diffusional transport in the kinetic energy equation (4) for a thin shear layer is modeled as

\[
\frac{1}{2} \frac{\partial \rho^2}{\partial t} + \frac{1}{\rho} \frac{\partial \rho \overline{u} \overline{v}}{\partial t} = -\frac{\partial}{\partial x_j} \left( P + G \right) - C_2 \frac{\partial k}{\partial t} - C_3 \frac{\partial \epsilon}{\partial t}
\]  

(9)

Using \( \overline{\rho \overline{u} \overline{v}} / \rho = -\overline{\rho \overline{u} \overline{v}} / 5 \) from Lumley (1978) gives \( \overline{\rho^2} / 2 = -\left(5/3\right) \rho \overline{\rho \overline{u} \overline{v}} / \partial t \) from which the result, with the right side evaluated from experimental results, is shown in Fig. 6. It is seen that the predicted and experimental data peak at different radial locations; however, the predicted magnitude is more accurate, which indicates that the pressure diffusion needed to be taken into account.

In the \( k-\epsilon \) model the dissipation is calculated from

\[
\frac{\partial}{\partial t} \left( P + G \right) - C_2 \frac{\partial k}{\partial t} - C_3 \frac{\partial \epsilon}{\partial t} = \frac{\partial}{\partial x_j} \left( \overline{u \partial U / \partial x_j} \right)
\]  

(10)

where \( \epsilon / \rho \overline{u} \overline{v} = -\left(\gamma / \rho \right) \delta \overline{u} / \partial x_j \) and \( \alpha_1 = 1.3, C_{1 \epsilon} = 1.44, \) and \( C_{3 \epsilon} = 1.92 \) as given by Launder and Spalding (1974). In order to get an indication of the validity of equation (10), it was numerically solved for the dissipation \( \epsilon \) with all other quantities needed to evaluate the coefficients determined from the experimental correlations. The result is shown in Fig. 1(b) and it is seen that it compares reasonably well with the curve obtained from balancing the turbulent kinetic energy equation with experimental data.

Launder et al. (1972) showed that the standard \( k-\epsilon \) model yields a solution for the axisymmetric jet that overpredicts the spreading rate by about 30 percent. The standard \( k-\epsilon \) model also does not correctly predict the axisymmetric buoyant plume (Hossain and Rodi, 1982). Proposals have been made (Pope, 1978; Hanjalic and Launder, 1980) for modifying the dissipation equation, based on arguments concerned with vortex or eddy structures characteristic of axisymmetric flows. The modified equation produces more dissipation, thus decreasing the turbulent eddy viscosity, which results in a smaller spreading rate of the flow. Here we use the empirical correction given by Rodi (1972) where \( C_{2 \epsilon} = 1.92 \left(1-0.035H \right) \) with \( H = \left( \gamma \rho / U_{\infty} \right) \overline{\rho \overline{u} \overline{v}} / \partial x_j \) and where \( U_{\infty} \) is the maximum velocity and \( \gamma \) is the distance from the centerline to the edge of the shear layer. This correction decreases the destruction term in the dissipation equation, hence producing an increased dissipation.

However, when this correction is used in equation (10) there is very little change in the solution for \( \epsilon \) when experimental data are used for the other quantities in the equation. This is probably due to the approach taken here, which does not allow for the nonlinear interactions between the various terms in the closure. If the kinetic energy and dissipation equations are solved simultaneously, then the axisymmetric correction will produce a significant change in the solution of the \( k-\epsilon \) model.

4 Assessment of Closure Hypotheses for Algebraic Stress Model

Chen and Rodi (1975), Tamanini (1978), Chen and Chen (1979), and Hossain and Rodi (1982) have made predictions for the buoyant jet using algebraic stress models. Many of the ideas used in these models for calculating buoyant flows originated with Launder (1975, 1978). Algebraic stress models are obtained by simplifying the convective transport equations for Reynolds stresses and heat fluxes so they are no longer differential equations. The dynamic equation for the Reynolds stress tensor is

\[
(C - D)_{\epsilon ij} = P_{ij} + G_{ij} - \frac{2}{3} \rho \overline{e} \delta_{ij}
\]

\[
- C_4 \epsilon \left( \frac{\partial U_i}{\partial x_j} - \frac{1}{3} \delta_{ij} \right) - C_2 \left( P_{ij} - \frac{2}{3} \rho \overline{e} \delta_{ij} \right)
\]

\[
- \frac{30C_4}{5} \left( D_j - \frac{2}{3} \rho \overline{e} \right) - \left( 8C_2 - 6k \right) \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right)
\]

\[
- C_3 \left( G_{ij} - \frac{2}{3} \rho \overline{e} \delta_{ij} \right)
\]

where \( P_{ij} = -\overline{u_i \partial u_j / \partial x_i} - \overline{u_i \partial u_j / \partial x_j} \) is the mechanical production and \( G_{ij} = -\beta \gamma \overline{u_i \partial u_j / \partial x_j} \) is the buoyancy production. The left side represents convection minus diffusional transport, the dissipation is assumed isotropic, and the last three lines represent the closure formulation for \( p \left( \partial U_i / \partial x_j + \partial U_j / \partial x_i \right) / \rho \) given by Launder et al. (1975) and Launder (1975, 1978). Launder assumes: (1) an equilibrium situation where convection is balanced by diffusion \( (C - D = 0) \) and production is balanced by dissipation \( (P + G - \epsilon = 0) \); (2) the second and third terms (third line) in the rapid part of the pressure–velocity correlation are negligible; the coefficient \( C_2 \) is adjusted so that the first term approximates the entire rapid part; (3) the parameter \( C_3 \) is taken equal to \( C_{1 \epsilon} \). After applying all the assumptions

\[
\overline{u_i \partial j} = \frac{2}{3} \frac{C_1 + C_2 - 1}{C_3} \frac{\partial k}{\partial x_j} - \frac{1}{3} \frac{C_2}{C_1} \left( P_{ij} + G_{ij} \right)
\]

where \( C_1 = 2.2 \) and \( C_2 = 0.6 \). It should be pointed out that in free shear flows the equilibrium condition \( (C - D = 0) \) and the first line in the outer portion of the flow. Also, Zeman and Lumley (1978) found \( C_3 = 0.3 \), after applying all the constraints applicable to determining the contribution of buoyancy to the pressure-strain correlation.

The dynamic equation for the heat flux is

\[
(C - D)_{\epsilon ij} = -\overline{u_i \partial T / \partial x_j} - \overline{u_j \partial T / \partial x_i} - \beta \gamma \overline{u_i \partial T / \partial x_j}
\]

\[
- C_4 \epsilon \left( \frac{\partial T}{\partial x_j} + C_{u \gamma} \overline{u_j \partial T / \partial x_j} \right)
\]

\[
- \frac{30C_4}{5} \left( D_j - \frac{2}{3} \rho \overline{e} \right) - \left( 8C_2 - 6k \right) \left( \frac{\partial T}{\partial x_j} + C_{u \gamma} \overline{u_j \partial T / \partial x_j} \right)
\]

where the first line on the right side is the production and the second line is the closure for \( \partial \rho \partial T / \partial x_j \). Neglecting convection and diffusion \( (C - D = 0) \) and the third term in the second line, equation (13) becomes

\[
\overline{u_i \partial T / \partial x_j} = \frac{1}{C_4} \left[ -\overline{u_i \partial T / \partial x_j} - \left( 1 - C_3 \right) \overline{u_j \partial T / \partial x_j} - (1 - C_3) \beta \gamma \overline{u_i \partial T / \partial x_j} \right]
\]

where \( C_4 = 3.0, C_{u \gamma} = 0.5 \), and \( C_{u \gamma} = 0.5 \). Zeman and Lumley (1976) show that \( C_{u \gamma} = 0.8 \) and \( C_{u \gamma} = 0.2 \) from theoretical considerations.

Neglecting the convection and diffusional transport in equation (5) and eliminating \( \epsilon \) with equation (6) gives

\[
\overline{T} = -R \frac{k}{\epsilon} \frac{\partial T}{\partial x_i}
\]

(13)
which was given by Launder (1975, 1978) and used by Hossain and Rodi (1982).

Chen and Rodi (1975) and Chen and Cheng (1979) used the differential equation (5), with $\epsilon$ eliminated by using equation (6) to determine $r$ rather than using equation (15). In either case $R$ is taken to be a constant equal to 0.8 (Hossain and Rodi, 1982; Chen and Rodi, 1975; Chen and Chen, 1979; Launder, 1975, 1978). It is seen in Fig. 2 that the experimentally determined value of $R$ is much lower with an average value across the profile of roughly 0.25. Launder (1978) cites experimental evidence for $R$ being in the range of 0.3 to 0.8. However, he found that the algebraic stress relations agreed best with an experiment for a stably stratified homogeneous shear flow with $R = 0.8$. Hence, that value has been adopted in the algebraic stress models. The experimental results of Shabbir and George (1987) indicate $R$ is much lower for strongly buoyant flows. When the algebraic stress model is applied to this experiment with $R = 0.8$, the results are very poor for $r^2$. Therefore, in the following evaluation of the algebraic stress model, the experimentally determined profile for $R$ (Fig. 2) is used.

Equations (10), (12), and (13) represent a system of algebraic equations that can be solved for $\bar{u}\bar{u}, \bar{u}\bar{v},$ and $r^2$. Employing the thin shear layer approximation, where only gradients in the radial direction are retained, Hossain and Rodi (1982) give

$$
\overline{u^2} = \frac{2}{3} \frac{C_1 + C_2 - 1}{C_1} k + \frac{1 - C_2}{C_1} \epsilon \left( -\frac{3\bar{u}}{2} \frac{\partial U}{\partial r} + 2\bar{u}g \right)
$$

(16)

$$
\overline{u\bar{v}} = -\frac{1 - C_2}{C_1} k \epsilon \left( -\frac{3\bar{u}}{2} \frac{\partial U}{\partial r} + g \bar{u} \right)
$$

(17)

$$
r^2 = \frac{2}{3} \frac{C_1 + C_2 - 1}{C_1} k
$$

(18)

$$
\bar{u} = \frac{1}{C_{lu}} \epsilon \left[ \overline{\bar{u}\bar{\eta}} - \left( 1 - C_{lu} \right) \overline{\bar{u}} \frac{\partial U}{\partial r} + \left( 1 - C_{lu} \right) \bar{g} \epsilon \right]
$$

(19)

$$
\bar{v} = \frac{1}{C_{lv}} \epsilon \left[ \frac{\partial \bar{T}}{\partial r} - \overline{\bar{u}\bar{\eta}} \right]
$$

(20)

$$
\bar{T} = -2r \frac{\bar{v}}{\epsilon} \frac{\partial \bar{T}}{\partial r}
$$

(21)

from which $r = \frac{C_{k^2}}{\epsilon}$ where

$$
C_{k^2} = \frac{2}{3} \frac{(1 - C_1)(C_1 + C_2 - 1)}{C_1} \left( 1 + \frac{1}{C_{lu}} \frac{g}{\epsilon} \frac{\partial \bar{T}}{\partial r} \frac{\partial U}{\partial r} \right)
$$

(22)

The system of equations (16)-(21) was solved to determine the Reynolds stress and heat flux components with $\bar{U}, \bar{T}, k, \epsilon,$ and $R$ given by the experiment. The following values for the constants were used:

$$
C_1 = 2.2, \quad C_2 = 0.6, \quad C_3 = 0.6
$$

$$
C_4 = 3.0, \quad C_5 = 0.5, \quad C_p = 0.5
$$

The value of $C_{k^2}$ which appears in the eddy viscosity relation $v = \frac{C_{k^2}}{\epsilon}$ is given by equation (22), is roughly 0.125 and is reasonably constant across the flow. This value is considerably larger than the value of $C_k = 0.09$ for the standard $k-\epsilon$ model. Rodi (1972), to correct for the discrepancies in the predictions for the axisymmetric jet, developed an empirical correction to $C_k$. The parameter $C_k$ is replaced by (1-$0.465H/C_\infty$), where $H = 1(Y_w/U_0) dU_0/dx$, $U_0$ is the maximum velocity, and $Y_w$ is the distance from the centerline of the edge of the jet. Hossain and Rodi (1982), Chen and Rodi (1975), and Chen and Chen (1979) used this correction in their predictions for turbulent buoyant jets. When the correction is applied, we get approximately 0.09, which is the value of $C_k$ for the standard $k-\epsilon$ model.

The question we are asking is, "given the turbulent energy, dissipation, velocity, and temperature, does the proposed algebraic stress expression correctly predict the Reynolds stress and heat flux components?" Figure 8 shows the radial Reynolds stress determined from equation (18). It is seen that the predicted value $\rho k = 0.53$ is a little smaller than the experimental curve in the center portion of the plume, but agrees quite well with experiment in the outer portion. The predicted shear stress $\bar{u}\bar{v}$, the axial heat flux $\bar{u}\bar{T}$, the radial heat flux $\bar{u}\bar{T}$, and the mean squared temperature $\bar{T}$ are shown in Figs. 3, 4, 5, and 7, respectively. Again the points are experimental data and the broken lines are from the model. It is seen that the shear stress $\bar{u}\bar{v}$ and radial heat flux $\bar{u}\bar{T}$ are predicted reasonably. However, the vertical heat flux $\bar{u}\bar{T}$ and temperature fluctuations $\overline{\rho T^2}$ are predicted poorly and have incorrect shapes; unlike the experimental values they go to zero near the origin.

Equation (21) gives $r^2$ proportional to the radial temperature gradient, which is zero at the centerline. Then since $r^2 = 0$ at $r = 0$, equation (19) gives $\bar{v} = 0$ at $r = 0$. In order to obtain nonzero values for $\bar{u}$ and $r^2$ at the centerline from the model equations (12), (14), and (15), terms containing the axial gradient, i.e., $\frac{\partial \bar{u}}{\partial z}$ and $\frac{\partial \bar{T}}{\partial z}$, were retained. These terms were added to equations (19) and (21) and the system of equations was solved again. Although the centerline values of $\bar{u}$ and $r^2$ were found to be nonzero, the predictions still decreased to relatively small values near the centerline.

Another possibility for this behavior is the neglect of advection and diffusion terms in the model. Gibson and Launder (1976) have proposed the following model for these terms:

$$
(C - D)_{\bar{z}} = \frac{\bar{u}\bar{T}}{2} \left( P_1 - \epsilon \right) + \frac{\bar{u}^2}{2} \left( P_1 - \epsilon \right)
$$

(23)

where $P_1$ is the production term in the $\overline{\rho T^2}$ equation. These were
Chen (1978) show reasonable agreement with the experiment for the mean velocity and buoyancy. The answer to this is that with \( R = 0.8 \) the temperature variance \( \theta^2 \) from equation (21) or (25) is too large. This makes the vertical heat flux \( \gamma \) from equation (19) large enough so that the mean velocity and buoyancy are reasonably predicted.

5 Summary and Conclusions

The experimental data on buoyant plumes were used to evaluate various closure relations for turbulence transport. The objective was not to propose new models, but to evaluate the closure schemes proposed by other workers for buoyancy-dominated flows. The closures evaluated were those used in the \( k-e \) and algebraic stress models. The results are summarized below.

1 The closure relations of the \( k-e \) model compare reasonably with experimental data, except for the axial turbulent transport, which is drastically underestimated. The axial heat flux governs the production due to buoyancy in the kinetic energy and dissipation equations and its correct prediction is very important. This is a probable reason why the results of Hossain and Rodi (1982) from the \( k-e \) model underpredict the spreading rate for the plume by 10 percent even when axisymmetric jet corrections are included.

2 The ratio \( R \) of the time scales, which is used to determine the dissipation of the mean squared temperature in the algebraic stress model, was found to be considerably different from the accepted value of \( R = 0.8 \). Apparently \( R \) is not a universal constant, but can vary from flow to flow and is influenced by the strength of the buoyancy present. From the experimental data on a plume it appears that \( R = 0.25 \) for strongly buoyant flows.

3 The closure equations for the shear stress and radial heat flux of the algebraic stress models also compared well with experiment but are not better than the simple gradient closures used in the \( k-e \) model. The axial heat flux and mean squared temperature are predicted poorly in the central core of the flow and had incorrect trends. This drawback could be attributed to the assumption of local equilibrium, which resulted in the neglect of convection and diffusion terms in the transport equations for Reynolds stress and heat flux. However, no substantial improvement was achieved by keeping the secondary derivatives or by incorporating the model for the convection and diffusion terms. Therefore, the full dynamic equations for Reynolds stress and heat flux with convection and diffusion are required to predict the axial heat flux and temperature variance properly.

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References


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